

DANIEL F. MERRIAM, Editor

**CORFAN - FORTRAN IV
COMPUTER PROGRAM FOR
CORRELATION, FACTOR
ANALYSIS (R- and Q-MODE)
AND VARIMAX ROTATION**

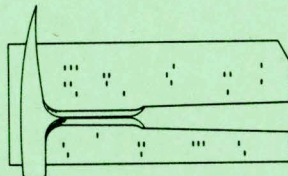
By

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and

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Kansas Geological Survey



COMPUTER CONTRIBUTION 42

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Editor's Remarks

This COMPUTER CONTRIBUTION 42, "CORFAN-FORTRAN IV computer program for correlation, factor analysis (R- and Q-mode) and varimax rotation", by C.W. Ondrick and G.S. Srivastava is an example of the larger more sophisticated programs now being developed. It embodies many "extras" not available in earlier programs of a similar nature. Because of complexity of the program, it is necessary to give detailed instructions on its use, but the rewards are greater for the effort as the results reflect the added analytical abilities. As stated by the authors the objectives of the programs are to (1) provide the researcher with a multivariate systems program package to accomplish maximum analysis with minimum computer runs, and to (2) analyze a large number of variables. Both objectives are met.

The program should find many uses in the earth sciences, especially in paleontology, sedimentology, and petrology. It provides a means of analyzing large amounts of data rapidly, and this is, of course, necessary in today's involved and complex scientific endeavors.

For a limited time the Geological Survey will make available on magnetic tape this computer program for \$25.00 (US). If punched cards are needed an extra \$10.00 is necessary to pay for handling and postage. An up-to-date, complete list of COMPUTER CONTRIBUTIONS can be obtained by writing, Editor, COMPUTER CONTRIBUTIONS, Kansas Geological Survey, University of Kansas, Lawrence, Kansas 66044.

Computer Contribution

- | | |
|---|----------------|
| 1. Mathematical simulation of marine sedimentation with IBM 7090/7094 computers, by J.W. Harbaugh, 1966 | (out of print) |
| 2. A generalized two-dimensional regression procedure, by J.R. Dempsey, 1966 | \$0.50 |
| 3. FORTRAN IV and MAP program for computation and plotting of trend surfaces for degrees 1 through 6, by Mont O'Leary, R.H. Lippert, and O.T. Spitz, 1966 | \$0.75 |
| 4. FORTRAN II program for multivariate discriminant analysis using an IBM 1620 computer, by J.C. Davis and R.J. Sampson, 1966 | \$0.50 |
| 5. FORTRAN IV program using double Fourier series for surface fitting of irregularly spaced data, by W.R. James, 1966 | \$0.75 |
| 6. FORTRAN IV program for estimation of cladistic relationships using the IBM 7040, by R.L. Bartcher, 1966 | \$1.00 |
| 7. Computer applications in the earth sciences: Colloquium on classification procedures, edited by D.F. Merriam, 1966 | \$1.00 |
| 8. Prediction of the performance of a solution gas drive reservoir by Muskat's equation, by Apolonio Baca, 1967 | \$1.00 |
| 9. FORTRAN IV program for mathematical simulation of marine sedimentation with IBM 7040 or 7094 computers, by J.W. Harbaugh and W.J. Wahlstedt, 1967 | \$1.00 |

(continued on inside back cover)

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CORFAN-FORTRAN IV COMPUTER PROGRAM FOR CORRELATION, FACTOR ANALYSIS (R- AND Q-MODE) AND VARIMAX ROTATION

by

C.W. Ondrick and G.S. Srivastava

INTRODUCTION

The geological maze (algorithm) as described by Griffiths (1966) illustrates a procedure for problem solving in the geosciences. The researcher collects data, transforms it to normal, classifies, correlates, factors, rotates, separates populations and plots results. Physically, considering the large volumes of data usually involved, it would be difficult to manipulate the analysis with pencil and pad. The digital computer has provided a rapid and precise means of data analysis for the modern researcher. Computer programs have been written separately for correlation, factor analysis and varimax rotation, and are provided at many computer centers.

The objectives of this computer contribution are: (1) to provide the researcher with a multivariate systems program package containing correlation, factor analysis (both R- and Q-modes) and varimax rotation linked together in a single program with a minimum of required parameter cards and computer runs; and (2) to produce a program capable of analyzing large numbers of variables (100) and which to a large extent is machine independent. Computer Contribution 30 (Griffiths and Ondrick, 1968) provided the first stage in statistical data analysis, namely logarithmic transformation, classification and regression analysis of data. The program described here provides a means for accomplishing the second stage in the geological algorithm-multivariate statistical analysis.

Acknowledgments. - CORFAN is a composite of four computer programs (COREL, FAN, QMOD, and VROT) originally written in FORTRAN II for the IBM 7074 computer. We express our thanks to The Pennsylvania State University Computation Center staff for the base programs from which this program was constructed. We also wish to thank Prof. John C. Griffiths for reading the manuscript and giving helpful suggestions. The FORTRAN IV program was tested in the GE 635 at the University of Kansas Computation Center.

PROGRAM DESCRIPTION

The general layout of CORFAN is illustrated in the flow diagram of Figure 1. Program dimensions provide intercorrelations between a maximum of 100

variables (5050 correlation coefficients), R-mode factor analysis with a maximum computation of 100 factors, of which up to 60 may be rotated (Kaiser, 1958), and analysis of an unlimited number of samples.

In Q-mode factor analysis the samples become the variables and the variables the samples, therefore the program dimensions provide for analysis of 100 samples. A value $\cos \theta$ (Imbrie and Purdy, 1962) is calculated for each pair of sample vectors and represents the input into factor analysis. Output from the Q-mode option includes IN (input matrix), DIV (divided matrix), and COS (Cos θ matrix) for each sample. The dimension restriction may be changed in statements MAIN 40, 45, and 91 to fit the core size required for a particular run. Card reader, printer and punch have been assigned variable names and their numerical designation may be altered in all subroutines by changing statements MAIN 80, 85, and 90 as desired.

There are 5 major options provided in this program: (1) correlation (including means and standard deviations); (2) correlation - R-mode factor analysis; (3) correlation - R mode factor analysis, varimax rotation; (4) Q-mode factor analysis; and (5) Q-mode factor analysis - varimax rotation. Additional options incorporated within the program are to punch correlation coefficients, alter diagonal elements of the correlation matrix, punch factor loadings, and bivariate plotting of input data or loadings of one factor against another, original or rotated. The "Hamburger Stand Option" (one with everything to go) produces a symmetrical correlation matrix of input variables and plots each variable against the other, calculates R-mode factor analysis for n factors, plots the factor loadings of each factor against the other, rotates J factors of the original factor matrix to "simple structure", and yields plots of the factor loadings of each rotated factor against the other. The number plotted on the output graph shows the number of points at that position, e.g. the number 2 indicates 2 points.

THOLEIITIC-ALKALIC BASALT PROBLEM

Defining the Problem

Eighty-six chemical analyses consisting of both tholeiitic and alkali basalt rocks from the Hawaiian

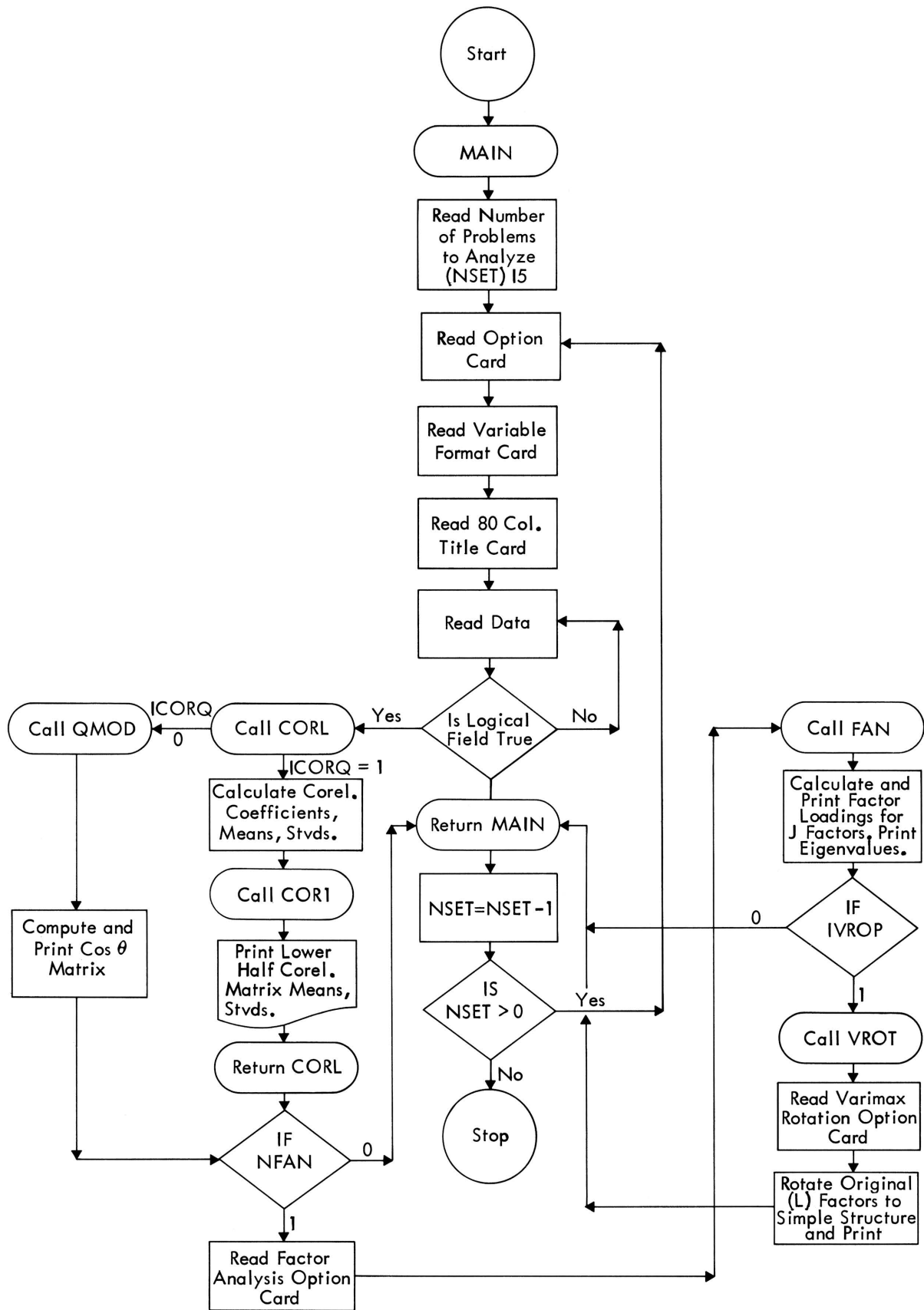


Figure 1. - Generalized flow diagram for CORFAN

Islands were subjected to factor analysis in the Q-mode for classification. Based upon simultaneous evaluation of 11 analyzed chemical oxides (SiO_2 , TiO_2 , Al_2O_3 , Fe_2O_3 , FeO , MnO , MgO , CaO , Na_2O , K_2O , P_2O_5) from each sample with respect to the other samples; a continuous series of samples ranging from alkali basalts to tholeiites is discernible. The analysis suggests a complete compositional gradation in basaltic magmas from alkalic to tholeiitic as well as exhibiting the potential value of factor analysis in the Q-mode in classifying rocks.

Introduction

Confusion is not an unfamiliar feeling to the igneous petrologist while trying to understand the differences and origin of what have been termed tholeiitic and alkali basalts (a concise review of the problem is given by Chayes, 1966; also see Kuno, 1959; Poldervaart, 1964). Some investigators rely on chemical composition while others use normative mineral percents or mineral composition in distinguishing between tholeiites and alkali basalts.

If indeed a distinct difference exists between the rocks which have been termed tholeiites and those classified as alkali basalts, certain combinations of the chemical oxides SiO_2 , TiO_2 , Al_2O_3 , Fe_2O_3 , FeO , MnO , MgO , CaO , Na_2O , K_2O , P_2O_5 when evaluated simultaneously for a group of samples should classify these samples into one of the two rock types or alternatively as neither. It is to be pointed out that the calculation of the percentage of normative minerals, given a rock of a particular chemical composition, and then the arbitrary assignment of certain percentages of these minerals as the "cut off" between the two rock types is a step executed only because the variation of the above 11 oxides composing the input for the norm calculation is not evaluated easily by the investigator. The simultaneous evaluation of 11 oxides of a particular sample with respect to other samples and then the classification of that sample based upon its overall similarity with the other samples is the concern of this example.

Procedure

In this investigation 86 chemical analyses of basaltic rocks from the Hawaiian Islands were selected randomly from over 200 analyses (C.P. Thornton, personal communication, 1969); 42 of these were classified by the investigators as tholeiites, 42 as alkali basalts and 2 were of unknown types. The norms of all rocks were calculated by computer. Then, the distinction between alkali and tholeiitic basalts was made based upon an arbitrary hypersthene value of 6 percent (A.J.R. White, personal communication, 1969), i.e. rocks containing greater than 6 percent normative hypersthene were classified as tholeiites and those with less than 6 percent were termed alkali basalts. After tentative classification

of rocks as either alkali or tholeiitic basalts the oxide percentages of each sample were subjected to factor analysis in the Q-mode which leads to the classification of samples in relation to "end member" components (Imbrie and Purdy, 1962). Figure 2 demonstrates the position of the samples with respect to each other when the factor loadings of the two axes are plotted.

Results

On the basis of the Q-mode classification of the 86 rocks investigated, 46 were classified as tholeiites, 23 as alkali basalts, and 17 as intermediate between the two rock types (Table 1). Seven alkali basalts and 5 tholeiites were classified differently from that suggested by White. The original petrographic point-count classification is in disagreement with White's and the Q-mode classification almost entirely within those rocks classed as alkali basalt, but agrees, with two exceptions, with respect to the tholeiites.

Summary and Conclusions

Based on the above results it seems that the simultaneous evaluation of chemical oxides for a given sample of basalt, using equal weighting of the oxides, and the subsequent classification of this sample by factor analysis in the Q-mode, yields a continuous series from alkali to tholeiitic basalts (Fig. 2). This implies the existence of a complete compositional gradation in basaltic magmas from tholeiitic to alkalic and not two separate parent magmas as has been suggested previously. Using the above classification the similarity of any one given sample to the other samples can be evaluated with respect to the 11 analyzed chemical oxides.

The above analysis is not intended to prove that, with respect to chemical composition, a complete gradation from alkali basalts to tholeiitic exists, because the experiment is restricted to rocks of the Hawaiian Islands and only 88 samples have been investigated. It is intended however to illustrate the potential value of the above technique in classifying all types of rocks in future investigations.

PROGRAM COMPATIBILITY AND MODIFICATIONS

This version of CORFAN has been compiled and executed successfully on both the GE 635 and IBM System/360 Model 50 computers. The program requires no external subroutines and makes use only of the system library subroutine SQRT (square root) and library function ABS (absolute).

Plots of loadings of both the unrotated and rotated factors against each other yield a "square" scattergram (approximately equal horizontal and

vertical scales). The vertical (Y axis) scale may be altered by changing statements FAN 1730 and VROT 1305. The maximum and minimum scale values for

both the vertical and horizontal scales may be altered by changing the numeric values of statements FAN 1710 through 1725 and VROT 1285 through 1300.

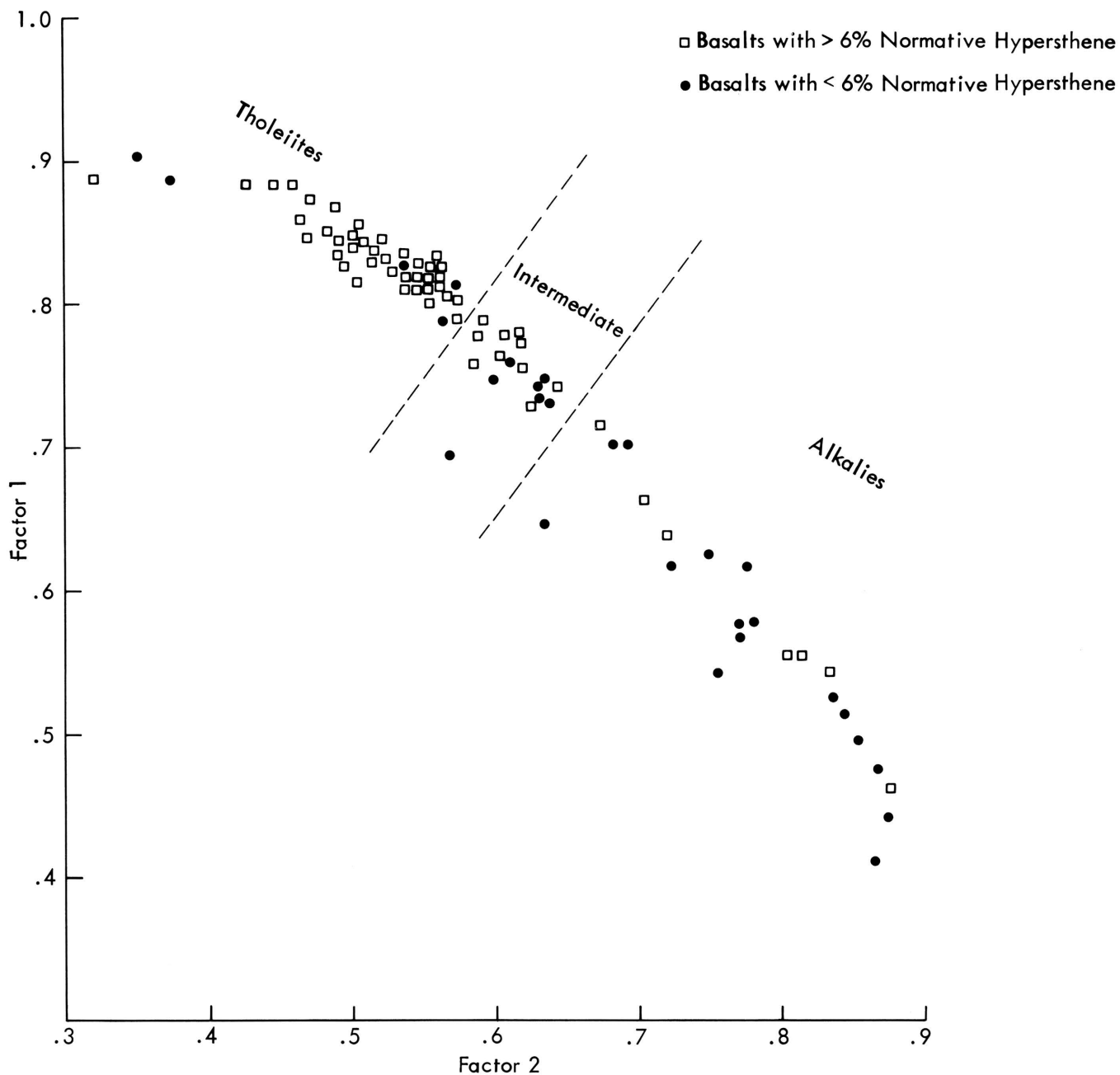


Figure 2. - Plots of loadings of rotated factor one against factor two and classification of basaltic samples on basis of factor analysis in Q-mode.

Table 1. - Classification of Hawaiian basalts as tholeiitic or alkalic by original investigator (petrographic), A.J.R. White (Normative) and Q-mode

Sample No.	Original Classification	White's Classification	Q-mode Classification
1	Alkali Basalt	Alkali Basalt	Alkali Basalt
2	Alkali Basalt	Alkali Basalt	Alkali Basalt
3	Alkali Basalt	Alkali Basalt	Alkali Basalt
4	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
5	Alkali Basalt	Alkali Basalt	Alkali Basalt
6	Alkali Basalt	Alkali Basalt	Intermediate
7	Alkali Basalt	Tholeiitic Basalt	Alkali Basalt
8	Alkali Basalt	Alkali Basalt	Intermediate
9	Alkali Basalt	Alkali Basalt	Intermediate
10	Alkali Basalt	Alkali Basalt	Alkali Basalt
11	Alkali Basalt	Tholeiitic Basalt	Alkali Basalt
12	Alkali Basalt	Alkali Basalt	Alkali Basalt
13	Alkali Basalt	Alkali Basalt	Alkali Basalt
14	Alkali Basalt	Alkali Basalt	Alkali Basalt
15	Alkali Basalt	Alkali Basalt	Alkali Basalt
16	Alkali Basalt	Tholeiitic Basalt	Alkali Basalt
17	Alkali Basalt	Alkali Basalt	Tholeiitic Basalt
18	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
19	Alkali Basalt	Tholeiitic Basalt	Intermediate
20	Alkali Basalt	Alkali Basalt	Alkali Basalt
21	Alkali Basalt	Alkali Basalt	Tholeiitic Basalt
22	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
23	Alkali Basalt	Alkali Basalt	Tholeiitic Basalt
24	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
25	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
26	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
27	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
28	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
29	Alkali Basalt	Tholeiitic Basalt	Tholeiitic Basalt
30	Alkali Basalt	Alkali Basalt	Tholeiitic Basalt
31	Alkali Basalt	Tholeiitic Basalt	Intermediate
32	Alkali Basalt	Alkali Basalt	Intermediate
33	Alkali Basalt	Alkali Basalt	Tholeiitic Basalt
34	Alkali Basalt	Tholeiitic Basalt	Intermediate
35	Alkali Basalt	Alkali Basalt	Intermediate
36	Alkali Basalt	Alkali Basalt	Intermediate
37	Alkali Basalt	Tholeiitic Basalt	Alkali Basalt
38	Alkali Basalt	Tholeiitic Basalt	Alkali Basalt
39	Alkali Basalt	Tholeiitic Basalt	Alkali Basalt
40-42	Alkali Basalt	Alkali Basalt	Alkali Basalt
43-69	Tholeiitic Basalt	Tholeiitic Basalt	Tholeiitic Basalt
70	Tholeiitic Basalt	Alkali Basalt	Alkali Basalt
71	Tholeiitic Basalt	Tholeiitic Basalt	Alkali Basalt
72-86	Tholeiitic Basalt	Tholeiitic Basalt	Tholeiitic Basalt

Program Input and Options

CARD 1

Col. 1-5 Number of sets of data (integer)

CARD 2

Col. 1-5 Total number of variables (integer)

Col. 6-10 Number of variables per data card (integer)

Col. 15 1 = Punch correlation matrix
0 = No punch of correlation matrix

Col. 16-23 Alphameric identification

Col. 30 1 = Produce factor analysis (see card 5)
0 = No factor analysis

Col. 35 1 = Produce varimax rotation (see card 6)
0 = No varimax rotation

Col. 40 1 = Produce correlation matrix which is input to R-mode factor analysis
0 = Cosine θ matrix generator which is input to Q-mode factor analysis

Col. 41 T = Bivariate plots of original data (see cards 5A, 6A)
F = No plotting original data

Col. 42 T = Bivariate plots of unrotated factor loadings (see cards 6B, 7B)
F = No plotting unrotated factor loadings

Col. 43 T = Bivariate plots of rotated factor loadings (see cards 7C, 8C)
F = No plotting rotated factor loadings

(Examples of parameter card 2 are presented in Table 2)

CARD 3

Col. 1-80 Variable format card of the form (nFX.Y, L1)
Where n is the number of variables per data card (cols. 6-10 of card 2), X is the field width, Y the number of decimal places, and L1 a logical field for termination)

CARD 4

Col. 1-80 Alphameric title card

Data cards

The data must be restricted to cols. 1 through 79 and the number of variables per data card are based on the number punched in cols. 6-10 of input card 2. For example if the total number of variables measured per sample is 29 and 8 variables are punched on a single card, 5 cards are required for each sample to input the 29 variables measured. Stack the 5 cards sequentially behind one another for each sample. Therefore if 100 samples were analyzed for 29 variables each, and 8 variables were punched per card 500 cards would be the data cards of this problem. The last card of a particular set of data must contain

a "T" in L field defined by the variable format (parameter card 3 above).

Plotting original data option cards
Parameter cards for plotting original data if card 2 col. 41 option is "T".

CARD 5A

Col. 1-5 Number of bivariate original data maps desired.

CARD 6A

Col. 1-5 Index (integer) for Y variable to be plotted against X variable

Col. 6-15 Upper limit of Y variable in floating point format

Col. 16-25 Lower limit of Y variable in floating point format

Col. 26-30 Index (integer) of X variable to be plotted against Y variable

Col. 31-40 Upper limit of X variable in floating point format

Col. 41-50 Lower limit of X variable in floating point format

Col. 51-60 Plotting interval, along the Y (vertical) axis, in floating point format

Repeat 6A type card for the number of maps desired (number punched on card 5A)

Factor analysis option card (right justify all values)
Required if parameter card 2 col. 30 option is 1.

CARD 5

Col. 1-5 FACTORS. Number of factors (integer) to be extracted (number of eigenvalues to be found). This number must be less than or equal to the number of variables.

Col. 7-10 DIAGONAL. Leave blank or punch zeros if the diagonal elements of the matrix are to be assumed equal to 1.0. Punch 9999 if each diagonal element is to have the same value. This value then is punched on one diagonal card which follows this parameter card. Punch any other number if diagonal cards are supplied.

Col. 12-15 HISTORY. Leave blank or punch zeros if no history and statement records are desired. Punch 9999 to obtain history and statement records for debugging. Punch any other number to obtain history records only.

Col. 17-20 INPUT MATRIX. Leave blank or punch zeros if no printout of the input and residual matrices are desired. Punch 5555 if both are desired. Punch a number greater than 5555 if the printout of the residual matrix only is desired. Punch any number less than 5555 to obtain a

Table 2. - Examples of Parameter Card 2 for program input and options (right justify all parameters)

Operation	Total No. Variables Column 1-5	No. Variables Per Card 6-10	Correlation Punch 15	Title 16-23	FAN 30	VROT 35	COREL 40	PLOT* 41 42 43
A. Correlation only-plot original data, no punch; 9 data cards/sample.	43	5	0	CORRELTS	0	0	1	T F F
B. Correlation only-no plot, punch; 4 data cards/sample.	29	8	1	CORRELTS	0	0	1	F F F
C. Correlation plus Factor Analysis (FAN)-no correlation punch; plot original data and factor loadings; 4 data cards/sample.	16	4	0	CORFANTS	1	0	1	T T F
D. Correlation plus FAN-correlation punch; plot original factor loadings but not original data; 9 data cards/sample.	87	10	1	CORFANTS	1	0	1	F T F
E. Correlation plus FAN plus Varimax Rotation (VROT)-no correlation punch; plot rotated factor loadings; 1 data card/sample.	8	8	0	CORFANVR	1	1	1	F F T
F. Correlation plus FAN plus VROT-correlation punch; plot original data and rotated factor loadings; 6 data cards/sample.	32	6	1	CORFANVR	1	1	1	T T T
G. Q-Mode plus FAN-no plot; 10 data cards/sample.	100	10	0	QMODFAN	1	0	0	F F F
H. Q-Mode plus FAN plus VROT; plot original factor loadings; 2 data cards/sample.	14	7	0	QMODFANVT	1	1	0	F T F

Col. 22-25 print out of the input matrix only. PUNCH LOADINGS. Leave blank or punch zeros if no punched cards containing the factor loadings are desired. Punch any nonzero number to receive the punched cards.

Col. 27-30 MINIMUM VARIANCE. This option permits termination of factor extraction when the variance accounted for by the factor most recently extracted is less than a selected minimum variance. Leave blank or punch zeros to continue extracting factors as long as the variance for each factor is positive; or punch the minimum variance which is to terminate factor extraction. If this number is a decimal, punch the decimal point.

Diagonal cards option
As stated above if the diagonal elements are assumed to be 1.0, no diagonal cards are required. If each diagonal element is to have the same value a single diagonal card is required; place the value in the first 8 columns with format F8.5. Alternatively, if diagonal cards are supplied punch 8 diagonal values (from element (1,1) to element (8,8) etc.) per card in 8 digit fields covering columns 17-80. The fields have format F8.5.

Plotting of unrotated factor loadings option cards

Parameter cards for plotting unrotated factor loadings if card 2 col. 42 option is "T".

CARD 6B
Col. 1-5 Number of bivariate unrotated factor loading maps desired.

CARD 7B
Col. 1-5 Index (integer) of factor to be considered as Y axis.

Col. 6-10	Index (integer) of factor to be considered as X axis.	Col. 12-15	Number of original factors to be rotated (integer)
Repeat 7B type card for the number of maps desired (number punched on card 6B)		Plotting of rotated factor loadings option cards	
Varimax rotation option card (right justify all parameters)		Parameter cards for plotting rotated factor loadings if card 2 col. 43 option is "T".	
Required if parameter card 2 col. 35 option is 1.		CARD 7C	
CARD 6		Col. 1-5	Number of bivariate rotated factor loading maps desired.
Col. 1-5	PRINT ORIGINAL FACTOR MATRIX. Leave blank or punch zeros if no printout of the original factor matrix is desired. Punch a nonzero integer number to obtain a printout of the input matrix.	CARD 8C	
		Col. 1-5	Index (integer) of factor to be considered as Y axis
Col. 7-10	PUNCH ROTATED LOADINGS. Leave blank if the rotated factor loadings are not to be punched. Punch 0001 to re-	Col. 6-10	Index (integer) of factor to be considered as X axis
		Repeat 8C type card for the number of maps desired (number punched on card 7C).	

REFERENCES

- Chayes, F., 1966, Alkaline and subalkaline basalts: *Am. Jour. Sci.*, v. 264, no. 2, p. 128-145.
- Griffiths, J.C., 1966, A genetic model for the interpretive petrology of detrital sediments: *Jour. Geology* v. 74, no. 5, p. 655-672.
- Griffiths, J.C., and Ondrick, C.W., 1968, Sampling a geological population: *Kansas Geol. Survey, Computer Contr.* 30, 53 p.
- Imbrie, J., and Purdy, E.G., 1962, Classification of modern Bahamian carbonate sediments: *Am. Assoc. Petroleum Geologists Mem.* 1, p. 253-272.
- Kaiser, H.F., 1958, The varimax criterion for analytic rotation in factor analysis: *Psychometrika*, v. 23, no. 3, p. 187-200.
- Kuno, H., 1959, Origin of Cenozoic petrographic provenances of Japan and surrounding area: *Bull. Volcanology*, ser. 2, v. 20, p. 37-76.
- Poldervaart, A., 1964, Chemical definition of alkali basalts and tholeiites: *Geol. Soc. America Bull.*, v. 75, no. 3, p. 229-232.

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C *****MAIN 5
C *****CORFAN*****MAIN 10
C *****MAIN 15
C THIS PROGRAM REPRESENTS A COMPOSITE OF 4 LIBRARY COMPUTER PROGRAMSMAIN 20
C WRITTEN BY THE STAFF AT THE PENNSYLVANIA STATE UNIVERSITY COMPUTERMAIN 25
C CENTER COREL,QMOD,FAN AND VROT. THE PROGRAMS WERE LINKED TOGETHER MAIN 30
C AND REVISED BY C. W. ONDRICK AND G. S. SRIVASTAVA JANUARY 1969. MAIN 35
C DIMENSION SUM(100),VARS(100),SUMSQ(100),CP(5200),AVARS(100) MAIN 40
C DIMENSION FMT(20),ISUM(100),X(100,100),A(5500),FM(100,100) MAIN 45
C COMMON /TITLE/NO1,NO2, NUM, NVR, IREA, IPRI, IPUN MAIN 50
C COMMON /CORR1/ N1,M,L,K, IZERO, NPUN, ICD, IND, ICOR MAIN 55
C COMMON /CORR2/ FMT,NFMT MAIN 60
C COMMON /FACTR/NFAN,IVROP,FANPLT,VARPLT,ORJPLT MAIN 65
C COMMON /TLABL/TITLE(20) MAIN 70
C LOGICAL LCARD,ORJPLT,FANPLT,VARPLT MAIN 75
C IREA=5 MAIN 80
C IPRI=6 MAIN 85
C IPUN=43 MAIN 90
C JUM = 100 MAIN 91
C *****MAIN 95
C READ NUMBER OF PROBLEMS TO BE ANALYZED MAIN 100
C *****MAIN 105
C READ (IREA,5) NSET MAIN 110
C 5 FORMAT (I5) MAIN 115
C *****MAIN 120
C READ MASTER PARAMETER CARD MAIN 125
C *****MAIN 130
C 10 READ (IREA,45) N,NVR,NPUN,NO1,NO2,NFAN,IVROP,ICORQ,ORJPLT,FANPLT,VMAIN 135
C 1ARPLT MAIN 140
C 45 FORMAT (3I5,2A4,2X,3I5,3L1) MAIN 145
C MCP = ((N*(N-1))/2)+N MAIN 150
C K=0 MAIN 155
C DO 25 I=1,N MAIN 160
C SUM(I)=0. MAIN 165
C SUMSQ(I)=0. MAIN 170
C 25 VARS(I)=0. MAIN 175
C DO 30 I=1,MCP MAIN 180
C 30 CP(I)=0. MAIN 185
C NUM=0 MAIN 190
C IZERO=0 MAIN 195
C ILLK=1 MAIN 200
C *****MAIN 205
C READ FORMAT FOR INPUT DATA MAIN 210
C *****MAIN 215
C READ (IREA,50) FMT MAIN 220
C 50 FORMAT (20A4) MAIN 225
C READ (IREA,51) TTLE MAIN 230
C WRITE(IPRI,52) TTLE MAIN 235
C 51 FORMAT (20A4) MAIN 240
C 52 FORMAT(1H1,//////////////////////20X,20A4) MAIN 245
C *****MAIN 250
C READ RAW DATA MAIN 255
C *****MAIN 260
C 55 READ (IREA,FMT) (AVARS(I),I=1,NVR),LCARD MAIN 265
C CALL COREL(LCARD,ICORQ,ILLK,SUM,VARS,SUMSQ,CP,AVARS,ISUM,N,MCP,X,AMAIN 275
C 1,FM,JUM ) MAIN 280
C IF (LCARD) GO TO 60 MAIN 285
C GO TO 55 MAIN 290
C 60 NSET=NSET-1 MAIN 295
C IF (NSET.GT.0) GO TO 10 MAIN 300

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WRITE (IPRI,65)
65 FORMAT (1H0,23X,85H****YOUR REQUESTED COMPUTATION IS COMPLETE, ITS
1 BEEN NICE DOING BUSINESS WITH YOU****)
STOP
END
SUBROUTINE COREL(LCARD,ICORQ,ILLK,SUM,VAR,SUMSQ,CP,AVARS,ISUM,N,
1MCP,X,A,FM,JUM)
C *****CORRELATION*****CORL 15
C *****CORRELATION*****CORL 80
C *****CORRELATION*****CORL 25
DIMENSION SUM(JUM),VAR(S(JUM),SUMSQ(JUM),CP(MCP ),AVARS(JUM) CORL 30
DIMENSION FMT(20),ISUM(JUM),X(JUM,JUM),A(MCP ),FM(JUM,JUM) CORL 35
COMMON /TITLE/NO1,NO2, NUM, NVR,IREA,IPRI,IPUN CORL 40
COMMON /CORR1/ N1,M,L,K,IZERO,NPUN,ICD,IND,ICOR CORL 45
COMMON /CORR2/ FMT,NFMT CORL 50
COMMON /FACTR/NFAN,IVROP,FANPLT,VARPLT,ORJPLT CORL 55
LOGICAL LCARD,ORJPLT,FANPLT,VARPLT CORL 60
IF (NPUN-N) 5,5,25 CORL 65
5 IF (N-120) 10,10,15 CORL 70
10 IF (N-NVR) 15,35,35 CORL 75
15 WRITE (IPRI,20) CORL 80
20 FORMAT (1H1,58HREREAD THE WRITE UP, YOUR NUMBER OF VARIABLES IS INCORL 85
1CORRECT) CORL 90
GO TO 220 CORL 95
25 WRITE (IPRI,30) CORL 100
30 FORMAT (1H1,61HNO. OF VARIABLES TO BE PUNCHED EXCEEDS TOTAL NO. OFCORL 105
1 VARIABLES) CORL 110
GO TO 220 CORL 115
35 DO 55 I=1,NVR CORL 120
K=K+1 CORL 125
VAR(S(K)=AVARS(I) CORL 130
FM(ILLK,K)=VAR(S(K) CORL 135
X(K,ILLK)=VAR(S(K) CORL 140
IF (K-N) 55,60,55 CORL 145
55 CONTINUE CORL 150
IF (LCARD) GO TO 110 CORL 155
RETURN CORL 160
60 DO 70 K=1,N CORL 165
SUM(K)=SUM(K)+VAR(S(K) CORL 170
SUMSQ(K)=SUMSQ(K)+(VAR(S(K)*VAR(S(K)) CORL 175
70 CONTINUE CORL 180
K=0 CORL 185
DO 100 I=2,N CORL 190
L=I-1 CORL 195
DO 100 J=1,L CORL 200
K=K+1 CORL 205
100 CP(K)=CP(K)+(VAR(S(I)*VAR(S(J)) CORL 210
NUM=NUM+1 CORL 215
ILLK=ILLK+1 CORL 220
K=0 CORL 225
IF (LCARD) GO TO 110 CORL 230
RETURN CORL 235
110 IF(ORJPLT) GO TO 250 CORL 240
GO TO 111 CORL 245
250 READ(IREA,1000) NMAP CORL 250
1000 FORMAT(I5) CORL 255
1001 FORMAT(I5,2F10.0,I5,3F10.0) CORL 260
DO 251 MAP = 1,NMAP CORL 265
READ(IREA,1001) I1,XMAX,XMIN,I2,YMAX,YMIN,XINT CORL 270
WRITE(IPRI,9999) CORL 275

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9999 FORMAT(1H1) CORL 280
WRITE(IPRI,3005)I1,I2 CORL 285
3005 FORMAT(45X29HSCATTERGRAM OF ORIGINAL DATA,/,50X,8HVARIABLE,I4,2X, CORL 290
13HVS.,I4,/) CORL 295
251 CALL PLOT(FM,XMAX,XMIN,YMAX,YMIN,XINT,NUM,I1,I2,JUM) CORL 300
111 DO 131 I=1,ILLK CORL 305
DO 131 J=1,N CORL 310
131 FM(I,J) = 0. CORL 315
IF (ICORQ.EQ.0) GO TO 205 CORL 320
COUNT=NUM CORL 325
DO 145 I=1,N CORL 330
C ***** CORL 335
C CALCULATE MEANS VARS(I) AND VARIANCES SUMSQ(I) CORL 340
C ***** CORL 345
VARS(I)=SUM(I)/COUNT CORL 350
SUMSQ(I)=(SUMSQ(I)/(COUNT-1.))-(VARS(I)**2)*(COUNT/(COUNT-1.)) CORL 355
CONTINUE CORL 360
IF (SUMSQ(I)) 135,135,140 CORL 365
135 IZERO=IZERO+1 CORL 370
SUMSQ(I)=0. CORL 375
GO TO 145 CORL 380
140 SUMSQ(I)=SQRT(SUMSQ(I)) CORL 385
145 CONTINUE CORL 390
K=0 CORL 395
DO 175 I=2,N CORL 400
L=I-1 CORL 405
DO 175 J=1,L CORL 410
K=K+1 CORL 415
C ***** CORL 420
C CALCULATE CORRELATION COEFFICIENTS CP(K) CORL 425
C ***** CORL 430
CP(K)=(CP(K)-(VARS(I)*SUM(J)))/((COUNT-1.)*SUMSQ(I)*SUMSQ(J)) CORL 435
IF (CP(K).GT.999.99)CP(K)=999.99 CORL 440
175 CONTINUE CORL 445
NI=N-1 CORL 450
ISUM(1)=1 CORL 455
DO 195 L=1,NI CORL 460
195 ISUM(L+1)=ISUM(L)+1 CORL 465
CALL COR1(SUM,VAR,SUMSQ,CP,AVARS,ISUM,N,MCP,JUM) CORL 470
IF (NFAN.EQ.1) GO TO 210 CORL 475
RETURN CORL 480
205 CALL QMOD (SUM,VAR,SUMSQ,CP,AVARS,ISUM,N,MCP,X,NN,JUM,JSAMP) CORL 485
NUM=JSAMP CORL 490
GO TO 212 CORL 495
C ***** CORL 500
C READ PARAMETER CARD FOR FACTOR ANALYSIS CORL 505
C ***** CORL 510
210 NN=N CORL 515
212 READ (IREA,215) J,IDIAG,IHSTY,IMTRX,IVMX,AB CORL 520
215 FORMAT (5I5,F5.0) CORL 525
CALL FAN(J,IDIAG,IHSTY,IMTRX,IVMX,AB,SUM,VAR,SUMSQ,CP,AVARS, CORL 530
1ISUM,NN,MCP,A,FM,JUM) CORL 535
GO TO 230 CORL 540
220 WRITE (IPRI,225) CORL 545
225 FORMAT (5X,38HWHOOOPS....WRONG DATA CHECK AGAIN,CLOD) CORL 550
STOP CORL 555
230 RETURN CORL 560
END CORL 565
SUBROUTINE COR1(SUM,VAR,SUMSQ,CP,AVARS,ISUM,N,MCP,JUM) CORL 5
C ***** CORL 10

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PRINTS THE LOWER HALF OF THE SYMMETRIC CORRELATION MATRIX, MEANS	COR1	15
AND STANDARD DEVIATIONS.	COR1	20
*****	COR1	25
DIMENSION SUM(JUM), VARS(JUM), SUMSQ(JUM), CP(MCP), AVARS(JUM)	COR1	30
DIMENSION FMT(20), ISUM(JUM)	COR1	35
COMMON /TITLE/NO1,NO2, NUM, NVR, IREA, IPRI, IPUN	COR1	40
COMMON /CORR1/ N1, M, L, K, IZERO, NPUN, ICD, IND, ICOR	COR1	45
COMMON /CORR2/ FMT, NFMT	COR1	50
COMMON /FACTR/NFAN, IVROP, FANPLT, VARPLT, ORJPLT	COR1	55
LOGICAL LCARD, ORJPLT, FANPLT, VARPLT	COR1	60
WRITE (IPRI,885)	COR1	65
WRITE (IPRI,890) NUM,NO1,NO2	COR1	70
IF (N-15) 20,20,55	COR1	75
20 WRITE (IPRI,870) (ISUM(I),I=1,N1)	COR1	80
M=1	COR1	85
DO 45 I=2,N	COR1	90
M=M+(I-2)	COR1	95
L=M+(I-2)	COR1	100
45 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1	105
GO TO 660	COR1	110
55 WRITE (IPRI,870) (ISUM(I),I=1,15)	COR1	115
M=1	COR1	120
DO 80 I=2,16	COR1	125
M=M+(I-2)	COR1	130
L=M+(I-2)	COR1	135
80 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1	140
IF (N-16) 660,660,90	COR1	145
90 DO 105 I=17,N	COR1	150
M=M+(I-2)	COR1	155
L=M+14	COR1	160
105 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1	165
IF (N-60) 125,120,115	COR1	170
115 IF (N-62) 120,120,125	COR1	175
120 WRITE (IPRI,940)	COR1	180
125 IF (N-30) 130,130,165	COR1	185
130 WRITE (IPRI,880) (ISUM(I),I=16,N1)	COR1	190
M=106+15	COR1	195
DO 155 I=17,N	COR1	200
M=M+(I-2)	COR1	205
L=M+I-17	COR1	210
155 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1	215
GO TO 660	COR1	220
165 WRITE (IPRI,880) (ISUM(I),I=16,30)	COR1	225
M=106+15	COR1	230
DO 190 I=17,31	COR1	235
M=M+(I-2)	COR1	240
L=M+I-17	COR1	245
190 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1	250
IF (N-31) 660,660,200	COR1	255
200 DO 215 I=32,N	COR1	260
M=M+(I-2)	COR1	265
L=M+14	COR1	270
215 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1	275
IF (N-79) 235,230,225	COR1	280
225 IF (N-81) 230,230,235	COR1	285
230 WRITE (IPRI,940)	COR1	290
235 IF (N-45) 240,240,275	COR1	295
240 WRITE (IPRI,880) (ISUM(I),I=31,N1)	COR1	300
M=436+30	COR1	305
DO 265 I=32,N	COR1	310

M=M+(I-2)	COR1 315
L=M+I-32	COR1 320
265 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 325
GO TO 660	COR1 330
275 WRITE (IPRI,880) (ISUM(I),I=31,45)	COR1 335
M=436+30	COR1 340
DO 300 I=32,46	COR1 345
M=M+(I-2)	COR1 350
L=M+I-32	COR1 355
300 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 360
IF (N-46) 660,660,310	COR1 365
310 DO 325 I=47,N	COR1 370
M=M+(I-2)	COR1 375
L=M+14	COR1 380
325 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 385
IF (N-94) 345,340,335	COR1 390
335 IF (N-96) 340,340,345	COR1 395
340 WRITE (IPRI,940)	COR1 400
345 IF (N-60) 350,350,385	COR1 405
350 WRITE (IPRI,880) (ISUM(I),I=46,N1)	COR1 410
M=991+45	COR1 415
DO 375 I=47,N	COR1 420
M=M+I-2	COR1 425
L=M+I-47	COR1 430
375 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 435
GO TO 660	COR1 440
385 WRITE (IPRI,880) (ISUM(I),I=46,60)	COR1 445
M=991+45	COR1 450
DO 410 I=47,61	COR1 455
M=M+I-2	COR1 460
L=M+I-47	COR1 465
410 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 470
IF (N-61) 660,660,420	COR1 475
420 DO 435 I=62,N	COR1 480
M=M+I-2	COR1 485
L=M+14	COR1 490
435 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 495
IF (N-75) 445,445,480	COR1 500
445 WRITE (IPRI,880) (ISUM(I),I=61,N1)	COR1 505
M=1771+60	COR1 510
DO 470 I=62,N	COR1 515
M=M+I-2	COR1 520
L=M+I-62	COR1 525
470 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 530
GO TO 660	COR1 535
480 WRITE (IPRI,880) (ISUM(I),I=61,75)	COR1 540
M=1771+60	COR1 545
DO 505 I=62,76	COR1 550
M=M+I-2	COR1 555
L=M+I-62	COR1 560
505 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 565
IF (N-76) 660,660,515	COR1 570
515 DO 530 I=77,N	COR1 575
M=M+I-2	COR1 580
L=M+14	COR1 585
530 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 590
IF (N-90) 540,540,575	COR1 595
540 WRITE (IPRI,880) (ISUM(I),I=76,N1)	COR1 600
M=2776+75	COR1 605
DO 565 I=77,N	COR1 610

M=M+I-2	COR1 615
L=M+I-77	COR1 620
565 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 625
GO TO 660	COR1 630
575 WRITE (IPRI,880) (ISUM(I),I=76,90)	COR1 635
M=2776+75	COR1 640
DO 600 I=77,91	COR1 645
M=M+I-2	COR1 650
L=M+I-77	COR1 655
600 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 660
IF (N-91) 660,660,610	COR1 665
610 DO 625 I=92,N	COR1 670
M=M+I-2	COR1 675
L=M+14	COR1 680
625 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 685
IF(N-105)631,631,632	COR1 690
631 WRITE (IPRI,880) (ISUM(I),I=91,N1)	COR1 695
M=4006+90	COR1 700
DO 655 I=92,N	COR1 705
M=M+I-2	COR1 710
L=M+I-92	COR1 715
655 WRITE (IPRI,875) I,(CP(K),K=M,L)	COR1 720
GO TO 660	COR1 725
632 WRITE(IPRI,880)(ISUM(I),I=91,105)	COR1 730
M=4006+90	COR1 735
DO 633 I=92,106	COR1 740
M=M+I-2	COR1 745
L=M+I-92	COR1 750
633 WRITE(IPRI,875)I,(CP(K),K=M,L)	COR1 755
IF(N-106)660,660,634	COR1 760
634 DO 636 I=107,N	COR1 765
M=M+I-2	COR1 770
L=M+14	COR1 775
636 WRITE(IPRI,875) I,(CP(K),K=M,L)	COR1 780
IF(N-120)637,637,639	COR1 785
637 WRITE(IPRI,880)(ISUM(I),I=106,N1)	COR1 790
M=4226+105	COR1 795
DO 638 I=107,N	COR1 800
M=M+I-2	COR1 805
L=M+I-77	COR1 810
638 WRITE(IPRI,875)I,(CP(K),K=M,L)	COR1 815
GO TO 660	COR1 820
639 WRITE(IPRI,880)(ISUM(I),I=106,120)	COR1 825
660 IF (IZERO) 665,670,665	COR1 830
665 WRITE (IPRI,930) IZERO	COR1 835
GO TO 670	COR1 840
670 WRITE (IPRI,910) NO1,NO2	COR1 845
WRITE (IPRI,925)	COR1 850
M=1	COR1 855
L=10	COR1 860
690 IF (L-N) 695,710,710	COR1 865
695 WRITE (IPRI,915) M,L,(VARS(K),K=M,L)	COR1 870
M=M+10	COR1 875
L=L+10	COR1 880
GO TO 690	COR1 885
710 WRITE (IPRI,915) M,N,(VARS(K),K=M,N)	COR1 890
WRITE (IPRI,920)	COR1 895
WRITE (IPRI,925)	COR1 900
M=1	COR1 905
L=10	COR1 910


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730 IF (L-N) 735,755,755 COR1 915
735 WRITE (IPRI,915) M,L,(SUMSQ(K),K=M,L) COR1 920
      M=M+10 COR1 925
      L=L+10 COR1 930
      GO TO 730 COR1 935
755 WRITE (IPRI,915) M,N,(SUMSQ(K),K=M,N) COR1 940
      IF (NPUN) 860,860,765 COR1 945
765 ICD=(NPUN+5)/6 COR1 950
      M=1 COR1 955
      DO 785 I=1,ICD COR1 960
      L=M+5 COR1 965
      WRITE (IPUN,895) NO1,NO2,I,(VARS(K),K=M,L) COR1 970
785 M=M+6 COR1 975
      M=1 COR1 980
      DO 805 I=1,ICD COR1 985
      L=M+5 COR1 990
      WRITE (IPUN,900) NO1,NO2,I,(SUMSQ(K),K=M,L) COR1 995
805 M=M+6 COR11000
      IND=1 COR11005
      DO 820 I=2,NPUN COR11010
820 IND=IND+(I-2) COR11015
      IND=IND+NPUN-2 COR11020
      ICOR=(IND+7)/8 COR11025
      M=1 COR11030
      DO 850 I=1,ICOR COR11035
      L=M+7 COR11040
      WRITE (IPUN,905) NO1,NO2,I,(CP(K),K=M,L) COR11045
850 M=M+8 COR11050
      WRITE (IPUN,935) NO1,NO2,NUM,NPUN COR11055
860 WRITE (IPRI,865) NO1,NO2 COR11060
865 FORMAT (1H0,25HSTATISTICS COMPLETED FOR ,2A4/) COR11065
870 FORMAT (1H0,3(4X,5I7)) COR11070
875 FORMAT (1H ,I3,2X,5F7.3,2(4X,5F7.3)) COR11075
880 FORMAT (1H1,3(4X,5I7)) COR11080
885 FORMAT (1H1,45X,28HSYMMETRIC CORRELATION MATRIX) COR11085
890 FORMAT (1H0,34X,12HNUMBER CASES,I7,10X,14HPROBLEM NAME ,2A4) COR11090
895 FORMAT (2A4,9H MEAN CD,I3,6F10.3) COR11095
900 FORMAT (2A4,9HST DEV CD,I3,6F10.3) COR11100
905 FORMAT (2A4,5H COR ,I3,8F8.5) COR11105
910 FORMAT (1H1,15X,5HMEANS,6X,2A4) COR11110
915 FORMAT (1H ,I3,4H TO ,I3,3X,10F10.3) COR11115
920 FORMAT (1H0,15X,19HSTANDARD DEVIATIONS) COR11120
925 FORMAT (11H VARIABLES) COR11125
930 FORMAT (1H0,I3,2X,81HVARIABLES HAVE ZERO VARIANCE. CORRELATIONS WHC COR11130
      ICH INCLUDE THEM ARE PRINTED *00.000) COR11135
935 FORMAT (2A4,2X,7HNO.OBS.,I7,6X,5HVAR.S.,I5) COR11140
940 FORMAT (1H1) COR11145
      RETURN COR11150
      END COR11155
SUBROUTINE QMOD(SUM,VARS,SUMSQ,COS,AVARS,ISUM,N,MCP,X,NN,JUM, JS)QMOD 5
C *****QMOD 10
C *****Q-MODE COSINE*****QMOD 15
C *****QMOD 20
DIMENSION SUM(JUM),VARS(JUM),SUMSQ(JUM),COS(MCP ),AVARS(JUM) QMOD 25
DIMENSION XMAX(120),SQ(120),X(JUM,JUM) QMOD 30
COMMON /TITLE/NO1,NO2, ISAMP, NVR,IREA,IPRI,IPUN QMOD 35
COMMON /FACTR/NFAN,IVROP,FANPLT,VARPLT,ORJPLT QMOD 40
LOGICAL LCARD,ORJPLT,FANPLT,VARPLT QMOD 45
C *****QMOD 50
C THE ORIGINAL INPUT DATA ENTERS THIS SUBROUTINE AS X(I,J). QMOD 55
C *****QMOD 60

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	IVAR = N	QMOD 65
	IF (IVAR) 5,110,5	QMOD 70
	5 NTOT=ISAMP*(ISAMP-1)/2	QMOD 75
C	*****	QMOD 80
C	PRINT INPUT MATRIX	QMOD 85
C	*****	QMOD 90
	WRITE (IPRI,10)	QMOD 95
10	FORMAT (1H1)	QMOD 100
	WRITE (IPRI,15) NO1,NO2	QMOD 105
15	FORMAT (1H ,55X,13HPROBLEM NAME ,2A4//)	QMOD 110
	IF(IVAR.LT.13)GO TO 21	QMOD 115
	DO 20 J=1,ISAMP	QMOD 120
	WRITE (IPRI,25) J,(X(I,J),I=1,13)	QMOD 125
	IF(IVAR.EQ.13)GO TO 31	QMOD 130
20	WRITE (IPRI,30) (X(I,J),I=14,IVAR)	QMOD 135
	GO TO 31	QMOD 140
21	DO 22 J=1,ISAMP	QMOD 145
22	WRITE(IPRI,25)J,(X(I,J),I=1,IVAR)	QMOD 150
25	FORMAT (1H ,3HIN ,13,13F9.4)	QMOD 155
30	FORMAT (1H ,3HIN ,3X,13F9.4)	QMOD 160
C	*****	QMOD 165
C	ZERO XMAX AREA	QMOD 170
C	*****	QMOD 175
31	DO 35 I=1,IVAR	QMOD 180
35	XMAX(I)=0.0	QMOD 185
C	*****	QMOD 190
C	FIND MAXIMUM FOR EACH VARIABLE	QMOD 195
C	*****	QMOD 200
	DO 45 I=1,IVAR	QMOD 205
	DO 45 J=1,ISAMP	QMOD 210
	IF (XMAX(I)-X(I,J)) 40,40,45	QMOD 215
40	XMAX(I)=X(I,J)	QMOD 220
45	CONTINUE	QMOD 225
C	*****	QMOD 230
C	DIVIDE ORIGINAL VALUES BY XMAX	QMOD 235
C	*****	QMOD 240
	DO 50 I=1,IVAR	QMOD 245
	DO 50 J=1,ISAMP	QMOD 250
50	X(I,J)=X(I,J)/XMAX(I)	QMOD 255
C	*****	QMOD 260
C	PRINT MATRIX OF DIVIDED VALUES	QMOD 265
C	*****	QMOD 270
	WRITE (IPRI,10)	QMOD 275
	WRITE (IPRI,15) NO1,NO2	QMOD 280
	DO 55 J=1,ISAMP	QMOD 285
	WRITE (IPRI,60) J,(X(I,J),I=1,13)	QMOD 290
55	WRITE (IPRI,65) (X(I,J),I=14,IVAR)	QMOD 295
60	FORMAT (1H ,3HDIV,I3,13F9.5)	QMOD 300
65	FORMAT (1H ,3HDIV,3X,13F9.5)	QMOD 305
C	*****	QMOD 310
C	ZERO SUMS OF SQUARES	QMOD 315
C	*****	QMOD 320
	DO 70 I=1,ISAMP	QMOD 325
70	SQ(I)=0.0	QMOD 330
C	*****	QMOD 335
C	*****	QMOD 340
C	ZERO COS AREA	QMOD 345
C	*****	QMOD 350
	DO 75 I=1,MCP	QMOD 355
75	COS(I)=0.0	QMOD 360

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C *****QMOD 365
C COMPUTE SUMS OF SQUARES QMOD 370
C *****QMOD 375
DO 80 J=1,ISAMP QMOD 380
DO 80 I=1,IVAR QMOD 385
80 SQ(J)=SQ(J)+X(I,J)**2 QMOD 390
C *****QMOD 395
C COMPUTE COSINES OF THETA QMOD 400
C *****QMOD 405
K=0 QMOD 410
DO 90 II=2,ISAMP QMOD 415
JJMAX=II-1 QMOD 420
DO 90 JJ=1,JJMAX QMOD 425
BUM=0.0 QMOD 430
DO 85 I=1,IVAR QMOD 435
85 BUM=BUM+X(I,JJ)*X(I,II) QMOD 440
K=K+1 QMOD 445
90 COS(K)=BUM/SQRT(SQ(II)*SQ(JJ)) QMOD 450
C *****QMOD 455
C PRINT COSINE MATRIX QMOD 460
C *****QMOD 465
WRITE (IPRI,10) QMOD 470
ICARD=1 QMOD 475
J=1 QMOD 480
JBEG=1 QMOD 485
JEND=8 QMOD 490
95 WRITE (IPRI,100) ICARD,(COS(J),J=JBEG,JEND) QMOD 495
100 FORMAT (6HOCOS ,I3,10F10.5) QMOD 500
IF (JEND-NTOT) 105,110,110 QMOD 505
105 J=J+1 QMOD 510
JBEG=JBEG+8 QMOD 515
JEND=JEND+8 QMOD 520
ICARD=ICARD+1 QMOD 525
GO TO 95 QMOD 530
110 NOLL=N QMOD 535
NN =ISAMP QMOD 540
JS = NOLL QMOD 545
RETURN QMOD 550
END QMOD 555
SUBROUTINE FAN(M,IDIAG,IHSTY,IMTRX,IVMX,AB,SUM,VAR,SUMSQ,CP,AVARSFAN 5
I,ISUM,N,MCP,A,FM,JUM) FAN 10
C *****FAN 15
C *****FACTOR ANALYSIS*****FAN 20
C *****FAN 25
DIMENSION A(MCP ),X(120),Y(120),Z(120),CP(MCP ) FAN 30
DIMENSION VARS(JUM),AVARS(JUM),ISUM(JUM),FM(JUM,JUM) FAN 35
COMMON /TITLE/NO1,NO2, NUM, NVR,IREA,IPRI,IPUN FAN 40
COMMON /FACTR/NFAN,IVROP,FANPLT,VARPLT,ORJPLT FAN 45
LOGICAL LCARD,ORJPLT,FANPLT,VARPLT FAN 50
COMMON /TLABL/TITLE(20) FAN 55
JOT=1 FAN 60
WRITE (IPRI,10) FAN 65
10 FORMAT (1H1,/////////51X,29HPRINCIPAL COMPONENTS ANALYSIS//) FAN 70
WRITE (IPRI,15)TILE FAN 75
15 FORMAT (1H ,25X,20A4//) FAN 80
WRITE (IPRI,25) NO1,NO2,N,M FAN 85
25 FORMAT (1H ,36X,12HPROBLEM NAME,2X,2A4,10X,I3,12H VARIABLES , ,I3,8FAN 90
1H FACTORS//) FAN 95
IABC=AB FAN 100
ABC=AB FAN 105

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IF (N) 1140,1140,45 FAN 110
45 IF (N-120) 50,50,1150 FAN 115
50 IF (M) 1160,1160,55 FAN 120
55 IF (M-120) 60,60,1170 FAN 125
60 IF (N-M) 1180,65,65 FAN 130
65 IF (IABC-N) 70,70,1200 FAN 135
70 IF (IDIAG) 80,150,75 FAN 140
75 IF (IDIAG-9999) 80,150,80 FAN 145
C *****FAN 150
C READ DIAGONAL CARDS (OPTIONAL) FAN 155
C *****FAN 160
80 NCARD=((N+7)/8)-1 FAN 165
MI=1 FAN 170
IF (NCARD) 115,115,95 FAN 175
95 DO 110 I=1,NCARD FAN 180
L=MI+7 FAN 185
READ (IREA,130) (X(K),K=MI,L) FAN 190
110 MI=MI+8 FAN 195
115 IREM=N-(8*NCARD) FAN 200
L=MI+IREM-1 FAN 205
READ (IREA,130) (X(K),K=MI,L) FAN 210
130 FORMAT (16X,8F8.5) FAN 215
K=(I*(I-1)/2)+I FAN 220
DO 145 I=1,N FAN 225
145 A(K)=X(I) FAN 230
C *****FAN 235
C START OF CALCULATION FAN 240
C *****FAN 245
150 CONTINUE FAN 250
NVOTQ=N*(N-1)/2 FAN 255
I=2 FAN 260
J=1 FAN 265
DO 170 IN=1,NVOTQ FAN 270
K=(I*(I-1)/2)+J FAN 275
A(K)=CP(IN) FAN 280
IF (I-J-1) 155,155,165 FAN 285
155 I=I+1 FAN 290
IF (NVOTQ-I) 185,160,160 FAN 295
160 J=1 FAN 300
GO TO 170 FAN 305
165 J=J+1 FAN 310
170 CONTINUE FAN 315
C *****FAN 320
C PUT A SINGLE NUMBER ON THE DIAGONAL (OPTIONAL) FAN 325
C *****FAN 330
IF (IDIAG.EQ.0) GO TO 185 FAN 335
IF (IDIAG.LT.9999) GO TO 205 FAN 340
READ (IREA,180) X(1) FAN 345
180 FORMAT (F8.5) FAN 350
GO TO 190 FAN 355
185 X(1)=1.0 FAN 360
190 DO 200 I=1,N FAN 365
K=(I*(I-1)/2)+I FAN 370
200 A(K)=X(1) FAN 375
205 IF (IMTRX-5555) 210,215,235 FAN 380
210 IF (IMTRX) 215,235,215 FAN 385
215 KEY=0 FAN 390
WRITE (IPRI,225) N,N FAN 395
225 FORMAT (1H1,27X,69HSYMMETRIC (CORRELATION) MATRIX -LOWER HALF -ELEFAN 400
1MENT(1,1) TO ELEMENT (,I3,1H,,I3,1H)/) FAN 405

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	GO TO 965	FAN	410
235	B=N	FAN	415
	C=M	FAN	420
	TOL3G=5.E-6	FAN	425
	SWI=1.000	FAN	430
	FACT=1.000	FAN	435
	DO 265 I=1,N	FAN	440
265	Z(I)=1.000/B	FAN	445
C	*****	FAN	450
C	RETURN TO 9999 TO EXTRACT NEXT FACTOR	FAN	455
C	*****	FAN	460
270	YSUM=1.000	FAN	465
	DIFFY=0.000	FAN	470
	DIFFS=0.000	FAN	475
	RATS=0.000	FAN	480
	RATSD=0.000	FAN	485
	TOL3=0.000	FAN	490
	VITER=0.000	FAN	495
	DO 310 I=1,N	FAN	500
	XXXX=I	FAN	505
310	X(I)=Z(I)+2.E-6*XXXX	FAN	510
C	*****	FAN	515
C	RETURN TO 2222 TO PERFORM AN ITERATION	FAN	520
C	*****	FAN	525
315	SUM=0.000	FAN	530
	DO 325 I=1,N	FAN	535
325	Y(I)=0.000	FAN	540
C	*****	FAN	545
C	MULTIPLY MATRICES Y=A*X	FAN	550
C	*****	FAN	555
	DO 355 I=1,N	FAN	560
	K0=(I*(I-1))/2	FAN	565
	DO 350 J=1,I	FAN	570
	K=K0+J	FAN	575
350	Y(I)=A(K)*X(J)+Y(I)	FAN	580
355	CONTINUE	FAN	585
	L=N-1	FAN	590
	DO 390 I=1,L	FAN	595
	K=I+1	FAN	600
	DO 385 J=K,N	FAN	605
	K0T=(J*(J-1))/2+I	FAN	610
385	Y(I)=A(K0T)*X(J)+Y(I)	FAN	615
390	CONTINUE	FAN	620
	DO 400 I=1,N	FAN	625
400	SUM=SUM+ABS(Y(I))	FAN	630
C	*****	FAN	635
C	RETURN TO 3333 AFTER AN EXTRAPOLATION	FAN	640
C	*****	FAN	645
405	DIFS9=0.000	FAN	650
	DO 415 I=1,N	FAN	655
415	Y(I)=Y(I)/SUM	FAN	660
	DO 425 I=1,N	FAN	665
425	DIFS9=DIFS9+ABS(Y(I)-X(I))	FAN	670
	DIFFY=SUM-YSUM	FAN	675
	YSUM=SUM	FAN	680
	IF(DIFFS.EQ.0.)GO TO 426	FAN	685
	V5FG=DIFS9/DIFFS	FAN	690
426	IF (V5FG.GT.99999.9)V5FG=0.000	FAN	695
	RATSD=V5FG-RATS	FAN	700
	RATS=V5FG	FAN	705

	DIFFS=DIFS9	FAN	710
	DIFS9=1.000-V5FG	FAN	715
	VITER=VITER+1.000	FAN	720
	TOL3=(VITER*VITER)*DIFS9*TOL3G	FAN	725
C	*****	FAN	730
C	PRINT HISTORY RECORD (OPTIONAL)	FAN	735
C	*****	FAN	740
	IF (IHSTY) 480,525,480	FAN	745
480	IF (VITER-1.000) 515,485,515	FAN	750
485	WRITE (IPRI,490)	FAN	755
490	FORMAT (1H1, //4X, 13HHISTORY CARDS/)	FAN	760
	WRITE (IPRI,500)	FAN	765
500	FORMAT (1H ,9HFACT ITER,9X,4HYSUM,14X,5HDIFFY,13X,5HDIFFS,15X,4HRA	FAN	770
	ITS,12X,5HRATSD,11X,4HTOL3)	FAN	775
	WRITE (IPRI,510)	FAN	780
510	FORMAT (1H ,49X,20H(CHECKS CONVERGENCE))	FAN	785
515	WRITE (IPRI,520) FACT,VITER,YSUM,DIFFY,DIFFS,RATS,RATSD,TOL3	FAN	790
520	FORMAT (1H ,2F4.0,4X,3E18.8,4X,3E16.8)	FAN	795
C	*****	FAN	800
C	TESTS FOR CONVERGENCE	FAN	805
C	*****	FAN	810
525	DIFS9=FACT	FAN	815
	IF (VITER*FACT*.2E-8-ABS(DIFFS)) 535,680,680	FAN	820
535	IF (2.E-7-ABS(DIFFS-2.000)-ABS(DIFFY)-ABS(RATS-1.000)) 540,665,66	FAN	825
	15	FAN	830
540	IF (-ABS(RATSD)) 545,1105,545	FAN	835
545	IF (-ABS(RATSD)+TOL3) 555,550,550	FAN	840
550	IF (-ABS(RATSD)+ABS(RATS)) 600,1105,600	FAN	845
555	IF (TOL3) 560,1105,1105	FAN	850
560	IF (1.E-2-ABS(RATSD)) 1105,565,565	FAN	855
565	IF (ABS(DIFFS)-1.E-3) 1105,575,570	FAN	860
570	IF (ABS(DIFFS)-1.000) 575,1105,1105	FAN	865
C	*****	FAN	870
C	ENTER EXTRAPOLATION ROUTINE-TYPE 1	FAN	875
C	*****	FAN	880
575	V5FG=1.000	FAN	885
	IF (IHSTY-9999) 595,585,595	FAN	890
585	WRITE (IPRI,590) VITER	FAN	895
590	FORMAT (1H ,13HSTATEMENT 490,F5.0)	FAN	900
595	SWI=0.000	FAN	905
C	*****	FAN	910
C	ENTER EXTRAPOLATION ROUTINE-TYPE 2	FAN	915
C	*****	FAN	920
600	SUM=0.000	FAN	925
	DO 635 I=1,N	FAN	930
	Y(I)=-V5FG*X(I)+Y(I)	FAN	935
	IF (Y(I)-10.000) 620,1190,1190	FAN	940
620	DIFS9=Y(I)	FAN	945
	IF (SWI) 630,635,630	FAN	950
630	Z(I)=Y(I)-X(I)	FAN	955
635	SUM=SUM+ABS(DIFS9)	FAN	960
	IF (IHSTY-9999) 655,645,655	FAN	965
645	WRITE (IPRI,650) VITER	FAN	970
650	FORMAT (1H ,14HSTATEMENT 5555,F5.0)	FAN	975
655	SWI=0.000	FAN	980
	GO TO 405	FAN	985
C	*****	FAN	990
C	ARRIVE AT 6666 IF A FACTOR HAS BEEN EXTRACTED	FAN	995
C	*****	FAN	1000
665	WRITE (IPRI,670)	FAN	1005

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670 FORMAT (1H1,60HNEGATIVE ROOT ENCOUNTERED. FACTOR LOADINGS ARE IMAFAN 1010
    IGINARY. ) FAN 1015
    SUM=-SUM FAN 1020
680 SS=0.000 FAN 1025
    IF (IHSTY-9999) 700,690,700 FAN 1030
690 WRITE (IPRI,695) VITER FAN 1035
695 FORMAT (1H ,14HSTATEMENT 6666,F5.0) FAN 1040
700 DO 705 I=1,N FAN 1045
705 SS=SS+(Y(I)*Y(I)) FAN 1050
    ANORM=SQRT(SS) FAN 1055
    DEFLG=SUM/SS FAN 1060
    IF (DEFLG.GT.99999.9)PCHFG=0.000 FAN 1065
    IF (SUM) 735,725,725 FAN 1070
725 PCHFG=SQRT(DEFLG) FAN 1075
    GO TO 740 FAN 1080
735 PCHFG=0.000 FAN 1085
740 S1828=1.000 FAN 1090
C ***** FAN 1095
C PRINT THE RESULTS FAN 1100
C ***** FAN 1105
    WRITE (IPRI,750) FAN 1110
750 FORMAT (1H1, //24X,6HFACTOR,5X,4HTEST,6X,6HFACTOR,7X,8HVARIANCE,7X,FAN 1115
    I11HEIGENVECTOR,5X,10HITERATIONS) FAN 1120
    WRITE (IPRI,760) FAN 1125
760 FORMAT (1H ,23X,6HNUMBER,4X,6HNUMBER,5X,7HLOADING,4X,12H(EIGENVALU FAN 1130
    IE),21X,8HREQUIRED) FAN 1135
    DO 770 IMAX=1,N FAN 1140
770 X(IMAX)=0.000 FAN 1145
    DO 840 I=1,N FAN 1150
    S1830=Y(I)/ANORM FAN 1155
    S1829=PCHFG*Y(I) FAN 1160
    IFACT=FACT FAN 1165
    I1828=S1828 FAN 1170
    ITER=VITER FAN 1175
    IF (I1828-1) 820,805,820 FAN 1180
805 WRITE (IPRI,810) IFACT,I1828,S1829,SUM,S1830,ITER FAN 1185
810 FORMAT (1H ,23X,I4,I10,2F14.5,F16.5,I13) FAN 1190
    GO TO 830 FAN 1195
820 WRITE (IPRI,825) I1828,S1829,S1830 FAN 1200
825 FORMAT (1H ,27X,I10,F14.5,14X,F16.5) FAN 1205
830 S1828=S1828+1.000 FAN 1210
    X(I)=S1829 FAN 1215
    FM(I,JOT)=X(I) FAN 1220
840 CONTINUE FAN 1225
    JOT=JOT+1 FAN 1230
    IF (SUM) 875,850,850 FAN 1235
850 IF (IVMX) 855,875,855 FAN 1240
C ***** FAN 1245
C PUNCH FACTOR LOADING CARDS FOR VARIMAX ROTATION (OPTIONAL) FAN 1250
C ***** FAN 1255
855 ICOR=(N-1)/6+1 FAN 1260
    IVM=1 FAN 1265
    DO 865 JIM=1,ICOR FAN 1270
    IEND=IVM+5 FAN 1275
    WRITE (IPUN,870) NO1,NO2,IFACT,JIM,(X(IW),IW=IVM,IEND) FAN 1280
865 IVM=IVM+6 FAN 1285
870 FORMAT (2A4,1X,3HFCT,I3,2HCD,I3,6F10.5) FAN 1290
C ***** FAN 1295
C TEST IF LAST FACTOR OR MINIMUM VARIANCE HAS BEEN REACHED. FAN 1300
C ***** FAN 1305

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875	IF (FACT-C)	880,885,880	FAN	1310
880	IF (SUM-ABC)	885,895,895	FAN	1315
885	KING=1		FAN	1320
	GO TO 910		FAN	1325
895	SWI=FACT+1.000		FAN	1330
	FACT=SWI		FAN	1335
	KING=0		FAN	1340
C	*****		FAN	1345
C	DEFLATION SUBROUTINE		FAN	1350
C	*****		FAN	1355
910	DO 935 I=1,N		FAN	1360
	LUM=(I*(I-1)/2)		FAN	1365
	DO 935 J=1,I		FAN	1370
	K=LUM+J		FAN	1375
	A(K)=(-Y(I)*Y(J)*DEFLG)+A(K)		FAN	1380
935	CONTINUE		FAN	1385
C	*****		FAN	1390
C	TEST TO SEE IF CURRENT PROBLEM IS FINISHED		FAN	1395
C	*****		FAN	1400
	IF (KING-1)	270,945,270	FAN	1405
945	IF (IMTRX-5555)	1135,950,950	FAN	1410
950	WRITE (IPRI,955) N,N		FAN	1415
955	FORMAT (1H1,27X,28HPRINT OUT OF RESIDUAL MATRIX,2X,38H-LOWER HALF		FAN	1420
	1-ELEMENT(1,1) TO ELEMENT (,I3,1H,,I3,1H)/)		FAN	1425
	KEY=1		FAN	1430
C	*****		FAN	1435
C	PRINT INPUT AND/OR RESIDUAL MATRICES (BOTH OPTIONAL)		FAN	1440
C	*****		FAN	1445
965	DO 970 L=1,N		FAN	1450
970	ISUM(L)=L		FAN	1455
	JAS=1		FAN	1460
	KOR=15		FAN	1465
	MASS=1		FAN	1470
	IF (N-KOR)	995,995,1040	FAN	1475
995	WRITE (IPRI,1000) (ISUM(I),I=JAS,N)		FAN	1480
1000	FORMAT (1H ,1X,5(2X,3I7))		FAN	1485
	GO TO 1015		FAN	1490
1005	WRITE (IPRI,1010) (ISUM(I),I=JAS,N)		FAN	1495
1010	FORMAT (1H1,1X,5(2X,3I7))		FAN	1500
1015	DO 1030 I=JAS,N		FAN	1505
	MASS=MASS+(I-1)		FAN	1510
	L=MASS+(I-JAS)		FAN	1515
1030	WRITE (IPRI,1100) I,(A(K),K=MASS,L)		FAN	1520
	IF (KEY-1)	235,1135,235	FAN	1525
1040	JAS14=JAS+14		FAN	1530
	JAS15=JAS+15		FAN	1535
	WRITE (IPRI,1000) (ISUM(I),I=JAS,JAS14)		FAN	1540
	GO TO 1050		FAN	1545
1045	JAS14=JAS+14		FAN	1550
	JAS15=JAS+15		FAN	1555
	WRITE (IPRI,1010) (ISUM(I),I=JAS,JAS14)		FAN	1560
1050	DO 1065 I=JAS,JAS14		FAN	1565
	MASS=MASS+(I-1)		FAN	1570
	L=MASS+(I-JAS)		FAN	1575
1065	WRITE (IPRI,1100) I,(A(K),K=MASS,L)		FAN	1580
	DO 1085 I=JAS15,N		FAN	1585
	MASS=MASS+(I-1)		FAN	1590
	L=MASS+14		FAN	1595
1085	WRITE (IPRI,1100) I,(A(K),K=MASS,L)		FAN	1600
	JAS=JAS+15		FAN	1605


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BASS=MASS
BAS=JAS
BASS=(BAS/2.000)*(BAS-1.000)+1.000
MASS=BASS
KOR=KOR+15
IF (N-KOR) 1005,1005,1045
1100 FORMAT (1H ,13,5(2X,3F7.3))
C *****
C SET UP NEXT ITERATION
C *****
1105 DO 1110 I=1,N
1110 X(I)=Y(I)
IF (IHSTY-9999) 1130,1120,1130
1120 WRITE (IPRI,1125) VITER
1125 FORMAT (1H ,14HSTATEMENT 1002,F5.0)
1130 GO TO 315
1135 IF(FANPLT) GO TO 2001
GO TO 1136
2001 READ(IREA,2003) NMAP
2003 FORMAT(I5)
XMAX = 1.0
XMIN = -1.0
YMAX = 1.0
YMIN = -1.0
XINT = .0333
DO 2005 MAP=1,NMAP
READ(IREA,2006) NF1,NF2
WRITE(IPRI,9999)
9999 FORMAT(1H1)
WRITE(IPRI,3006)NF1,NF2
3006 FORMAT(45X,30HSCATTERGRAM OF FACTOR LOADING,/,50X, 6HFACTOR,I4,2X
13HVS.,I4,/)
2005 CALL PLOT(FM, XMAX,XMIN,YMAX,YMIN,XINT,N,NF1,NF2,JUM)
2006 FORMAT(2I5)
1136 IF(IVROP.EQ.0) RETURN
IF (NFAN.EQ.0) STOP
CALL VROT(FM,N,M,JUM)
RETURN
C *****
C ERROR MESSAGES CAUSED BY MISTAKES IN INPUT OR OVERFLOWS
C *****
1140 WRITE (IPRI,1145)
1145 FORMAT (1H ,75HERROR IN PARAMETER CARD-THE NUMBER OF VARIABLES MAYFAN
1 NOT BE ZERO OR NEGATIVE)
GO TO 1215
1150 WRITE (IPRI,1155)
1155 FORMAT (1H ,62HERROR IN PARAMETER CARD-THE MAXIMUM NUMBER OF VARIAFAN
IBLES IS 120)
GO TO 1215
1160 WRITE (IPRI,1165)
1165 FORMAT (1H ,73HERROR IN PARAMETER CARD-THE NUMBER OF FACTORS MAY NFAN
1OT BE ZERO OR NEGATIVE)
GO TO 1215
1170 WRITE (IPRI,1175)
1175 FORMAT (1H ,60HERROR IN PARAMETER CARD-THE MAXIMUM NUMBER OF FACTOFAN
1RS IS 120)
GO TO 1215
1180 WRITE (IPRI,1185)
1185 FORMAT (1H ,79HTHE NUMBER OF FACTORS EXTRACTED MAY NOT BE GREATER FAN
1THAN THE NUMBER OF VARIABLES)

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GO TO 1215
1190 WRITE (IPRI,1195)
1195 FORMAT (1H ,27HOVERFLOW ERROR Y(I)-10. POS)
GO TO 1135
1200 WRITE (IPRI,1205)
1205 FORMAT (1H ,89HERROR IN PARAMETER CARD-VALUE OF VARIANCE (EIGENVAL
LUE) MAY NOT EXCEED SUM OF DIAGONALS. )
GO TO 1215
1215 RETURN
END
SUBROUTINE VROT(FM,N,M,JUM)
C *****
C *****VARIMAX ROTATION*****
C *****
DIMENSION H(120),FM(JUM,JUM)
DIMENSION SUMSQ(60),COMSUM(120),CUMPER(60),SUMQ(120)
COMMON /TITLE/NO1,NO2, NUM, NVR,IREA,IPRI,IPUN
COMMON /FACTR/NFAN,IVROP,FANPLT,VARPLT,ORJPLT
LOGICAL LCARD,ORJPLT,FANPLT,VARPLT
COMMON /TLABL/TTLE(20)
WRITE (IPRI,10)
10 FORMAT (1H1,/////////57X,16HVARIMAX ROTATION//)
WRITE (IPRI,20)TTLE
20 FORMAT (1H ,25X,20A4//)
C *****
C READ OPTIONS FOR VARIMAX ROTATION
C *****
READ (IREA,25) IMPRT,INPCH,LZ
25 FORMAT (3I5)
WRITE (IPRI,30) NO1,NO2,N,LZ
30 FORMAT (1H ,36X,12HPROBLEM NAME,2X,2A4,10X,I3,12H VARIABLES , ,I3,8V
1H FACTORS//)
XN=N
L = LZ
IF (N-120) 40,40,840
40 IF (L-60) 45,45,850
45 IF (N) 860,860,50
50 IF (L) 870,870,55
55 IF (N-L) 885,60,60
60 E=.005
IHO=0
ICOR=((N-1)/6)+1
ICORK=((L-1)/6)+1
IVM=1
IF (IMPRT) 75,95,75
75 KEY=1
1000 FORMAT(10F11.5)
WRITE (IPRI,85)
85 FORMAT (1H1,47X,38HTHE ORIGINAL MATRIX OF FACTOR LOADINGS/)
GO TO 545
95 SQRT2=0.70710678
IHO=1
WRITE (IPRI,105)
105 FORMAT (1H1,59X,13HCOMMUNALITIES/)
C *****
C NORMALIZE FACTOR MATRIX
C *****
DO 145 I=1,N
SUMH=0.0
DO 130 J=1,L

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X=FM(I,J) VROT 255
130 SUMH=SUMH+(X*X) VROT 260
C ***** VROT 265
C PRINT COMMUNALITIES VROT 270
C ***** VROT 275
WRITE (IPRI,140) I,SUMH VROT 280
140 FORMAT (1H ,54X,I6,F12.5) VROT 285
145 H(I)=SQRT(SUMH) VROT 290
DO 160 I=1,N VROT 295
DO 160 J=1,L VROT 300
160 FM(I,J)=FM(I,J)/H(I) VROT 305
C ***** VROT 310
C FACTOR MATRIX ROTATION VROT 315
C ***** VROT 320
165 LL=L-1 VROT 325
DO 480 J=1,LL VROT 330
JJ=J+1 VROT 335
DO 480 K=JJ,L VROT 340
A=0.0 VROT 345
B=0.0 VROT 350
C=0.0 VROT 355
D=0.0 VROT 360
DO 235 I=1,N VROT 365
X=FM(I,J) VROT 370
Y=FM(I,K) VROT 375
A=A+(X-Y)*(X+Y) VROT 380
B=B+2.0*X*Y VROT 385
C=C+X*X*X*X-(6.0*X*X*Y*Y)+Y*Y*Y*Y VROT 390
235 D=D+(4.0*X*X*X*Y)-(4.0*Y*Y*Y*X) VROT 395
XN=N VROT 400
XNUM=D-(2.0*A*B)/XN VROT 405
DEN=C-(A*A-B*B)/XN VROT 410
ANUM=ABS(XNUM) VROT 415
ADEN=ABS(DEN) VROT 420
IF (ANUM-ADEN) 275,270,300 VROT 425
270 IF (ANUM) 800,470,325 VROT 430
275 TAN4T=ANUM/ADEN VROT 435
IF (TAN4T-E) 405,285,285 VROT 440
285 COS4T=1.0/SQRT(1.0+(TAN4T*TAN4T)) VROT 445
SIN4T=TAN4T*COS4T VROT 450
GO TO 340 VROT 455
300 CTN4T=ADEN/ANUM VROT 460
IF (CTN4T-E) 425,310,310 VROT 465
310 SIN4T=1.0/SQRT(1.0+(CTN4T*CTN4T)) VROT 470
COS4T=CTN4T*SIN4T VROT 475
GO TO 340 VROT 480
325 TAN4T=1.0 VROT 485
COS4T=SQRT2 VROT 490
SIN4T=SQRT2 VROT 495
C ***** VROT 500
C ANUM=ADEN=0 DO NEXT ROTATION VROT 505
C ***** VROT 510
340 COS2T=SQRT((1.0+COS4T)/2.0) VROT 515
SIN2T=SIN4T/(2.0*COS2T) VROT 520
COST=SQRT((1.0+COS2T)/2.0) VROT 525
SINT=SIN2T/(2.0*COST) VROT 530
IF (DEN) 380,380,365 VROT 535
365 COSQ=COST VROT 540
SINQ=SINT VROT 545
GO TO 390 VROT 550

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380 COSO=(SQRT2*COST)+(SQRT2*SINT)          VROT 555
    SINO=(SQRT2*COST)-(SQRT2*SINT)          VROT 560
390 IF (XNUM) 395,470,440                    VROT 565
395 SINO=0.0-SINO                            VROT 570
    GO TO 440                                VROT 575
405 IF (DEN) 410,470,470                    VROT 580
410 COSO=SQRT2                              VROT 585
    SINO=SQRT2                              VROT 590
    GO TO 440                                VROT 595
425 COS4T=0.0                               VROT 600
    SIN4T=1.0                               VROT 605
    GO TO 340                                VROT 610
440 DO 460 I=1,N                             VROT 615
    X=FM(I,J)                               VROT 620
    Y=FM(I,K)                               VROT 625
    FM(I,J)=X*COSO+Y*SINO                   VROT 630
460 FM(I,K)=Y*COSO-X*SINO                   VROT 635
465 LTEST=(L*(L-1))/2                       VROT 640
470 LTEST=LTEST-1                          VROT 645
    IF (LTEST) 465,490,480                 VROT 650
480 CONTINUE                                 VROT 655
    GO TO 165                                VROT 660
C ***** VROT 665
C DENORMALIZE FACTOR MATRIX                 VROT 670
C ***** VROT 675
490 DO 500 I=1,N                             VROT 680
    DO 500 J=1,L                             VROT 685
500 FM(I,J)=H(I)*FM(I,J)                   VROT 690
C ***** VROT 695
C PRINT MATRIX OF FACTOR LOADINGS (INPUT MATRIX OPTIONAL) VROT 700
C ***** VROT 705
    KEY=2                                    VROT 710
    WRITE (IPRI,540)                         VROT 715
540 FORMAT (1H1,47X,37HTHE ROTATED MATRIX OF FACTOR LOADINGS//) VROT 720
545 WRITE (IPRI,550)                         VROT 725
    IF (KEY.EQ.1) L=M                       VROT 730
    IF (KEY.EQ.2) L=LZ                      VROT 735
    DO 510 J=1,L                             VROT 740
    SUM=0.0                                  VROT 745
    DO 505 I=1,N                             VROT 750
505 SUM=SUM+(FM(I,J))**2                    VROT 755
    SUMQ(J)=SUM                              VROT 760
510 SUMSQ(J)=(SUM*100.0)/XN                 VROT 765
    DO 520 I=1,N                             VROT 770
    SUM=0.0                                  VROT 775
    DO 515 J=1,L                             VROT 780
515 SUM=SUM+(FM(I,J))**2                    VROT 785
520 COMSUM(I)=SUM                          VROT 790
    SUM=0.0                                  VROT 795
    DO 525 I=1,L                             VROT 800
    SUM=SUM+SUMSQ(I)                        VROT 805
525 CUMPER(I)=SUM                          VROT 810
    IHO=1                                    VROT 815
550 FORMAT (5X,110H          F 1          F 2          F 3          F 4          VROT 820
    IF 5          F 6          F 7          F 8          F 9          F 10/) VROT 825
    MASS=1                                   VROT 830
    IF (L-10) 760,560,560                 VROT 835
560 DO 565 I=1,N                             VROT 840
565 WRITE (IPRI,750) I,(FM(I,J),J=1,10) VROT 845
    IF (IHO-1) 575,570,575                 VROT 850

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570 WRITE (IPRI,790) (SUMQ(J),J=1,10) VROT 855
    WRITE (IPRI,785) (SUMSQ(J),J=1,10) VROT 860
    WRITE (IPRI,780) (CUMPER(J),J=1,10) VROT 865
575 IF (L-10) 795,795,580 VROT 870
580 WRITE (IPRI,585) VROT 875
585 FORMAT (1H1,4X,110H F 11 F 12 F 13 F 14 VROT 880
1 F 15 F 16 F 17 F 18 F 19 F 20/) VROT 885
    MASS=11 VROT 890
    IF (L-20) 760,595,595 VROT 895
595 DO 600 I=1,N VROT 900
600 WRITE (IPRI,750) I,(FM(I,J),J=11,20) VROT 905
    IF (IHO-1) 610,605,610 VROT 910
605 WRITE (IPRI,790) (SUMQ(J),J=11,20) VROT 915
    WRITE (IPRI,785) (SUMSQ(J),J=11,20) VROT 920
    WRITE (IPRI,780) (CUMPER(J),J=11,20) VROT 925
610 IF (L-20) 795,795,615 VROT 930
615 WRITE (IPRI,620) VROT 935
620 FORMAT (1H1,4X,110H F 21 F 22 F 23 F 24 VROT 940
1 F 25 F 26 F 27 F 28 F 29 F 30/) VROT 945
    MASS=21 VROT 950
    IF (L-30) 760,630,630 VROT 955
630 DO 635 I=1,N VROT 960
635 WRITE (IPRI,750) I,(FM(I,J),J=21,30) VROT 965
    IF (IHO-1) 645,640,645 VROT 970
640 WRITE (IPRI,790) (SUMQ(J),J=21,30) VROT 975
    WRITE (IPRI,785) (SUMSQ(J),J=21,30) VROT 980
    WRITE (IPRI,780) (CUMPER(J),J=21,30) VROT 985
645 IF (L-30) 795,795,650 VROT 990
650 WRITE (IPRI,655) VROT 995
655 FORMAT (1H1,4X,110H F 31 F 32 F 33 F 34 VROT1000
1 F 35 F 36 F 37 F 38 F 39 F 40/) VROT1005
    MASS=31 VROT1010
    IF (L-40) 760,665,665 VROT1015
665 DO 670 I=1,N VROT1020
670 WRITE (IPRI,750) I,(FM(I,J),J=31,40) VROT1025
    IF (IHO-1) 680,675,680 VROT1030
675 WRITE (IPRI,790) (SUMQ(J),J=31,40) VROT1035
    WRITE (IPRI,785) (SUMSQ(J),J=31,40) VROT1040
    WRITE (IPRI,780) (CUMPER(J),J=31,40) VROT1045
680 IF (L-40) 795,795,685 VROT1050
685 WRITE (IPRI,690) VROT1055
690 FORMAT (1H1,4X,110H F 41 F 42 F 43 F 44 VROT1060
1 F 45 F 46 F 47 F 48 F 49 F 50/) VROT1065
    MASS=41 VROT1070
    IF (L-50) 760,700,700 VROT1075
700 DO 705 I=1,N VROT1080
705 WRITE (IPRI,750) I,(FM(I,J),J=41,50) VROT1085
    IF (IHO-1) 715,710,715 VROT1090
710 WRITE (IPRI,790) (SUMQ(J),J=41,50) VROT1095
    WRITE (IPRI,785) (SUMSQ(J),J=41,50) VROT1100
    WRITE (IPRI,780) (CUMPER(J),J=41,50) VROT1105
715 IF (L-50) 795,795,720 VROT1110
720 WRITE (IPRI,725) VROT1115
725 FORMAT (1H1,4X,110H F 51 F 52 F 53 F 54 VROT1120
1 F 55 F 56 F 57 F 58 F 59 F 60/) VROT1125
    MASS=51 VROT1130
    IF (L-60) 760,735,735 VROT1135
735 DO 740 I=1,N VROT1140
740 WRITE (IPRI,750) I,(FM(I,J),J=51,60) VROT1145
    IF (IHO-1) 755,745,755 VROT1150

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745	WRITE (IPRI,790) (SUMQ(J),J=51,60)	VROT1155
	WRITE (IPRI,785) (SUMSQ(J),J=51,60)	VROT1160
	WRITE (IPRI,780) (CUMPER(J),J=51,60)	VROT1165
750	FORMAT (1H ,I3,3X,10F11.5)	VROT1170
755	CONTINUE	VROT1175
	GO TO 795	VROT1180
760	DO 765 I=1,N	VROT1185
765	WRITE (IPRI,775) I,(FM(I,J),J=MASS,L)	VROT1190
	IF (IHO-1) 795,770,795	VROT1195
770	WRITE (IPRI,790) (SUMQ(J),J=MASS,L)	VROT1200
	WRITE (IPRI,785) (SUMSQ(J),J=MASS,L)	VROT1205
	WRITE (IPRI,780) (CUMPER(J),J=MASS,L)	VROT1210
775	FORMAT (1H ,I3,3X,9F11.5)	VROT1215
785	FORMAT(1H ,/,6HVAREXP,10F11.5)	VROT1225
780	FORMAT(1H ,/,6HCUMPER,10F11.5)	VROT1220
790	FORMAT(1H ,/,6HSUM SQ,10F11.5)	VROT1230
795	IF (KEY-1) 95,95,800	VROT1235
C	*****	VROT1240
C	PUNCH MATRIX OF VARIABLES (OPTIONAL)	VROT1245
C	*****	VROT1250
800	WRITE (IPRI,105)	VROT1255
	WRITE (IPRI,140) (I,CONSUM(I),I=1,N)	VROT1260
	IF (VARPLT) GO TO 1005	VROT1265
	GO TO 801	VROT1270
1005	READ(IREA,2003) NMAP	VROT1275
2003	FORMAT(I5)	VROT1280
	XMAX = 1.0	VROT1285
	XMIN = -1.0	VROT1290
	YMAX = 1.0	VROT1295
	YMIN = -1.0	VROT1300
	XINT = .0333	VROT1305
	DO 2005 MAP=1,NMAP	VROT1310
	READ(IREA,2006) NF1,NF2	VROT1315
	WRITE(IPRI,9999)	VROT1320
9999	FORMAT(1H1)	VROT1325
	WRITE(IPRI,3006)NF1,NF2	VROT1330
3006	FORMAT(45X,30HSCATTERGRAM OF ROTATED FACTORS,/,50X,6HFACTOR,I4,2X,	VROT1335
	13HVS.,I4,//)	VROT1340
2005	CALL PLOT(FM,XMAX,XMIN,YMAX,YMIN,XINT,N,NF1,NF2,JUM)	VROT1345
2006	FORMAT(2I5)	VROT1350
801	IF(INPCH) 805,835,805	VROT1355
805	DO 830 J=1,N	VROT1360
	IVM=1	VROT1365
	DO 825 JIM=1,ICORK	VROT1370
	IEND=IVM+5	VROT1375
	IF (IEND-L) 815,815,810	VROT1380
810	IEND=L	VROT1385
815	WRITE (IPUN,820) J,JIM,(FM(J,I),I=IVM,IEND)	VROT1390
820	FORMAT (4HVAR.,I3,2HCD,I3,6F10.5)	VROT1395
825	IVM=IVM+6	VROT1400
830	CONTINUE	VROT1405
835	RETURN	VROT1410
C	*****	VROT1415
C	ERROR MESSAGES CAUSED BY MISTAKES IN INPUT	VROT1420
C	*****	VROT1425
840	WRITE (IPRI,845)	VROT1430
845	FORMAT (1H ,62HERROR IN PARAMETER CARD-THE MAXIMUM NUMBER OF VARIA	VROT1435
	IBLES IS 120)	VROT1440
	GO TO 890	VROT1445
850	WRITE (IPRI,855)	VROT1450

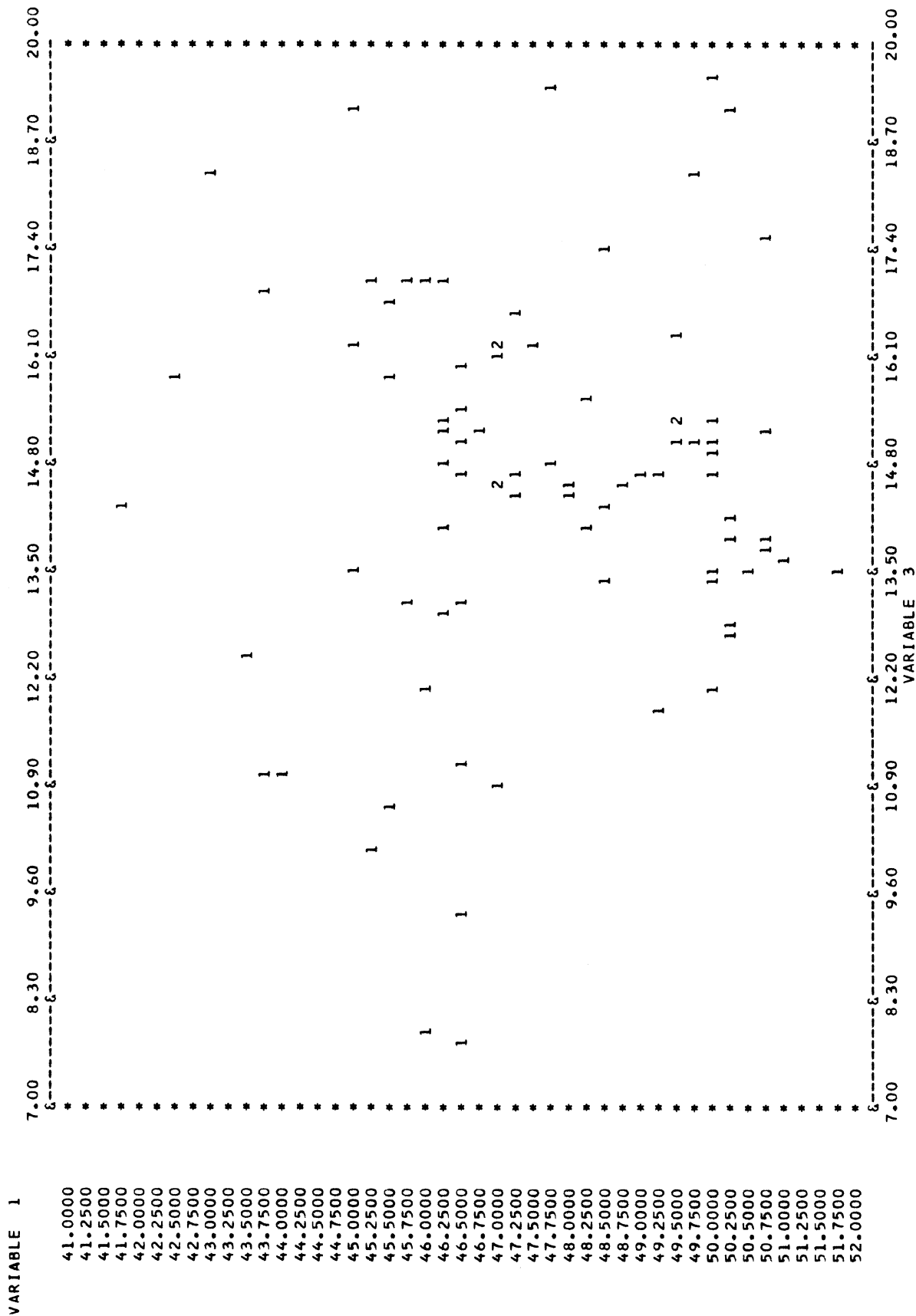
855	FORMAT (1H ,59HERROR IN PARAMETER CARD-THE MAXIMUM NUMBER OF FACTORS MAY NOT BE GREATER THAN THE NUMBER OF VARIABLES)	VROT1455
	1RS IS 60)	VROT1460
	GO TO 890	VROT1465
860	WRITE (IPRI,865)	VROT1470
865	FORMAT (1H ,75HERROR IN PARAMETER CARD-THE NUMBER OF VARIABLES MAY NOT BE ZERO OR NEGATIVE)	VROT1475
	1 NOT BE ZERO OR NEGATIVE)	VROT1480
	GO TO 890	VROT1485
870	WRITE (IPRI,875)	VROT1490
875	FORMAT (1H ,73HERROR IN PARAMETER CARD-THE NUMBER OF FACTORS MAY NOT BE ZERO OR NEGATIVE)	VROT1495
	1 NOT BE ZERO OR NEGATIVE)	VROT1500
880	FORMAT (1H ,69HTHE NUMBER OF FACTORS MAY NOT BE GREATER THAN THE NUMBER OF VARIABLES)	VROT1505
	1UMBER OF VARIABLES)	VROT1510
	GO TO 890	VROT1515
885	WRITE (IPRI,880)	VROT1520
890	RETURN	VROT1525
	END	VROT1530
	SUBROUTINE PLOT(X, XMAX,XMIN,YMAX,YMIN,XINT,NPOINT,I1,I2,JUM)	PLOT 5
C	TWO DIMENSIONAL PLOTTING	PLOT 10
	INTEGER BLNK,STAR,PLUS	PLOT 15
	DIMENSION X(JUM,JUM), NUM(9),YS(11)	PLOT 20
	DIMENSION MAP(100)	PLOT 25
	COMMON /TITLE/NO1,NO2, MUM, NVR,IREA,IPRI,IPUN	PLOT 30
	DATA BLNK/1H /,STAR/1H*/ ,LINE/1HI/, NUM/1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9/	PLOT 35
	DATA MINUS/1H-/,PLUS/1H+/	PLOT 40
	YD=100./(YMAX-YMIN)	PLOT 45
	NX=(XMAX-XMIN)/XINT+1.	PLOT 50
	DO 110 I= 1,11	PLOT 55
110	YS(I) =YMIN+10.*FLOAT(I-1)/YD	PLOT 60
	WRITE(IPRI,1007) I1	PLOT 65
1007	FORMAT(1X, 8HVARIABLE,I3)	PLOT 70
	WRITE(IPRI,1005) (YS(I),I=1,11)	PLOT 75
1005	FORMAT(17X,11(F6.2,4X))	PLOT 80
	DO 120 LIN=1,100	PLOT 85
120	MAP(LIN)=MINUS	PLOT 90
	DO 130 LIN=1,100,10	PLOT 95
130	MAP(LIN)=PLUS	PLOT 100
	WRITE(IPRI,1001)(MAP(I),I=1,100)	PLOT 105
	DO 11 I=1,NX	PLOT 110
	XX=XMIN+FLOAT(I-1)*XINT	PLOT 115
	DO 12 J=1,100	PLOT 120
12	MAP(J)=0	PLOT 125
	MAP(1)=LINE	PLOT 130
	MAP(100)=LINE	PLOT 135
	DO 13 J=1,NPOINT	PLOT 140
	XNX = XX+ XINT	PLOT 145
299	IF(X(J,I1).GE.XX.AND. X(J,I1).LT.XNX) GO TO 300	PLOT 150
	GO TO 13	PLOT 155
300	NSP=(X(J,I2)-YMIN)*YD+1.49999999	PLOT 160
301	IF(NSP.GT.100)NSP=100	PLOT 165
	IF(NSP.LT.1)NSP=1	PLOT 170
	MAP(NSP)=MAP(NSP)+1	PLOT 175
13	CONTINUE	PLOT 180
	DO 17 NSP=1,100	PLOT 185
	IF(MAP(NSP).GT.9)MAP(NSP)=STAR	PLOT 190
	IF(MAP(NSP).EQ.0)MAP(NSP)=BLNK	PLOT 195
	DO 16 K=1,9	PLOT 200
	IF(MAP(NSP).EQ.K)MAP(NSP)=NUM(K)	PLOT 205
16	CONTINUE	PLOT 210
17	CONTINUE	PLOT 215
		PLOT 220

11	WRITE(IPRI,1000)XX,(MAP(J),J=1,100)	PLOT 225
	DO 140 LIN=1,100	PLOT 230
140	MAP(LIN)=MINUS	PLOT 235
	DO 150 LIN=1,100,10	PLOT 240
150	MAP(LIN)=PLUS	PLOT 245
	WRITE(IPRI,1001)(MAP(I),I=1,100)	PLOT 250
	WRITE(IPRI,1005) (YS(I),I=1,11)	PLOT 255
	WRITE(IPRI,1008) I2	PLOT 260
1008	FORMAT(60X,8HVARIABLE,I3)	PLOT 265
1000	FORMAT(1X,F12.4,7X,100A1)	PLOT 270
1001	FORMAT(20X,100A1)	PLOT 275
	RETURN	PLOT 280
	END	PLOT 285

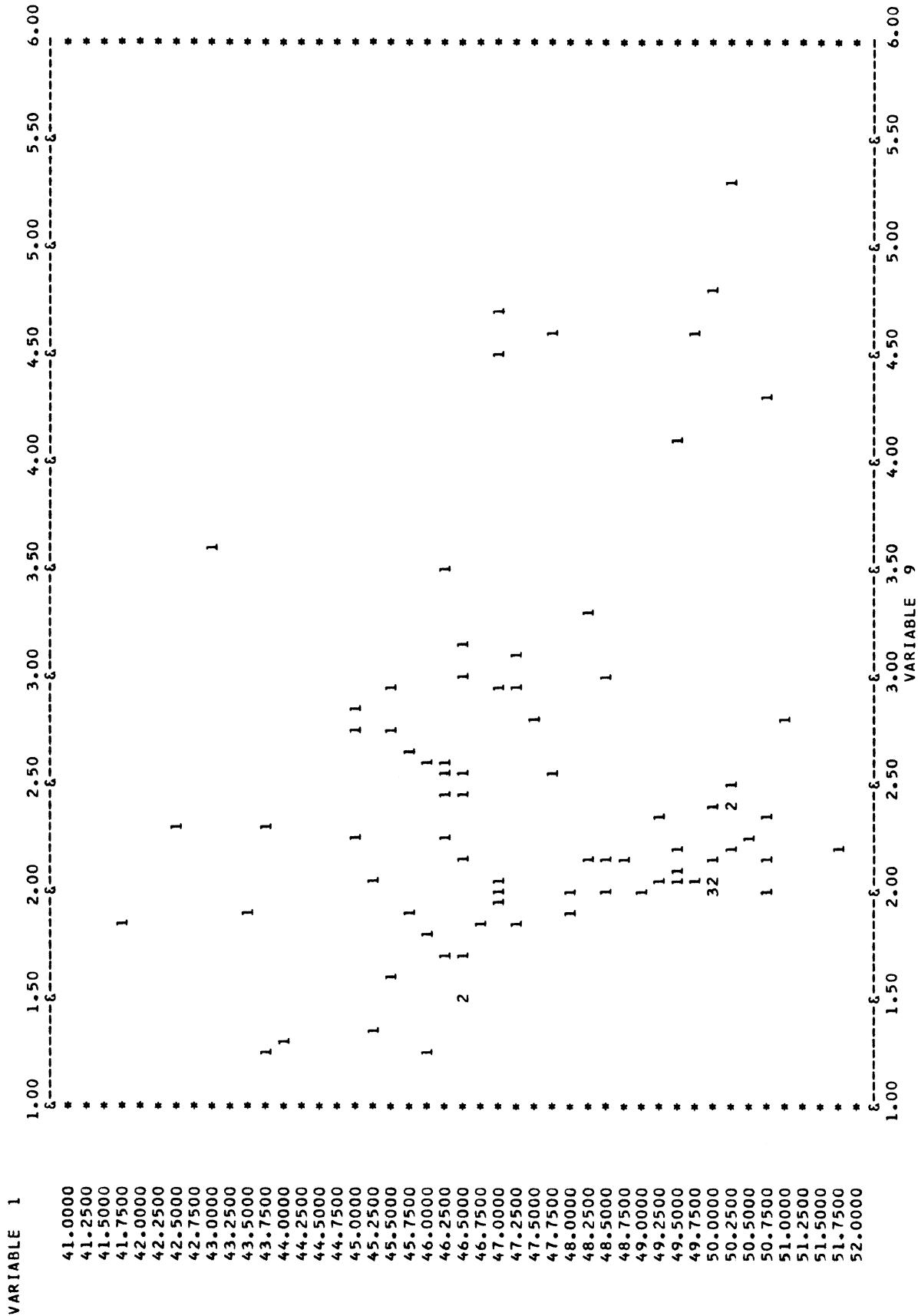
11	11	QQMODFNV	1	1	TTT						
(2X,11F7.0,L1)											
THOLEIITIC - ALKALIC BASALT PROBLEM											
Q-MODE FACTOR ANALYSIS											
42	50.25	2.12	19.03	4.53	5.50	.22	3.11	5.98	5.30	2.20	1.14
2	45.74	4.16	16.76	9.39	2.83	.21	3.24	9.02	2.73	2.24	.61
39	49.73	3.05	16.39	7.58	3.98	.23	4.06	7.17	4.12	1.93	.84
41	49.79	2.51	18.37	6.03	4.82	.22	4.01	6.68	4.58	2.08	.56
20	47.99	2.62	19.36	5.83	5.17	.21	4.39	6.54	4.58	1.82	.63
14	45.94	3.00	17.04	7.81	3.28	.25	3.67	10.14	2.63	1.94	.55
13	46.52	2.78	16.00	5.56	4.20	.23	6.09	10.40	2.45	2.45	.50
7	45.10	0.70	19.05	5.37	5.73	.22	6.03	7.06	2.85	1.90	.66
11	47.20	3.85	16.22	5.20	6.95	.18	4.77	8.49	2.93	2.00	.74
38	50.92	2.55	17.59	3.80	6.69	.20	3.90	6.97	4.28	1.86	.40
40	50.09	2.47	19.49	.73	8.47	.15	4.33	6.92	4.82	1.93	.78
86	47.03	1.92	16.22	5.53	6.07	.10	4.00	8.08	4.50	1.54	.24
15	46.68	4.20	15.01	6.35	5.44	.10	4.30	9.84	3.13	1.51	.47
12	48.65	3.80	17.43	2.80	7.12	.17	4.14	9.72	2.98	2.13	.52
3	45.24	3.22	16.17	4.52	6.86	.19	7.01	9.76	2.75	1.95	.48
10	43.04	4.00	18.26	2.91	7.82	.20	4.95	9.80	3.62	1.67	.55
85	46.42	1.58	15.28	2.22	5.93	.17	7.06	11.48	3.49	1.61	.78
37	48.42	3.25	13.97	4.17	9.57	.17	4.61	8.86	3.30	1.29	.91
16	43.58	3.30	12.49	8.41	4.92	.19	10.33	9.34	1.91	1.10	.24
1	46.51	2.98	15.48	3.41	8.68	.17	8.17	8.85	3.00	1.22	.59
5	42.60	3.79	15.89	2.86	8.34	.18	8.45	9.88	2.30	1.67	.44
70	45.60	3.19	15.89	5.98	7.54	.17	6.56	9.49	2.95	.70	.40
34	47.72	2.48	16.19	3.82	8.25	.08	5.68	11.20	2.80	.84	.43
9	43.75	4.25	16.92	1.82	9.30	.18	6.70	10.82	2.29	1.18	.39
19	46.49	3.09	17.07	5.35	7.84	.17	4.80	10.52	2.61	.52	.35
6	46.05	2.65	17.03	3.90	7.47	.32	6.30	11.24	2.60	1.07	.00
32	46.43	3.03	15.22	3.97	8.19	.10	8.40	10.37	2.55	.99	.33
35	47.32	3.09	16.68	2.63	8.67	.16	5.43	11.27	3.08	.79	.53
50	50.04	2.22	15.36	5.39	5.78	.17	7.32	10.17	2.02	.33	.31
8	45.25	4.00	17.06	2.30	8.42	.18	7.55	11.08	2.05	1.03	.27
36	47.19	2.27	10.95	3.31	10.21	.16	10.52	9.73	4.69	.93	.55
44	47.42	3.46	14.35	3.41	10.33	.18	5.57	9.80	2.95	.69	.43
31	46.65	3.22	14.72	3.63	8.98	.18	7.96	10.14	2.53	.80	.33
79	51.24	3.74	13.60	1.87	11.19	.18	5.12	9.03	2.81	.83	.41
29	41.83	3.16	14.32	4.81	8.98	.19	9.42	8.83	1.83	.77	.29
53	48.55	2.83	14.29	4.89	8.04	.18	6.42	10.76	2.15	.55	.28
54	48.17	2.44	14.46	5.58	6.05	.18	6.99	11.03	1.88	.29	.20
64	49.50	2.10	15.38	4.51	6.99	.17	7.23	10.44	2.10	.39	.28
66	46.91	2.44	15.23	5.54	6.18	.17	7.38	10.90	1.85	.19	.20
33	47.79	1.90	14.80	2.63	10.04	.14	6.89	11.31	2.56	.94	.26
68	50.02	2.23	15.05	3.77	7.37	.17	7.01	10.17	2.05	.33	.27
73	49.86	2.43	15.11	3.66	7.82	.17	6.00	10.34	2.05	.26	.27
72	48.29	2.56	15.54	3.27	7.88	.17	7.70	10.21	2.17	.28	.27
46	50.40	3.26	13.91	1.80	10.09	.18	6.57	10.65	2.52	.69	.30
27	45.77	2.47	13.16	2.97	9.27	.17	11.64	10.23	1.88	.29	.24
30	45.14	3.04	13.49	3.60	9.27	.18	10.02	10.60	2.24	.80	.26
48	49.42	2.42	11.83	3.83	8.08	.14	12.04	9.28	2.35	.59	.39
60	49.69	2.60	15.26	3.16	8.35	.16	6.50	10.78	2.20	.37	.25
4	43.96	2.36	11.06	5.29	6.37	.19	12.88	11.88	1.26	.57	.32
77	50.20	2.15	14.72	3.38	7.79	.17	7.88	9.81	2.00	.36	.27
76	50.20	2.40	14.93	3.64	7.67	.17	7.15	10.16	2.05	.30	.27
55	48.24	3.09	14.48	3.58	10.42	.20	6.05	10.02	2.00	.48	.30
51	50.80	1.93	15.25	2.91	7.23	.16	8.27	9.83	2.15	.28	.25
69	48.84	2.58	14.59	2.78	8.45	.17	7.25	10.90	2.15	.42	.33
75	49.67	2.33	15.08	2.86	8.57	.16	6.76	10.51	2.06	.32	.26
45	47.12	2.34	14.51	4.39	7.21	.18	10.74	10.36	1.94	.25	.25
17	46.39	2.13	12.94	2.05	10.16	.17	11.38	10.81	2.43	.93	.32
84	48.57	2.61	13.34	2.95	8.66	.17	10.41	10.26	2.02	.50	.26
28	46.31	3.10	14.83	4.06	9.26	.19	6.77	11.30	2.25	.20	.25
78	47.25	2.16	14.70	3.91	7.27	.16	10.46	10.22	1.86	.24	.25
59	47.10	2.31	16.05	3.12	8.27	.19	7.12	11.91	2.00	.19	.26
81	50.87	2.86	13.94	1.85	9.07	.17	7.35	11.09	2.34	.49	.25
47	49.37	2.50	14.73	1.71	9.39	.16	6.87	10.86	2.05	.40	.27
71	51.77	4.01	13.54	.75	9.63	.15	7.33	10.57	2.18	.45	.26
26	46.43	2.29	14.00	3.34	8.17	.17	11.41	11.86	1.69	.49	.25
58	50.07	2.70	13.32	1.92	9.28	.16	8.01	10.64	2.16	.45	.26
57	50.32	3.10	12.83	1.74	9.93	.10	7.39	11.06	2.38	.41	.30
82	50.68	2.54	13.55	1.39	9.35	.17	8.47	10.98	2.24	.45	.26
74	49.07	2.48	14.62	2.00	9.52	.17	7.80	10.38	2.01	.31	.28
65	47.14	2.88	14.57	2.09	10.85	.19	8.35	10.09	2.03	.33	.31
43	46.19	2.15	12.02	4.08	8.19	.17	12.75	10.73	1.79	.38	.20
83	50.24	2.92	13.46	1.17	10.94	.18	7.04	10.30	2.40	.52	.17
61	50.88	2.59	13.75	.73	10.42	.20	7.77	10.76	2.00	.52	.24
62	50.03	2.57	12.10	2.10	9.97	.16	9.57	10.58	2.01	.44	.21
49	50.37	2.33	14.20	1.28	10.10	.14	7.75	11.24	2.20	.56	.02
52	50.46	2.14	12.75	.82	10.68	.18	9.68	10.43	2.42	.51	.19
25	45.64	2.34	10.61	3.02	9.02	.18	14.32	10.88	1.62	.46	.25
22	44.24	2.34	11.01	3.36	8.97	.19	14.67	10.36	1.32	.30	.25
24	46.60	2.15	11.21	2.04	9.61	.17	15.01	10.60	1.52	.56	.18
18	45.30	1.85	10.11	3.75	8.91	.18	17.87	8.96	1.35	.30	.20
23	46.57	1.67	7.81	2.40	8.91	.13	19.74	10.65	1.70	.33	.34
21	46.01	1.61	7.96	2.54	9.09	.18	20.19	10.49	1.26	.27	.17
63	46.50	1.70	9.37	2.47	10.79	.11	21.00	6.25	1.52	.22	.10
67	46.68	1.91	13.15	4.71	7.62	.17	11.12	9.68	2.15	.49	.22 T
6											
1	52.	41.		3	20.		7.		0.25		
1	52.	41.		9			1.		0.25		
1	52.	41.		10	2.5		0.0		0.25		
6	.35	.05		7	22.		2.		.01		
5	12.	2.		7	22.		2.0		.2		
9	6.			10	2.5		0.0		.12		
5		5555									
3											
1	2										
1	3										
2	3										
1		3									
3											
1	2										
1	3										
2	3										

ALKALI-THOLEIITIC BASALT PROBLEM - HAMBURGER STAND OPTION

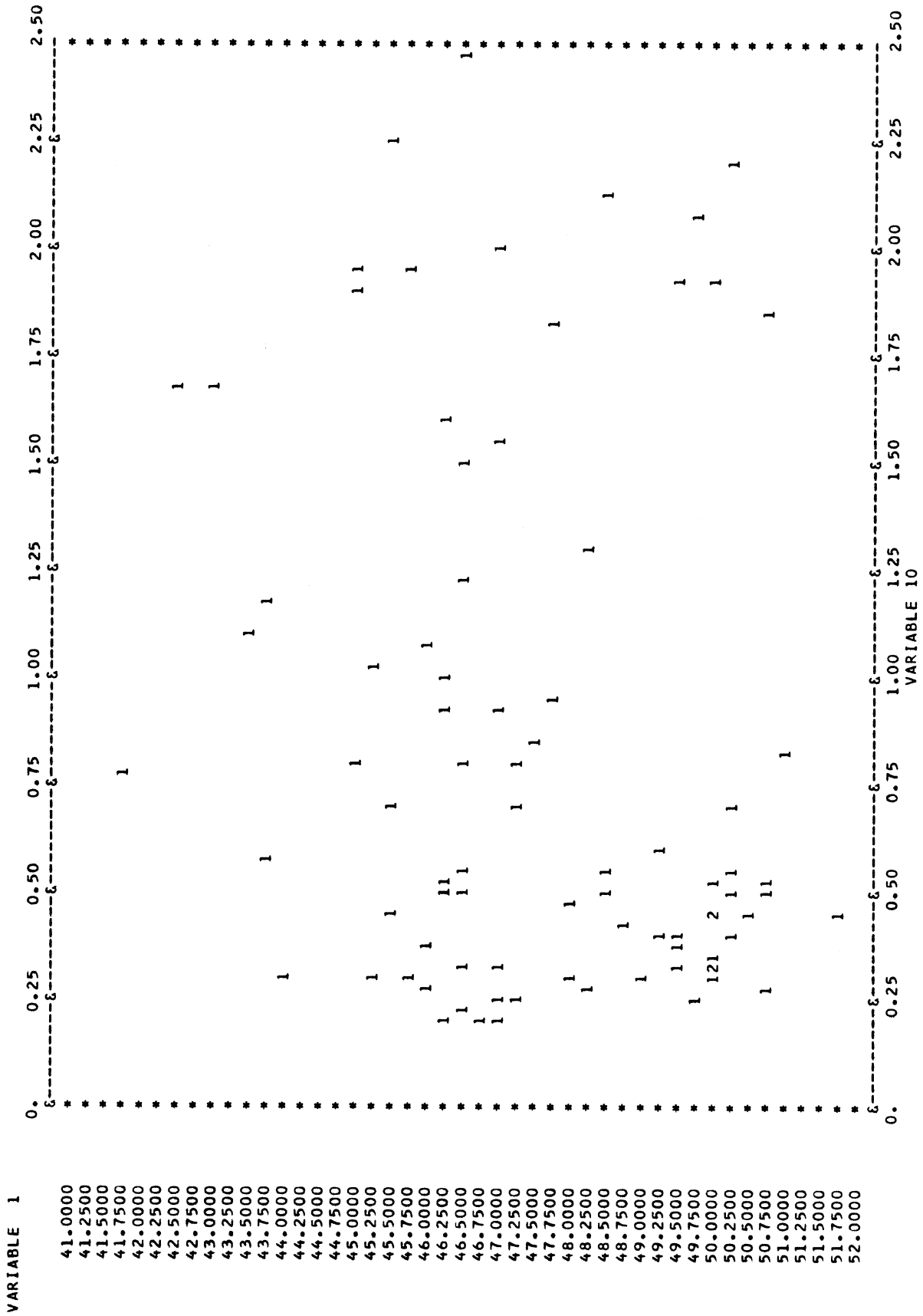
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 1 VS. 3



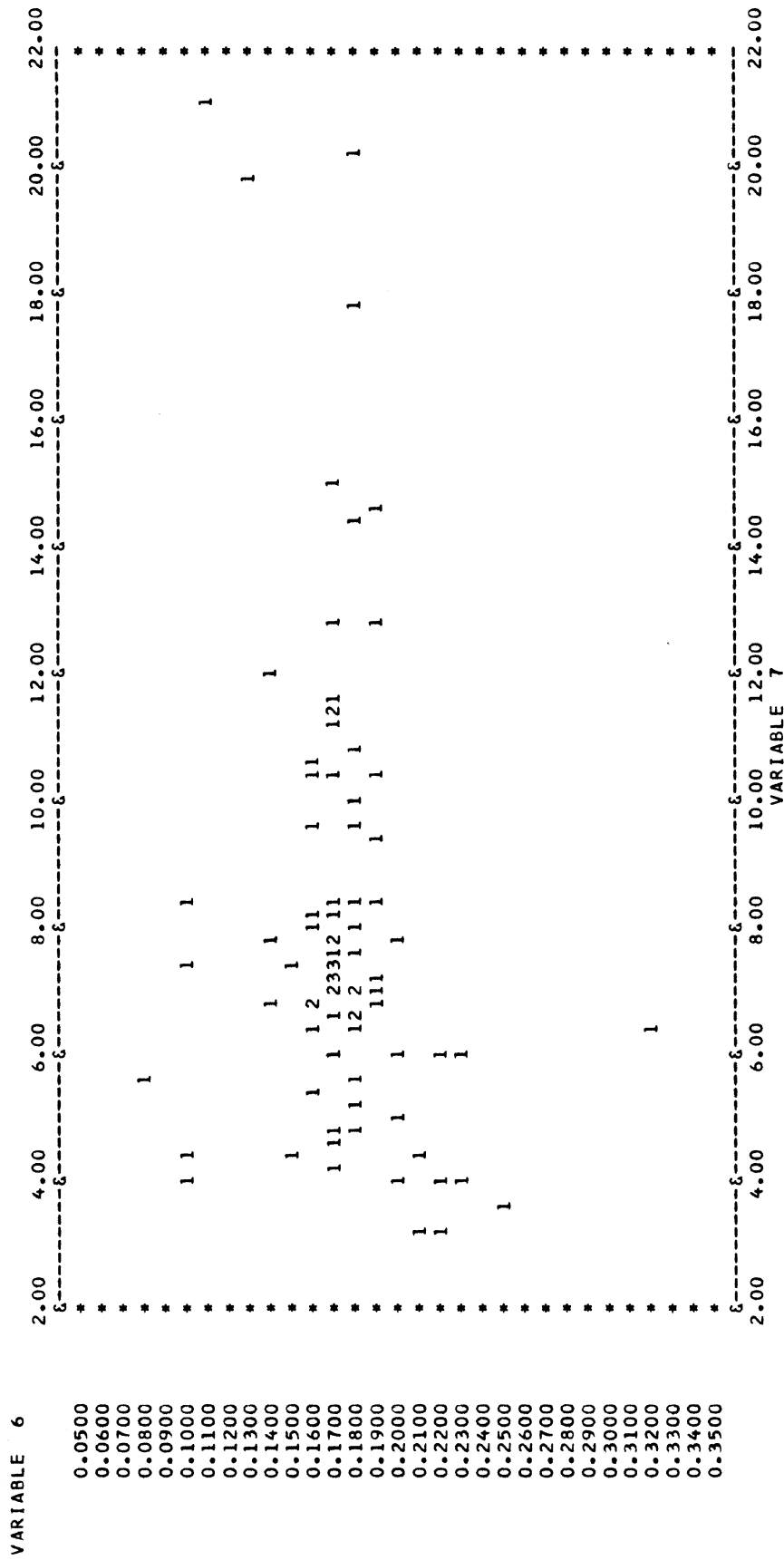
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 1 VS. 9



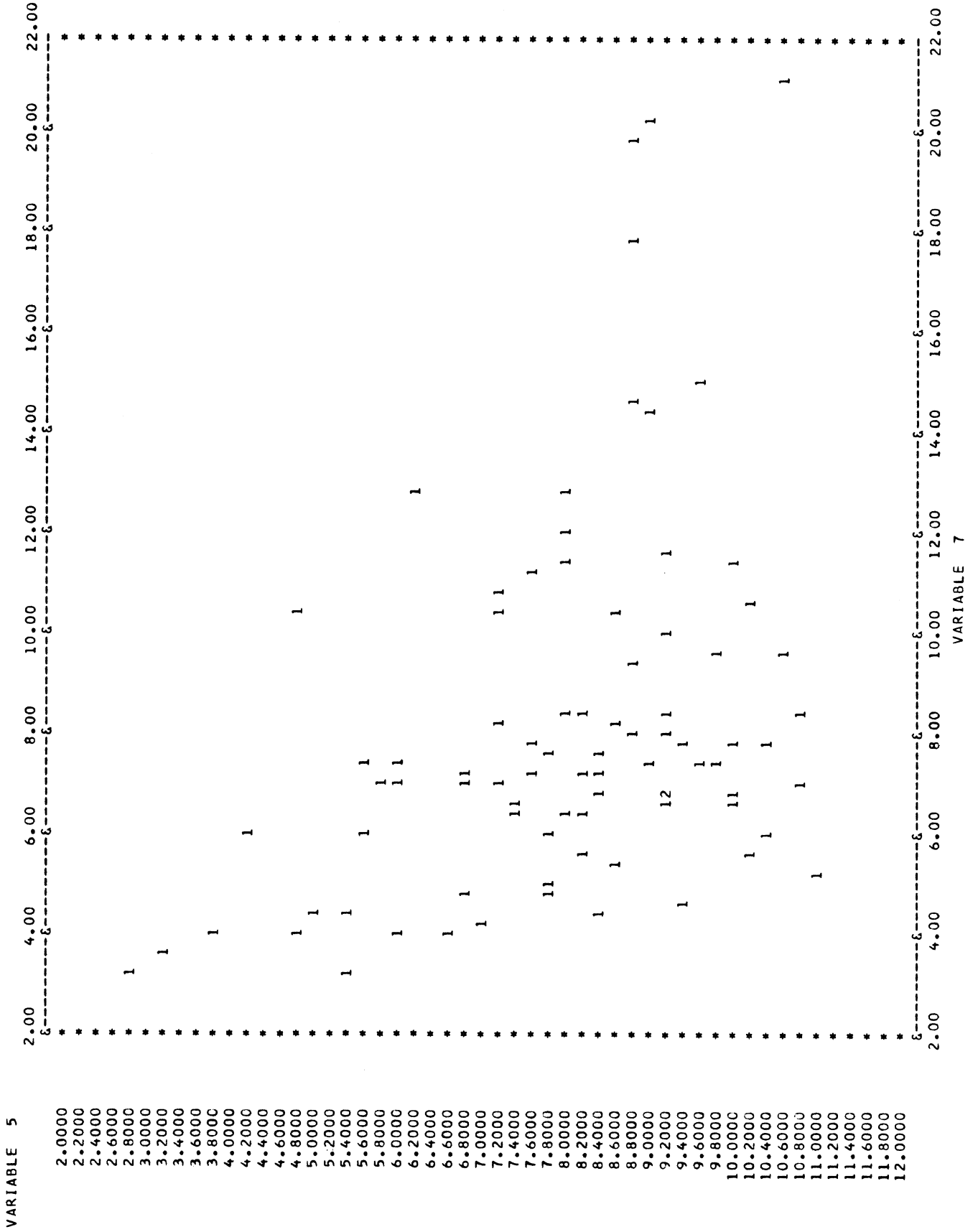
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 1 VS. 10



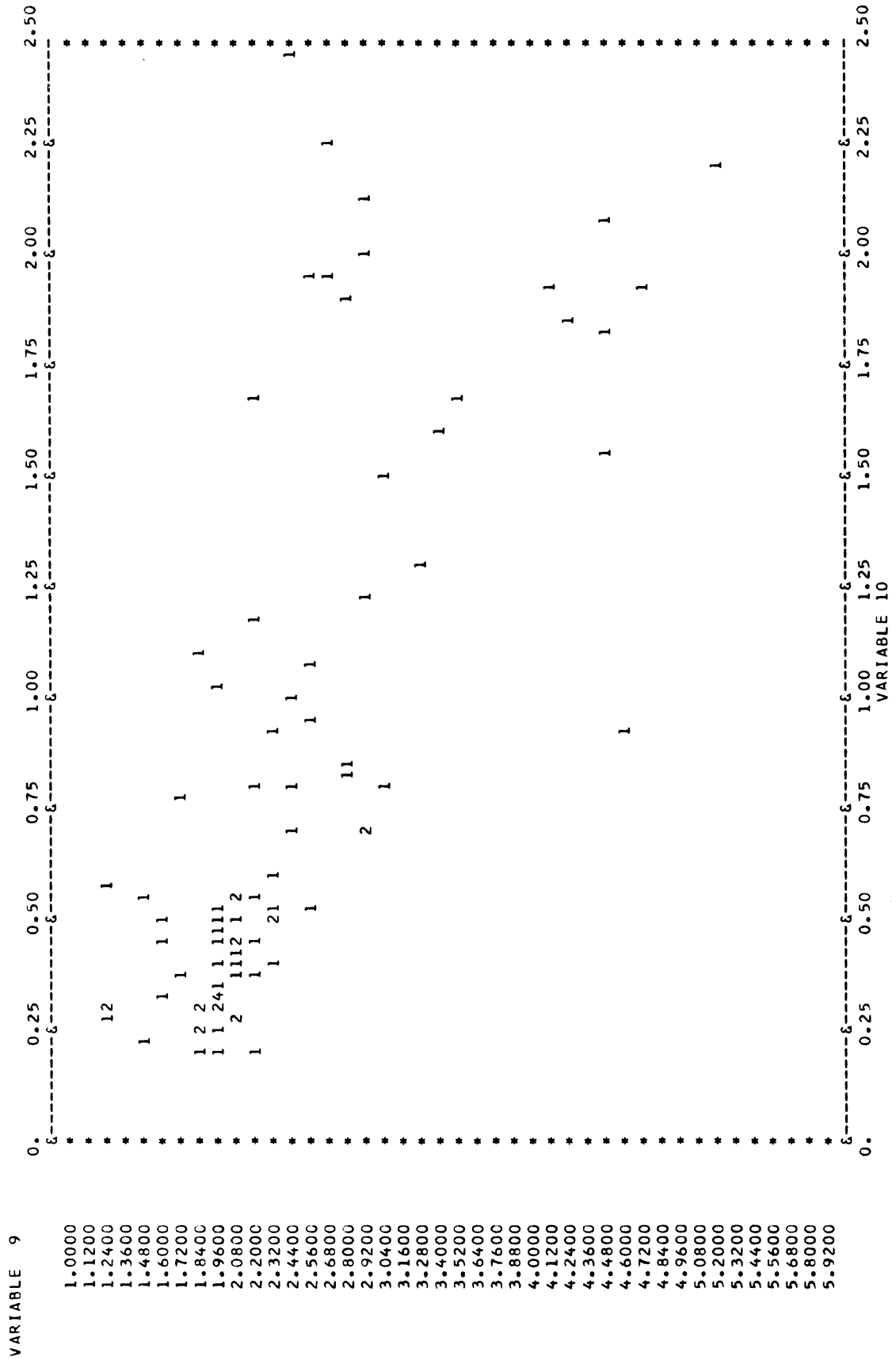
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 6 VS. 7



SCATTERGRAM OF ORIGINAL DATA
VARIABLE 5 VS. 7



SCATTERGRAM OF ORIGINAL DATA
VARIABLE 9 VS. 10



SYMMETRIC CORRELATION MATRIX

	NUMBER CASES					84	PROBLEM NAME				CORLFNVT
	1	2	3	4	5	6	7	8	9	10	
2	-0.146										
3	0.071	0.296									
4	-0.359	0.113	0.286								
5	0.175	-0.015	-0.493	-0.829							
6	-0.165	0.077	0.312	0.298	-0.338						
7	-0.301	-0.454	-0.860	-0.257	0.370	-0.216					
8	-0.065	0.053	-0.334	-0.329	0.322	-0.143	0.175				
9	0.183	0.137	0.619	0.200	-0.329	0.109	-0.614	-0.627			
10	-0.188	0.316	0.611	0.414	-0.580	0.331	-0.520	-0.556	0.718		
11	-0.021	0.200	0.510	0.310	-0.430	0.178	-0.481	-0.553	0.734	0.749	

VARIABLES	MEANS	CORLFNVT									
1 TO 10	47.691	2.685	14.589	3.602	8.103	0.174	8.154	9.985	2.482	0.835	
11 TO 11	0.356										

VARIABLES	STANDARD DEVIATIONS										
1 TO 10	2.247	0.671	2.329	1.738	1.829	0.033	3.695	1.312	0.847	0.629	
11 TO 11	0.194										

STATISTICS COMPLETED FOR CORLFNVT

PRINCIPAL COMPONENTS ANALYSIS

ALKALI-THOLEIITIC BASALT PROBLEM - HAMBURGER STAND OPTION

PROBLEM NAME CORLFNVT

11 VARIABLES , 5 FACTORS

SYMMETRIC %CORRELATION MATRIX -LOWER HALF -ELEMENT %1, 1 TO ELEMENT % 11, 11

	1	2	3	4	5	6	7	8	9	10	11
1	1.000										
2	-0.146	1.000									
3	0.071	0.296	1.000								
4	-0.359	0.113	0.286	1.000							
5	0.175	-0.015	-0.493	-0.829	1.000						
6	-0.165	0.077	0.312	0.298	-0.338	1.000					
7	-0.301	-0.454	-0.860	-0.257	0.370	-0.216	1.000				
8	-0.065	0.053	-0.334	-0.329	0.322	-0.143	0.175	1.000			
9	0.183	0.137	0.619	0.200	-0.329	0.109	-0.614	-0.627	1.000		
10	-0.188	0.316	0.611	0.414	-0.580	0.331	-0.520	-0.556	0.718	1.000	
11	-0.021	0.200	0.510	0.310	-0.430	0.178	-0.481	-0.553	0.734	0.749	1.000

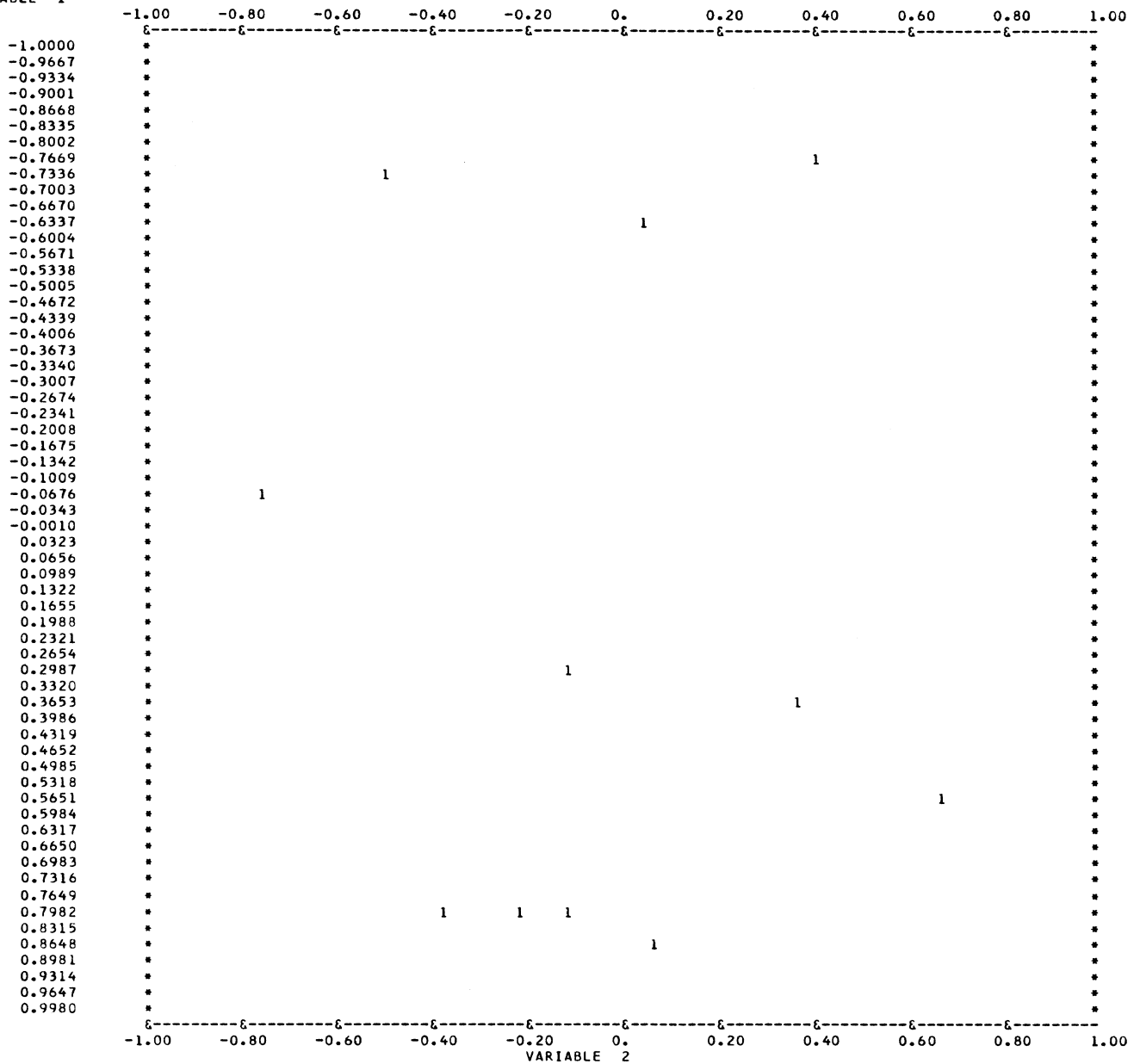
FACTOR NUMBER	TEST NUMBER	FACTOR LOADING	VARIANCE %EIGENVALUE	EIGENVECTOR	ITERATIONS REQUIRED
1	1	-0.04197	4.72366	-0.01931	15
	2	0.32331		0.14876	
	3	0.80859		0.37204	
	4	0.57667		0.26533	
	5	-0.70155		-0.32279	
	6	0.39242		0.18056	
	7	-0.74227		-0.34152	
	8	-0.61390		-0.28246	
	9	0.80193		0.36897	
	10	0.88112		0.40541	
	11	0.79846		0.36738	
2	1	-0.75988	1.76535	-0.57192	30
	2	-0.11348		-0.08541	
	3	-0.22378		-0.16842	
	4	0.65565		0.49346	
	5	-0.49258		-0.37073	
	6	0.35337		0.26596	
	7	0.40775		0.30688	
	8	0.04484		0.03375	
	9	-0.37493		-0.28219	
	10	0.05974		0.04496	
	11	-0.12321		-0.09273	
3	1	-0.17123	1.32522	-0.14874	33
	2	0.73667		0.63993	
	3	0.26339		0.22880	
	4	-0.01092		-0.00948	
	5	0.06151		0.05343	
	6	0.19610		0.17035	
	7	-0.40990		-0.35607	
	8	0.59785		0.51933	
	9	-0.25966		-0.22556	
	10	-0.04904		-0.04260	
	11	-0.21496		-0.18673	
4	1	0.49763	0.98663	0.50099	24
	2	-0.43697		-0.43992	
	3	0.21353		0.21497	
	4	0.17581		0.17699	
	5	-0.33223		-0.33447	
	6	0.33698		0.33926	
	7	-0.24300		-0.24464	
	8	0.16723		0.16836	
	9	-0.13518		-0.13609	
	10	-0.25373		-0.25544	
	11	-0.27920		-0.28109	
5	1	-0.08089	0.79193	-0.09090	20
	2	-0.07207		-0.08099	
	3	0.00798		0.00897	
	4	-0.34130		-0.38352	
	5	0.28473		0.31996	
	6	0.73829		0.82963	
	7	0.11810		0.13271	
	8	-0.10007		-0.11245	
	9	0.02595		0.02917	
	10	0.10597		0.11908	
	11	0.04051		0.04552	

PRINT OUT OF RESIDUAL MATRIX -LOWER HALF -ELEMENT %1, 1 TO ELEMENT % 11, 11

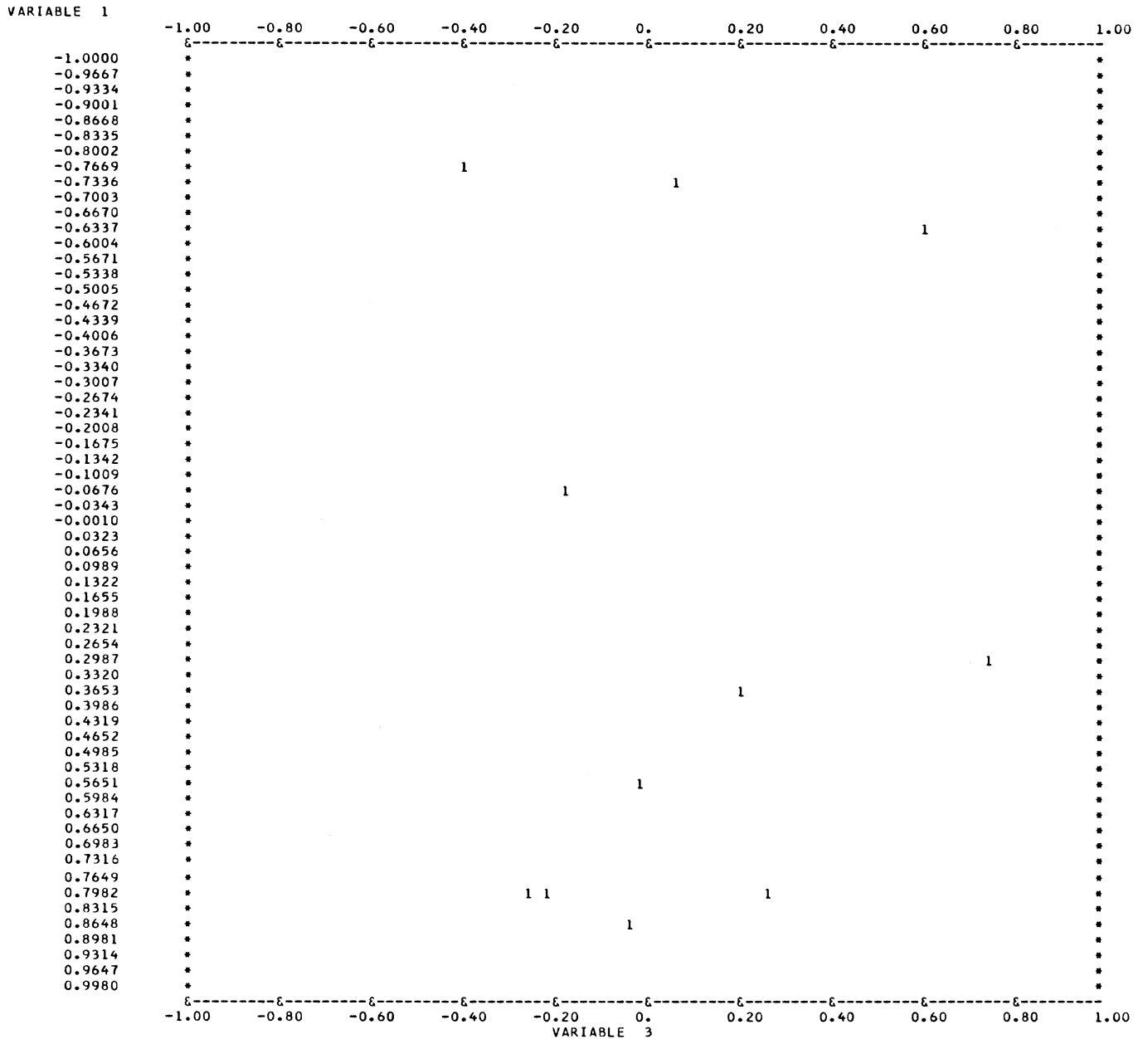
	1	2	3	4	5	6	7	8	9	10	11
1	0.137										
2	0.119	0.144									
3	-0.126	-0.091	0.181								
4	0.046	0.061	-0.065	0.090							
5	-0.030	-0.014	0.017	0.054	0.070						
6	0.046	0.047	-0.056	0.034	0.001	0.024					
7	0.038	0.036	-0.010	-0.017	-0.039	0.006	0.042				
8	-0.045	-0.118	-0.020	-0.062	-0.039	-0.017	-0.001	0.226			
9	-0.043	-0.031	-0.016	0.014	0.012	0.004	-0.008	0.063	0.130		
10	0.021	-0.029	-0.022	-0.053	-0.044	-0.019	0.015	0.065	-0.016	0.142	
11	0.024	-0.033	-0.047	-0.009	-0.022	0.015	0.001	0.122	-0.047	-0.033	0.221

SCATTERGRAM OF FACTOR LOADING
 FACTOR 1 VS. 2

VARIABLE 1

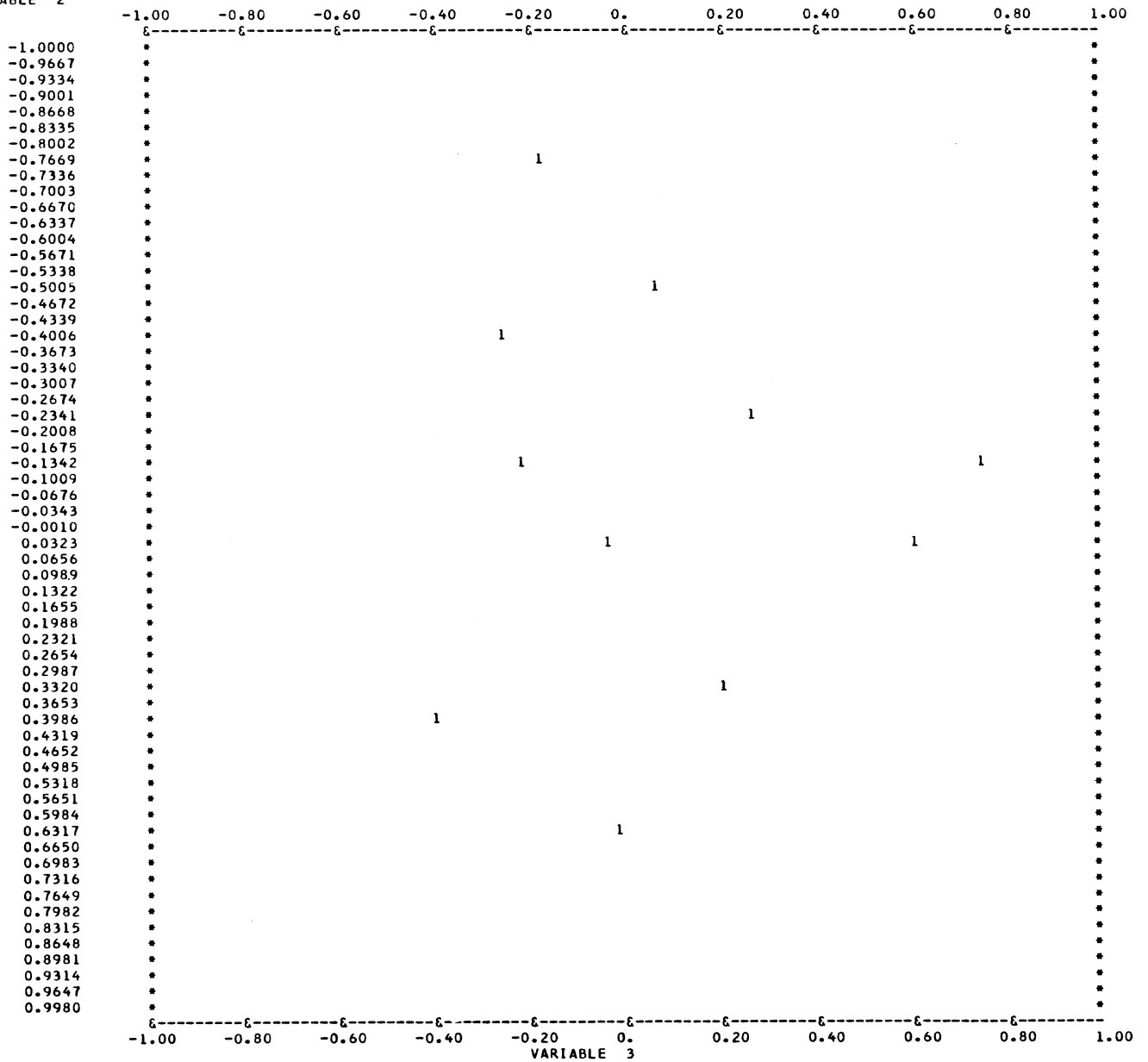


SCATTERGRAM OF FACTOR LOADING
 FACTOR 1 VS. 3



SCATTERGRAM OF FACTOR LOADING
 FACTOR 2 VS. 3

VARIABLE 2



VARIMAX ROTATION

ALKALI-THOLEIITIC BASALT PROBLEM - HAMBURGER STAND OPTION

PROBLEM NAME CORLFNVT 11 VARIABLES , 3 FACTORS

THE ORIGINAL MATRIX OF FACTOR LOADINGS

	F 1	F 2	F 3	F 4	F 5	F 6	F 7	F 8	F 9	F 10
1	-0.04197	-0.75988	-0.17123	0.49763	-0.08089					
2	0.32331	-0.11348	0.73667	-0.43697	-0.07207					
3	0.80859	-0.22378	0.26339	0.21353	0.00798					
4	0.57667	0.65565	-0.01092	0.17581	-0.34130					
5	-0.70155	-0.49258	0.06151	-0.33223	0.28473					
6	0.39242	0.35337	0.19610	0.33698	0.73829					
7	-0.74227	0.40775	-0.40990	-0.24300	0.11810					
8	-0.61390	0.04484	0.59785	0.16723	-0.10007					
9	0.80193	-0.37493	-0.25966	-0.13518	0.02595					
10	0.88112	0.05974	-0.04904	-0.25373	0.10597					
11	0.79846	-0.12321	-0.21496	-0.27920	0.04051					
SUM SQ	4.72366	1.76535	1.32522	0.98663	0.79193					
VAREXP	42.94236	16.04864	12.04744	8.96939	7.19934					
CUMPER	42.94236	58.99100	71.03844	80.00783	87.20717					

COMMUNALITIES

1	0.86269
2	0.85623
3	0.81893
4	0.90993
5	0.93003
6	0.97594
7	0.95823
8	0.77429
9	0.87003
10	0.85795
11	0.77853

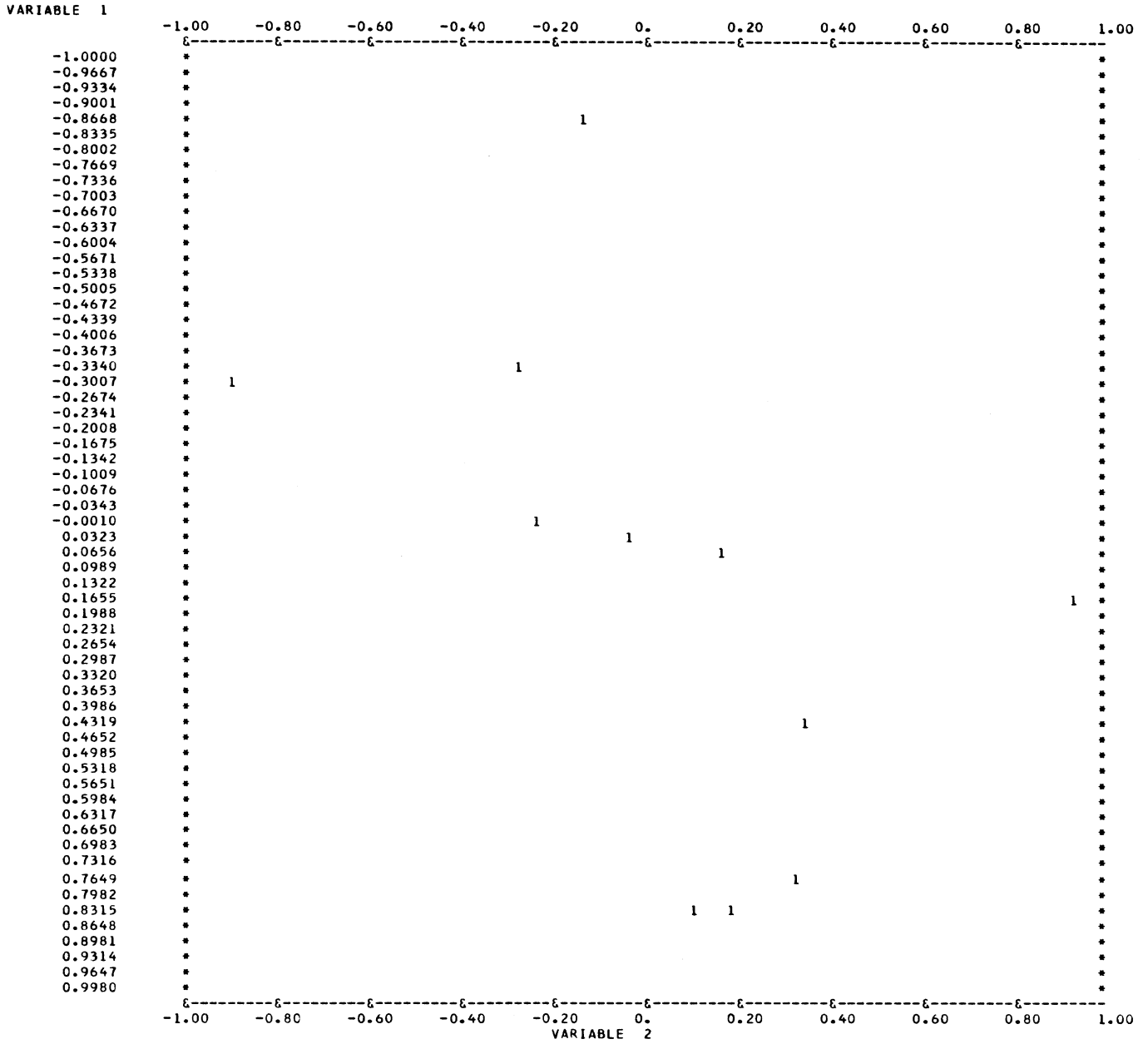
THE ROTATED MATRIX OF FACTOR LOADINGS

	F 1	F 2	F 3	F 4	F 5	F 6	F 7	F 8	F 9	F 10
1	0.02188	-0.24311	-0.15438							
2	0.05417	-0.03730	0.90959							
3	0.43683	0.34162	0.49215							
4	0.17157	0.91300	0.05210							
5	-0.27383	-0.90830	-0.03122							
6	0.09375	0.16972	0.03961							
7	-0.32687	-0.27531	-0.63464							
8	-0.83572	-0.14756	0.23018							
9	0.85753	0.09460	0.18888							
10	0.77234	0.31043	0.33508							
11	0.83380	0.18083	0.21840							
SUM SQ	3.13979	2.10017	1.75007							
VAREXP	28.54359	19.09247	15.90969							
CUMPER	28.54359	47.63605	63.54574							

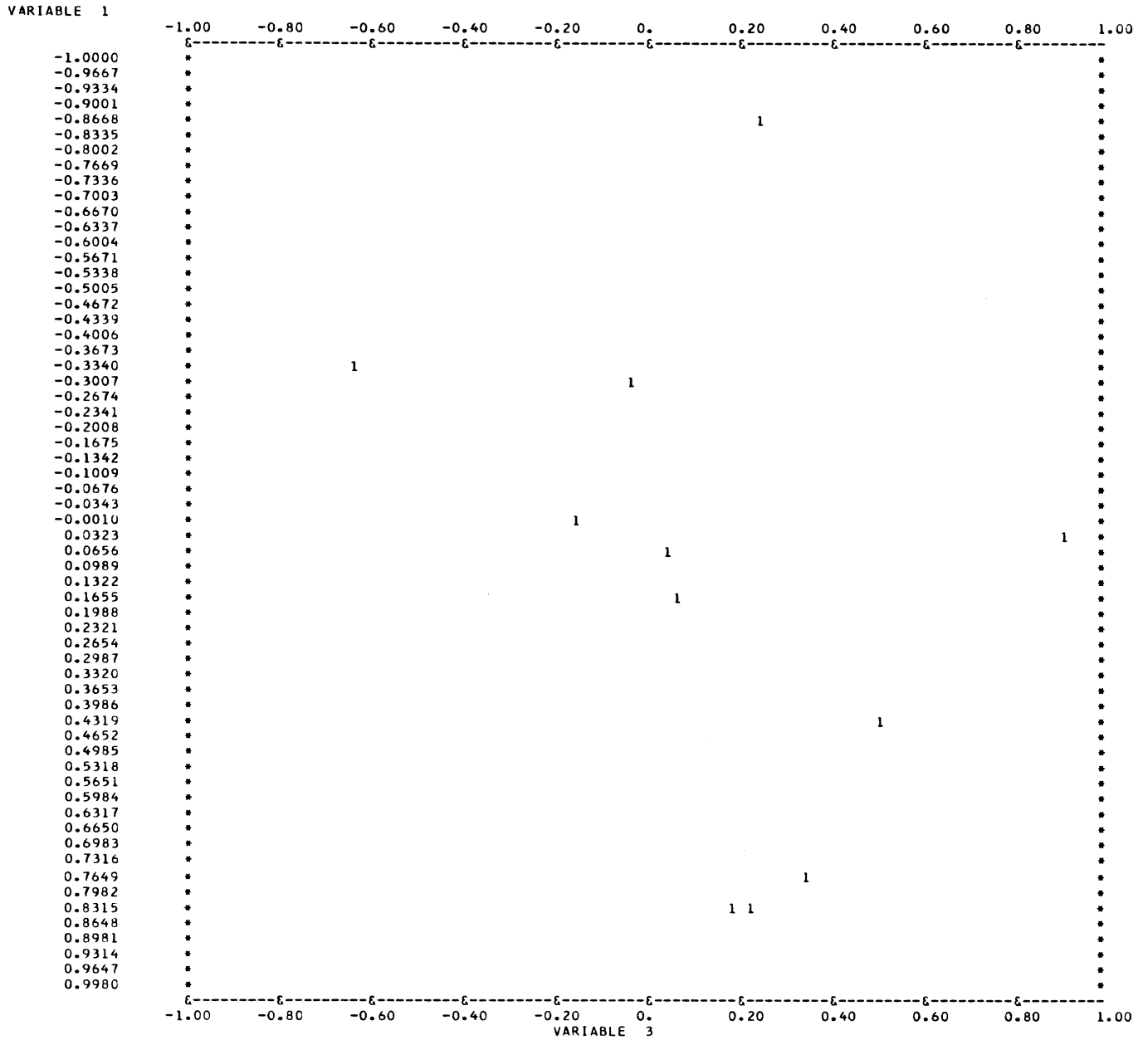
COMMUNALITIES

1	0.08342
2	0.83169
3	0.54974
4	0.86572
5	0.90097
6	0.03916
7	0.58540
8	0.77319
9	0.77998
10	0.80515
11	0.77561

SCATTERGRAM OF ROTATED FACTORS
 FACTOR 1 VS. 2



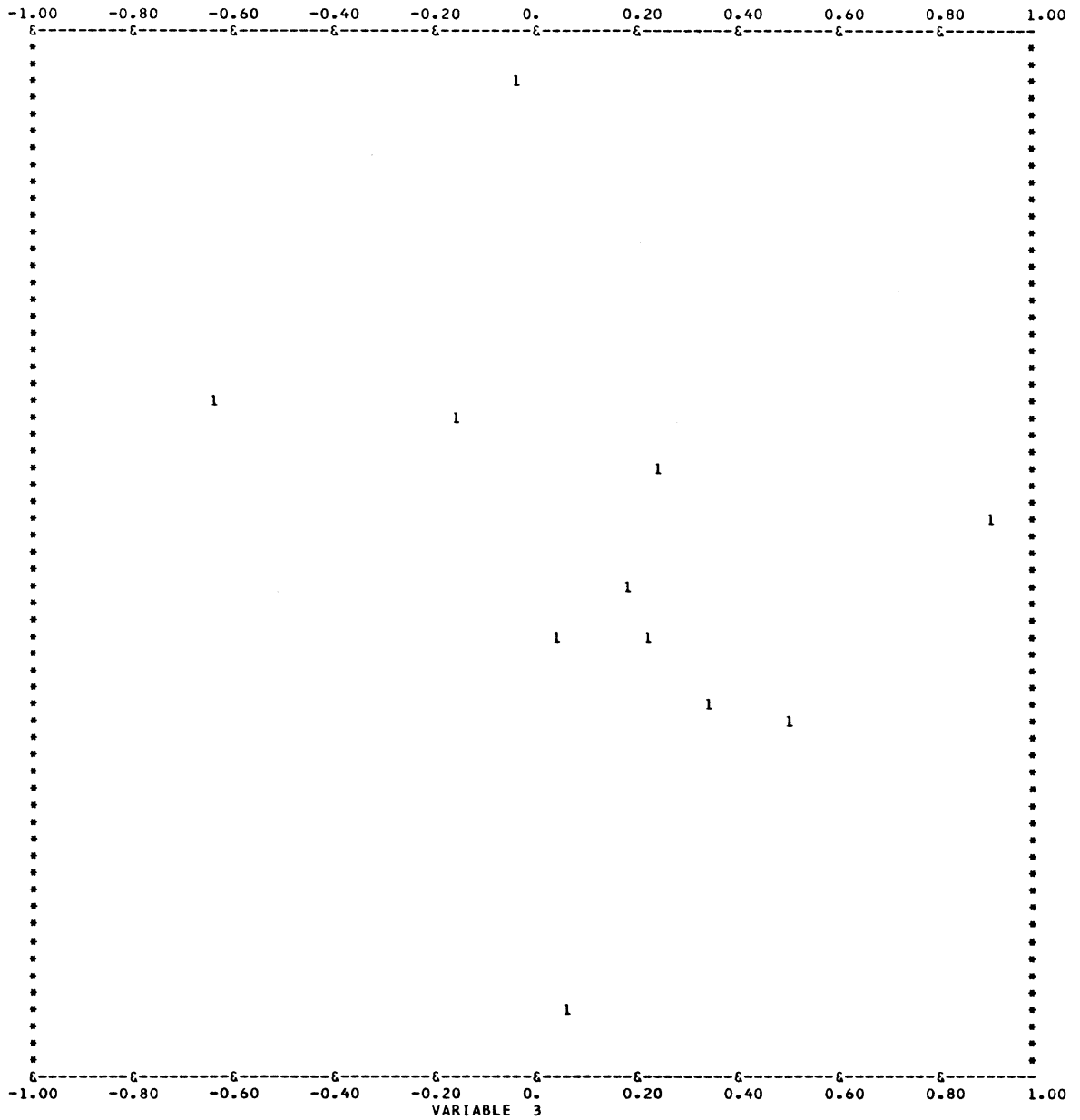
SCATTERGRAM OF ROTATED FACTORS
 FACTOR 1 VS. 3



SCATTERGRAM OF ROTATED FACTORS
 FACTOR 2 VS. 3

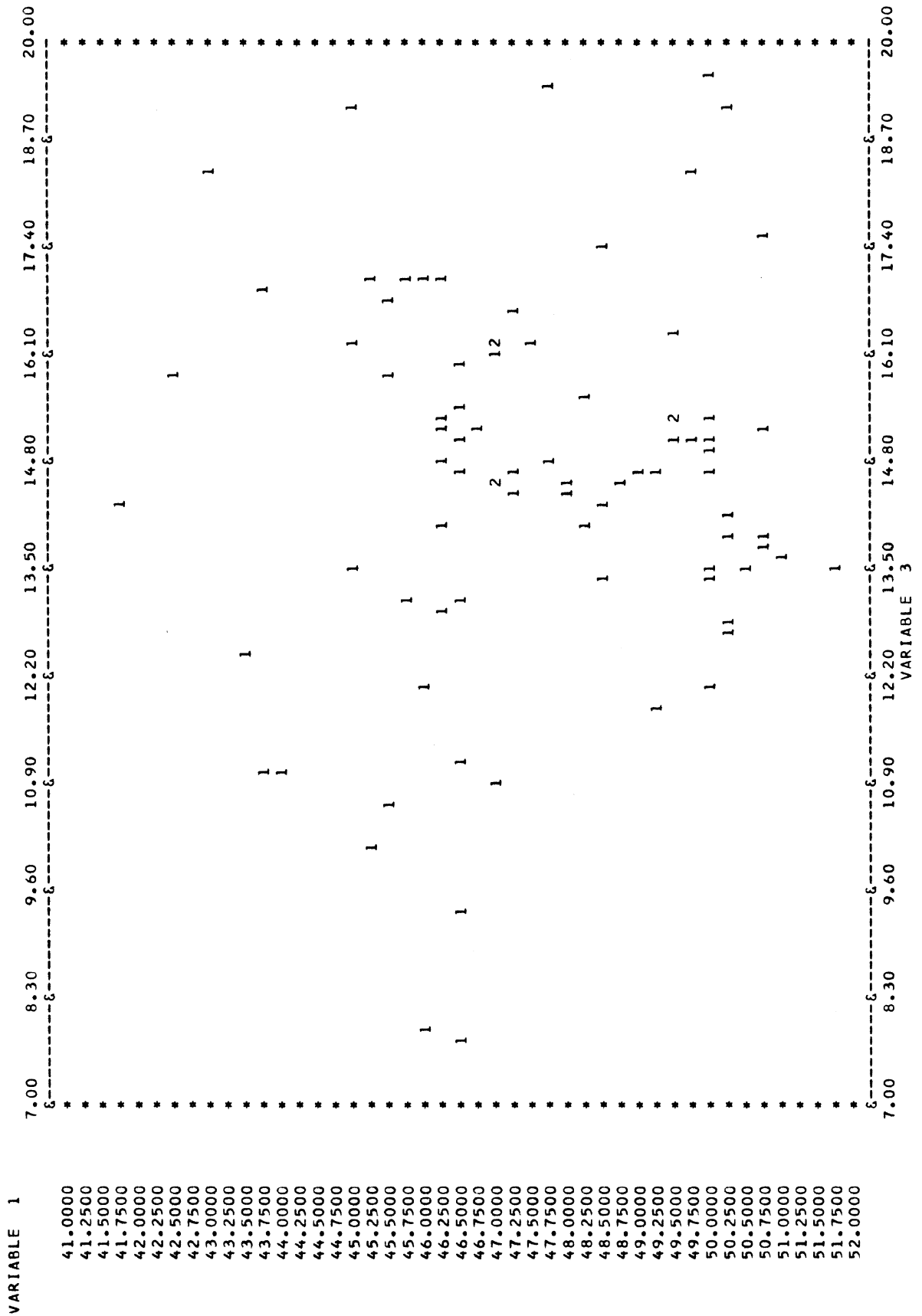
VARIABLE 2

- 1.0000
- 0.9667
- 0.9334
- 0.9001
- 0.8668
- 0.8335
- 0.8002
- 0.7669
- 0.7336
- 0.7003
- 0.6670
- 0.6337
- 0.6004
- 0.5671
- 0.5338
- 0.5005
- 0.4672
- 0.4339
- 0.4006
- 0.3673
- 0.3340
- 0.3007
- 0.2674
- 0.2341
- 0.2008
- 0.1675
- 0.1342
- 0.1009
- 0.0676
- 0.0343
- 0.0010
- 0.0323
- 0.0656
- 0.0989
- 0.1322
- 0.1655
- 0.1988
- 0.2321
- 0.2654
- 0.2987
- 0.3320
- 0.3653
- 0.3986
- 0.4319
- 0.4652
- 0.4985
- 0.5318
- 0.5651
- 0.5984
- 0.6317
- 0.6650
- 0.6983
- 0.7316
- 0.7649
- 0.7982
- 0.8315
- 0.8648
- 0.8981
- 0.9314
- 0.9647
- 0.9980

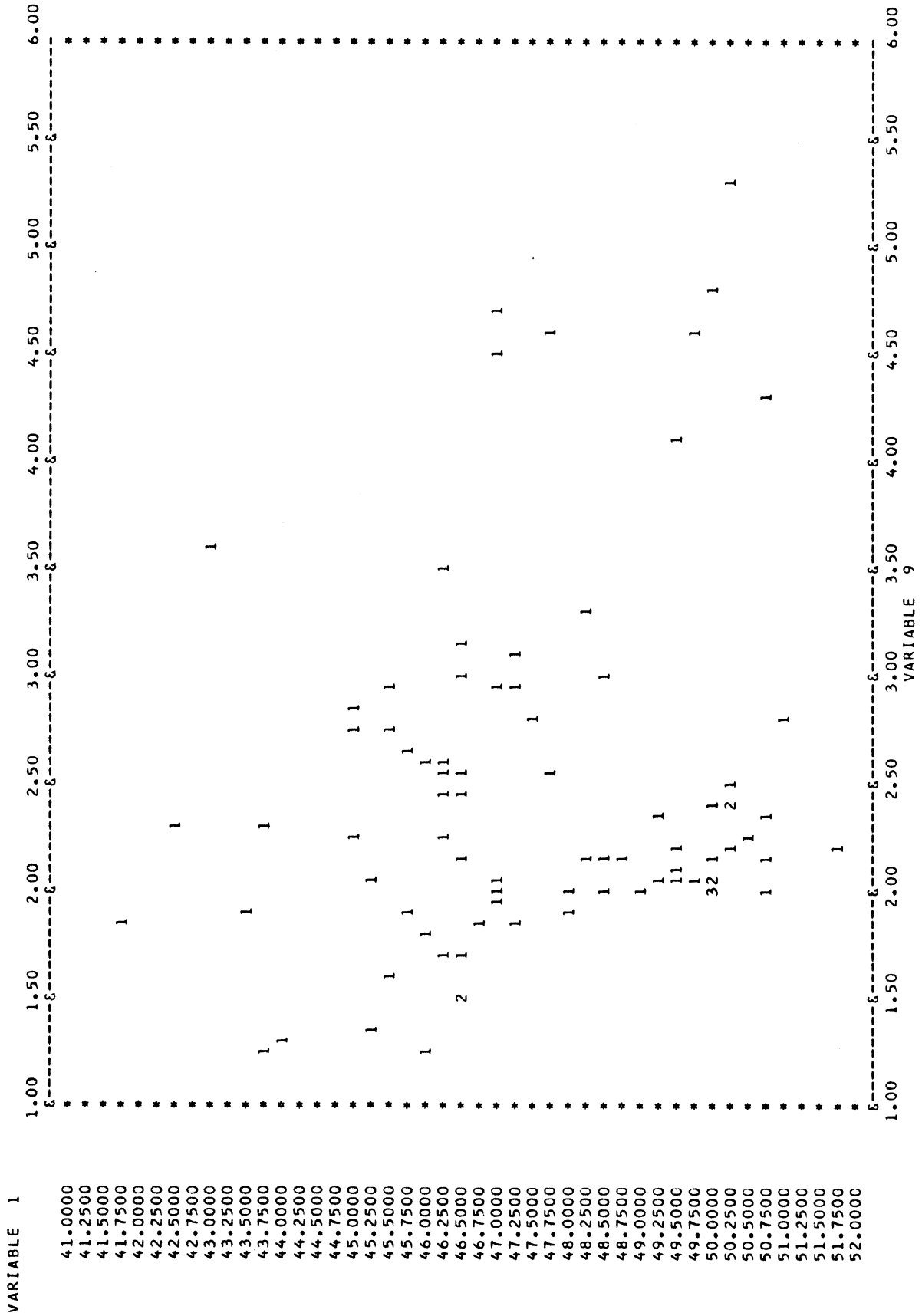


THOLEIITIC + ALKALIC BASALT PROBLEM Q-MODE FACTOR ANALYSIS

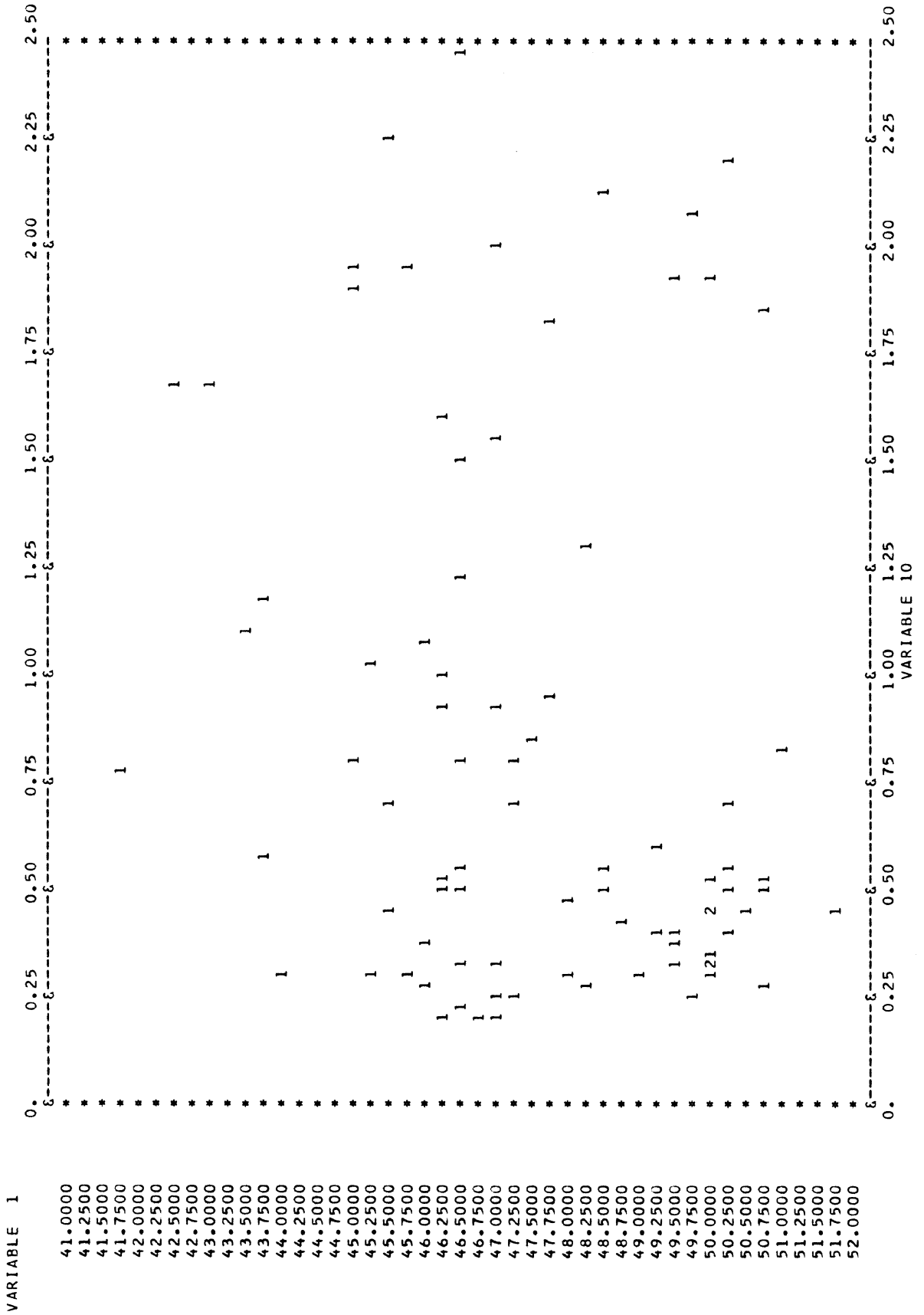
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 1 VS. 3



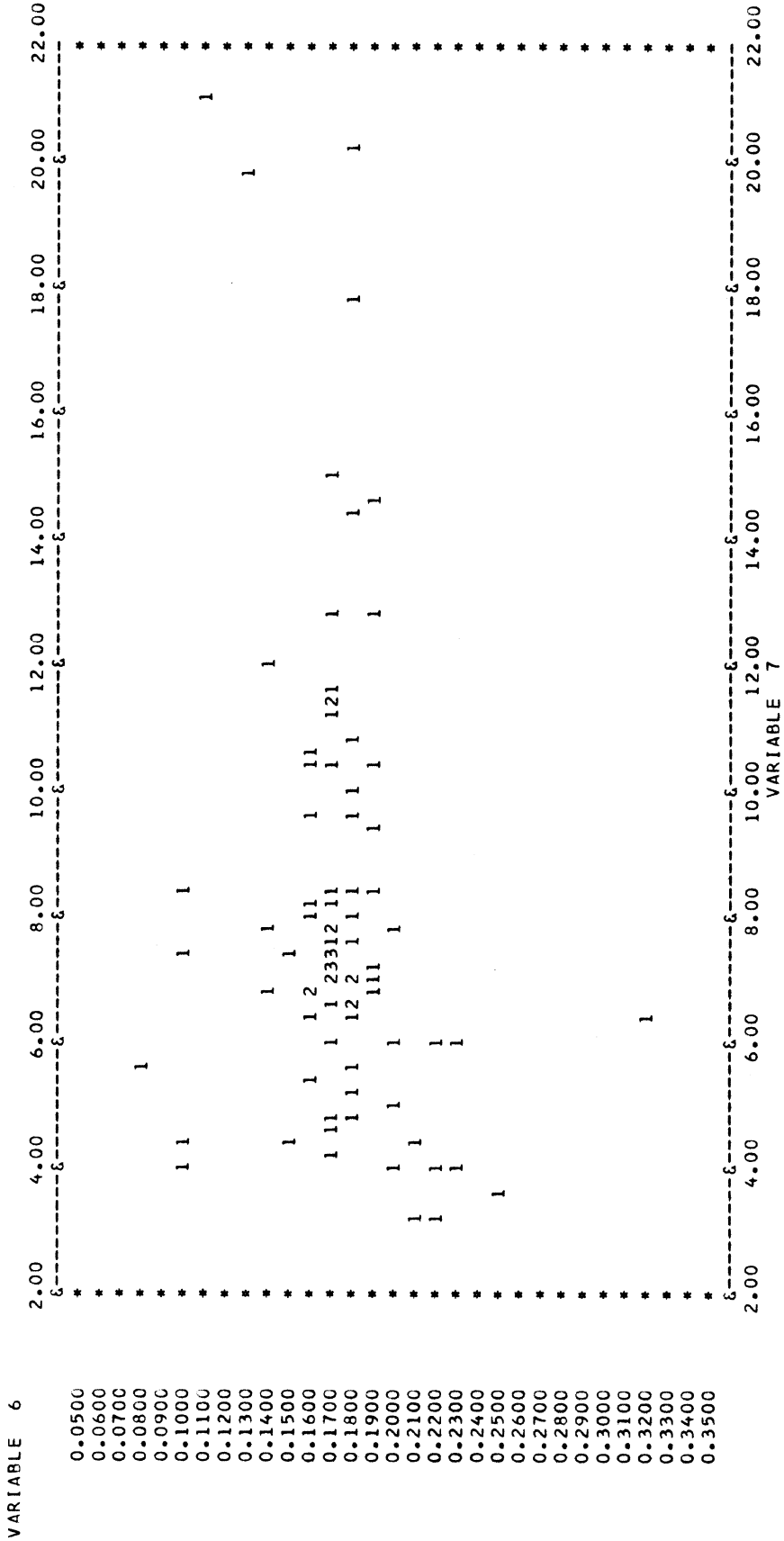
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 1 VS. 9



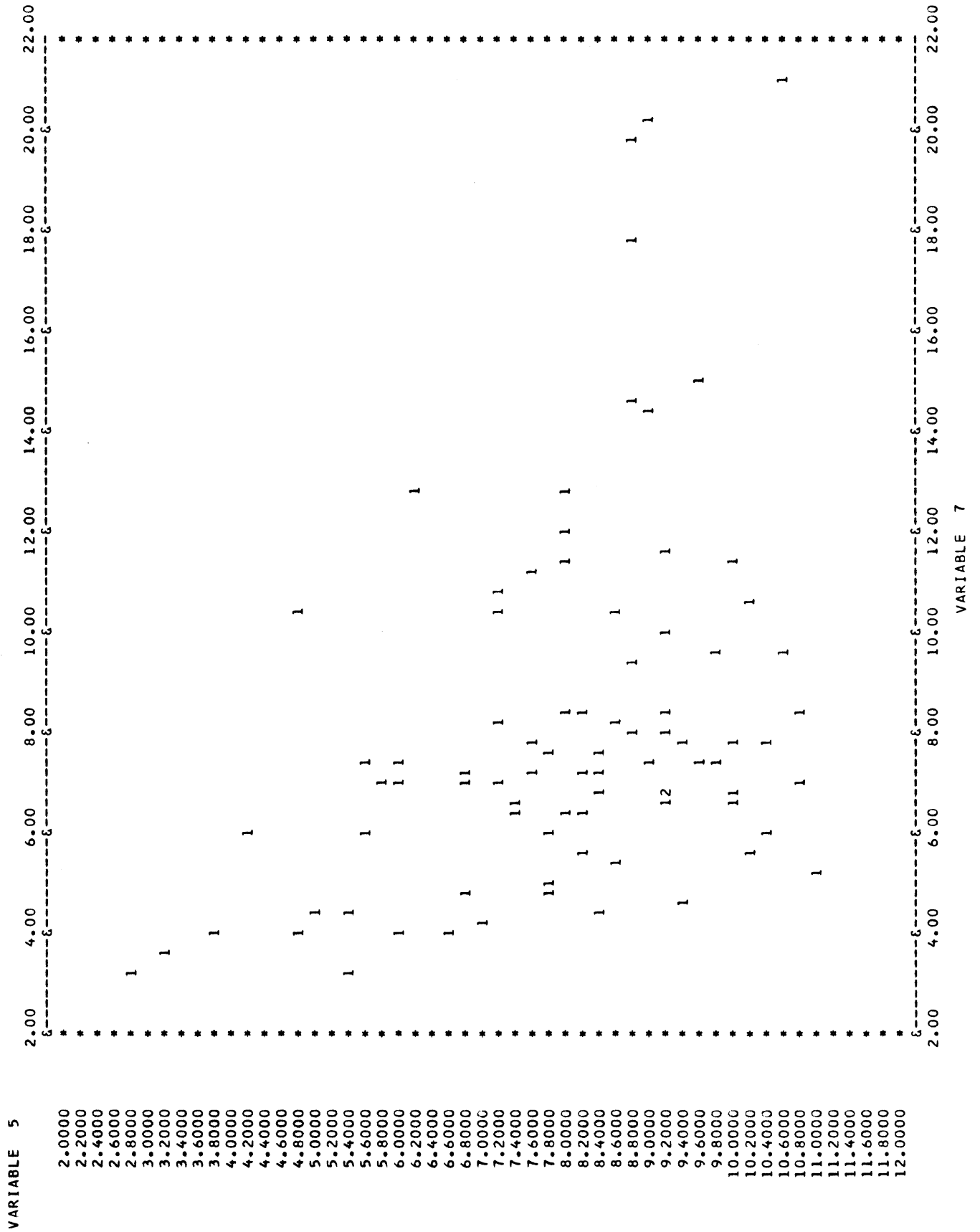
SCATTERGRAM OF ORIGINAL DATA
VARIABLE 1 VS. 10



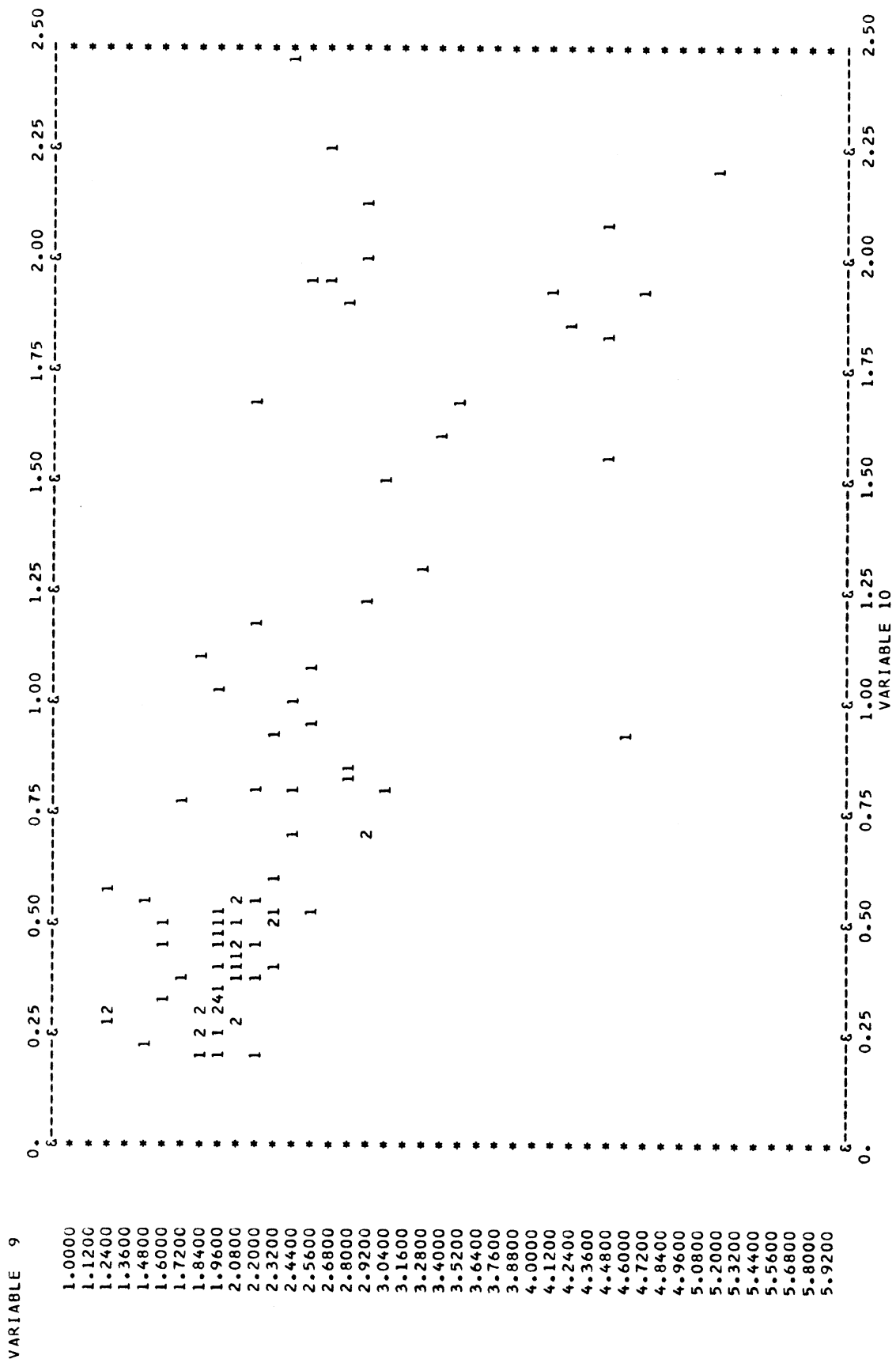
SCATTERGRAM OF ORIGINAL DATA
 VARIABLE 6 VS. 7



SCATTERGRAM OF ORIGINAL DATA
VARIABLE 5 VS. 7



SCATTERGRAM OF ORIGINAL DATA
VARIABLE 9 VS. 10



PROBLEM NAME QMODFVNT

IN 1	50.2500	2.1200	19.0300	4.5300	5.5000	0.2200	3.1100	5.9800	5.3000	2.2000	1.1400
IN 2	45.7400	4.1600	16.7600	9.3900	2.8300	0.2100	3.2400	9.0200	2.7300	2.2400	0.6100
IN 3	49.7300	3.0500	16.3900	7.5800	3.9800	0.2300	4.0600	7.1700	4.1200	1.9300	0.8400
IN 4	49.7900	2.5100	18.3700	6.0300	4.8200	0.2200	4.0100	6.6800	4.5800	2.0800	0.5600
IN 5	47.9900	2.6200	19.3600	5.8300	5.1700	0.2100	4.3900	6.5400	4.5800	1.8200	0.6300
IN 6	45.9400	3.0000	17.0400	7.8100	3.2800	0.2500	3.6700	10.1400	2.6300	1.9400	0.5500
IN 7	46.5200	2.7800	16.0000	5.5600	4.2000	0.2300	6.0900	10.4000	2.4500	2.4500	0.5000
IN 8	45.1000	0.7000	19.0500	5.3700	5.7300	0.2200	6.0300	7.0600	2.8500	1.9000	0.6600
IN 9	47.2000	3.8500	16.2200	5.2000	6.9500	0.1800	4.7700	8.4900	2.9300	2.0000	0.7400
IN 10	50.9200	2.5500	17.5900	3.8000	6.6900	0.2000	3.9000	6.9700	4.2800	1.8600	0.4000
IN 11	50.0900	2.4700	19.4900	0.7300	8.4700	0.1500	4.3300	6.9200	4.8200	1.9300	0.7800
IN 12	47.0300	1.9200	16.2200	5.5300	6.0700	0.1000	4.0000	8.0800	4.5000	1.5400	0.2400
IN 13	46.6800	4.2000	15.0100	6.3500	5.4400	0.1000	4.3000	9.8400	3.1300	1.5100	0.4700
IN 14	48.6500	3.8000	17.4300	2.8000	7.1200	0.1700	4.1400	9.7200	2.9800	2.1300	0.5200
IN 15	45.2400	3.2200	16.1700	4.5200	6.8600	0.1900	7.0100	9.7600	2.7500	1.9500	0.4800
IN 16	43.0400	4.0000	18.2600	2.9100	7.8200	0.2000	4.9500	9.8000	3.6200	1.6700	0.5500
IN 17	46.4200	1.5800	15.2800	2.2200	5.9300	0.1700	7.0600	11.4800	3.4900	1.6100	0.7800
IN 18	48.4200	3.2500	13.9700	4.1700	9.5700	0.1700	4.6100	8.8600	3.3000	1.2900	0.9100
IN 19	43.5800	3.3000	12.4900	8.4100	4.9200	0.1900	10.3300	9.3400	1.9100	1.1000	0.2400
IN 20	46.5100	2.9800	15.4800	3.4100	8.6800	0.1700	8.1700	8.8500	3.0000	1.2200	0.5900
IN 21	42.6000	3.7900	15.8900	2.8600	8.3400	0.1800	8.4500	9.8800	2.3000	1.6700	0.4400
IN 22	45.6000	3.1900	15.8900	5.9800	7.5400	0.1700	6.5600	9.4900	2.9500	0.7000	0.4000
IN 23	47.7200	2.4800	16.1900	3.8200	8.2500	0.0800	5.6800	11.2000	2.8000	0.8400	0.4300
IN 24	43.7500	4.2500	16.9200	1.8200	9.3000	0.1800	6.7000	10.8200	2.2900	1.1800	0.3900
IN 25	46.4900	3.0900	17.0700	5.3500	7.8400	0.1700	4.8000	10.5200	2.6100	0.5200	0.3500
IN 26	46.0500	2.6500	17.0300	3.9000	7.4700	0.3200	6.3000	11.2400	2.6000	1.0700	0.
IN 27	46.4300	3.0300	15.2200	3.9700	8.1900	0.1000	8.4000	10.3700	2.5500	0.9900	0.3300
IN 28	47.3200	3.0900	16.6800	2.6300	8.6700	0.1600	5.4300	11.2700	3.0800	0.7900	0.5300
IN 29	50.0400	2.2200	15.3600	5.3900	5.7800	0.1700	7.3200	10.1700	2.0200	0.3300	0.3100
IN 30	45.2500	4.0000	17.0600	2.3000	8.4200	0.1800	7.5500	11.0800	2.0500	1.0300	0.2700
IN 31	47.1900	2.2700	10.9500	3.3100	10.2100	0.1600	10.5200	9.7300	4.6900	0.9300	0.5500
IN 32	47.4200	3.4600	14.3500	3.4100	10.3300	0.1800	5.5700	9.8000	2.9500	0.6900	0.4300
IN 33	46.6500	3.2200	14.7200	3.6300	8.9800	0.1800	7.9600	10.1400	2.5300	0.8000	0.3300
IN 34	51.2400	3.7400	13.6000	1.8700	11.1900	0.1800	5.1200	9.0300	2.8100	0.8300	0.4100
IN 35	41.8300	3.1600	14.3200	4.8100	8.9800	0.1900	9.4200	8.8300	1.8300	0.7700	0.2900
IN 36	48.5500	2.8300	14.2900	4.8900	8.0400	0.1800	6.4200	10.7600	2.1500	0.5500	0.2800
IN 37	48.1700	2.4400	14.4600	5.5800	6.0500	0.1800	6.9900	11.0300	1.8800	0.2900	0.2000
IN 38	49.5000	2.1000	15.3800	4.5100	6.9900	0.1700	7.2300	10.4400	2.1000	0.3900	0.2800
IN 39	46.9100	2.4400	15.2300	5.5400	6.1800	0.1700	7.3800	10.9000	1.8500	0.1900	0.2000
IN 40	47.7900	1.9000	14.8000	2.6300	10.0400	0.1400	6.8900	11.3100	2.5600	0.9400	0.2600
IN 41	50.0200	2.2300	15.0500	3.7700	7.3700	0.1700	7.0100	10.1700	2.0500	0.3300	0.2700
IN 42	49.8600	2.4300	15.1100	3.6600	7.8200	0.1700	6.0000	10.3400	2.0500	0.2600	0.2700
IN 43	48.2900	2.5600	15.5400	3.2700	7.8800	0.1700	7.7000	10.2100	2.1700	0.2800	0.2700
IN 44	50.4000	3.2600	13.9100	1.8000	10.0900	0.1800	6.5700	10.6500	2.5200	0.6900	0.3000
IN 45	45.7700	2.4700	13.1600	2.9700	9.2700	0.1700	11.6400	10.2300	1.8800	0.2900	0.2400
IN 46	45.1400	3.0400	13.4900	3.6000	9.2700	0.1800	10.0200	10.6000	2.2400	0.8000	0.2600
IN 47	49.4200	2.4200	11.8300	3.8300	8.0800	0.1400	12.0400	9.2800	2.3500	0.5900	0.3900
IN 48	49.6900	2.6000	15.2600	3.1600	8.3500	0.1600	6.5000	10.7800	2.2000	0.3700	0.2500
IN 49	43.9600	2.3600	11.0600	5.2900	6.3700	0.1900	12.8800	11.8800	1.2600	0.5700	0.3200
IN 50	50.2000	2.1500	14.7200	3.3800	7.7900	0.1700	7.8800	9.8100	2.0000	0.3600	0.2700
IN 51	50.2000	2.4000	14.9300	3.6400	7.6700	0.1700	7.1500	10.1600	2.0500	0.3000	0.2700
IN 52	48.2400	3.0900	14.4800	3.5800	10.4200	0.2000	6.0500	10.0200	2.0000	0.4800	0.3000
IN 53	50.8000	1.9300	15.2500	2.9100	7.2300	0.1600	8.2700	9.8300	2.1500	0.2800	0.2500
IN 54	48.8400	2.5800	14.5900	2.7800	8.4500	0.1700	7.2500	10.9000	2.1500	0.4200	0.3300
IN 55	49.6700	2.3300	15.0800	2.8600	8.5700	0.1600	6.7600	10.5100	2.0600	0.3200	0.2600
IN 56	47.1200	2.3400	14.5100	4.3900	7.2100	0.1800	10.7400	10.3600	1.9400	0.2500	0.2500
IN 57	46.3900	2.1300	12.9400	2.0500	10.1600	0.1700	11.3800	10.8100	2.4300	0.9300	0.3200
IN 58	48.5700	2.6100	13.3400	2.9500	8.6600	0.1700	10.4100	10.2600	2.0200	0.5000	0.2600
IN 59	46.3100	3.1000	14.8300	4.0600	9.2600	0.1900	6.7700	11.3000	2.2500	0.2000	0.2500
IN 60	47.2500	2.1600	14.7000	3.9100	7.2700	0.1600	10.4600	10.2200	1.8600	0.2400	0.2500
IN 61	47.1000	2.3100	16.0500	3.1200	8.2700	0.1900	7.1200	11.9100	2.0000	0.1900	0.2600
IN 62	50.8700	2.8600	13.9400	1.8500	9.0700	0.1700	7.3500	11.0900	2.3400	0.4900	0.2500
IN 63	49.3700	2.5000	14.7300	1.7100	9.3900	0.1600	6.8700	10.8600	2.0500	0.4000	0.2700
IN 64	51.7700	4.0100	13.5400	0.7500	9.6300	0.1500	7.3300	10.5700	2.1800	0.4500	0.2600
IN 65	46.4300	2.2900	14.0000	3.3400	8.1700	0.1700	11.4100	11.8600	1.6900	0.4900	0.2500
IN 66	50.0700	2.7000	13.3200	1.9200	9.2800	0.1600	8.0100	10.6400	2.1600	0.4500	0.2600
IN 67	50.3200	3.1000	12.8300	1.7400	9.9300	0.1000	7.3900	11.0600	2.3800	0.4100	0.3000
IN 68	50.6800	2.5400	13.5500	1.3900	9.3500	0.1700	8.4700	10.9800	2.2400	0.4500	0.2600
IN 69	49.0700	2.4800	14.6200	2.0000	9.5200	0.1700	7.8000	10.3800	2.0100	0.3100	0.2800
IN 70	47.1400	2.8800	14.5700	2.0900	10.8500	0.1900	8.3500	10.0900	2.0300	0.3300	0.3100
IN 71	46.1900	2.1500	12.0200	4.0800	8.1900	0.1700	12.7500	10.7300	1.7900	0.3800	0.2000
IN 72	50.2400	2.9200	13.4600	1.1700	10.9400	0.1800	7.0400	10.3000	2.4000	0.5200	0.1700
IN 73	50.8800	2.5900	13.7500	0.7300	10.4200	0.2000	7.7700	10.7600	2.0000	0.5200	0.2400
IN 74	50.0300	2.5700	12.1000	2.1000	9.9700	0.1600	9.5700	10.5800	2.0100	0.4400	0.2100
IN 75	50.3700	2.3300	14.2000	1.2800	10.1000	0.1400	7.7500	11.2400	2.2000	0.5600	0.0200
IN 76	50.4600	2.1400	12.7500	0.8200	10.6800	0.1800	9.6800	10.4300	2.4200	0.5100	0.1900
IN 77	45.6400	2.3400	10.6100	3.0200	9.0200	0.1800	14.3200	10.8800	1.6200	0.4600	0.2500
IN 78	44.2400	2.3400	11.0100	3.3600	8.9700	0.1900	14.6700	10.3600	1.3200	0.3000	0.2500
IN 79	46.6000	2.1500	11.2100	2.0400	9.6100	0.1700	15.0100	10.6000	1.5200	0.5600	0.1800
IN 80	45.3000	1.8500	10.1100	3.7500	8.9100	0.1800	17.8700	8.9600	1.3500	0.3000	0.2000
IN 81	46.5700	1.6700	7.8100	2.4000	8.9100	0.1300	19.7400	10.6500	1.7000	0.3300	0.3400
IN 82	46.0100	1.6100	7.9600	2.5400	9.0900	0.1800	20.1900	10.4900	1.2600	0.2700	0.1700
IN 83	46.5000	1.7000	9.3700	2.4700	10.7900	0.1100	21.0000	6.2500	1.5200	0.2200	0.1000
IN 84	46.6800	1.9100	13.1500	4.7100	7.6200	0.1700	11.1200	9.6800	2.1500	0.4900	0.2200

PROBLEM NAME QMODFNVT

DIV	1	0.97064	0.49882	0.97640	0.48243	0.49151	0.68750	0.14810	0.50210	1.00000	0.89796	1.00000	0.	0.
DIV		0.												
DIV	2	0.88352	0.97882	0.85993	1.00000	0.25290	0.65625	0.15429	0.75735	0.51509	0.91429	0.53509	0.	0.
DIV		0.												
DIV	3	0.96059	0.71765	0.84094	0.80724	0.35567	0.71875	0.19333	0.60202	0.77736	0.78776	0.73684	0.	0.
DIV		0.												
DIV	4	0.96175	0.59059	0.94253	0.64217	0.43074	0.68750	0.19095	0.56087	0.86415	0.84898	0.49123	0.	0.
DIV		0.												
DIV	5	0.92698	0.61647	0.99333	0.62087	0.46202	0.65625	0.20905	0.54912	0.86415	0.74286	0.55263	0.	0.
DIV		0.												
DIV	6	0.88739	0.70588	0.87429	0.83174	0.29312	0.78125	0.17476	0.85139	0.49623	0.79184	0.48246	0.	0.
DIV		0.												
DIV	7	0.89859	0.65412	0.82093	0.59212	0.37534	0.71875	0.29000	0.87322	0.46226	1.00000	0.43860	0.	0.
DIV		0.												
DIV	8	0.87116	0.16471	0.97742	0.57188	0.51206	0.68750	0.28714	0.59278	0.53774	0.77551	0.57895	0.	0.
DIV		0.												
DIV	9	0.91172	0.90588	0.83222	0.55378	0.62109	0.56250	0.22714	0.71285	0.55283	0.81633	0.64912	0.	0.
DIV		0.												
DIV	10	0.98358	0.60000	0.90251	0.40469	0.59786	0.62500	0.18571	0.58522	0.80755	0.75918	0.35088	0.	0.
DIV		0.												
DIV	11	0.96755	0.58118	1.00000	0.07774	0.75693	0.46875	0.20619	0.58102	0.90943	0.78776	0.68421	0.	0.
DIV		0.												
DIV	12	0.90844	0.45176	0.83222	0.58892	0.54245	0.31250	0.19048	0.67842	0.84906	0.62857	0.21053	0.	0.
DIV		0.												
DIV	13	0.90168	0.98824	0.77014	0.67625	0.48615	0.31250	0.20476	0.82620	0.59057	0.61633	0.41228	0.	0.
DIV		0.												
DIV	14	0.93973	0.89412	0.89430	0.29819	0.63628	0.53125	0.19714	0.81612	0.56226	0.86939	0.45614	0.	0.
DIV		0.												
DIV	15	0.87387	0.75765	0.82966	0.48136	0.61305	0.59375	0.33381	0.81948	0.51887	0.79592	0.42105	0.	0.
DIV		0.												
DIV	16	0.83137	0.94118	0.93689	0.30990	0.69884	0.62500	0.23571	0.82284	0.68302	0.68163	0.48246	0.	0.
DIV		0.												
DIV	17	0.89666	0.37176	0.78399	0.23642	0.52994	0.53125	0.33619	0.96390	0.65849	0.65714	0.68421	0.	0.
DIV		0.												
DIV	18	0.93529	0.76471	0.71678	0.44409	0.85523	0.53125	0.21952	0.74391	0.62264	0.52653	0.79825	0.	0.
DIV		0.												
DIV	19	0.84180	0.77647	0.64084	0.89563	0.43968	0.59375	0.49190	0.78421	0.36038	0.44898	0.21053	0.	0.
DIV		0.												
DIV	20	0.89840	0.70118	0.79425	0.36315	0.77569	0.53125	0.38905	0.74307	0.56604	0.49796	0.51754	0.	0.
DIV		0.												
DIV	21	0.82287	0.89176	0.81529	0.30458	0.74531	0.56250	0.40238	0.82955	0.43396	0.68163	0.38596	0.	0.
DIV		0.												
DIV	22	0.88082	0.75059	0.81529	0.63685	0.67382	0.53125	0.31238	0.79681	0.55660	0.28571	0.35088	0.	0.
DIV		0.												
DIV	23	0.92177	0.58353	0.83068	0.40682	0.73727	0.25000	0.27048	0.94039	0.52830	0.34286	0.37719	0.	0.
DIV		0.												
DIV	24	0.84508	1.00000	0.86814	0.19382	0.83110	0.56250	0.31905	0.90848	0.43208	0.48163	0.34211	0.	0.
DIV		0.												
DIV	25	0.89801	0.72706	0.87583	0.56976	0.70063	0.53125	0.22857	0.88329	0.49245	0.21224	0.30702	0.	0.
DIV		0.												
DIV	26	0.88951	0.62353	0.87378	0.41534	0.66756	1.00000	0.30000	0.94374	0.49057	0.43673	0.	0.	0.
DIV		0.												
DIV	27	0.89685	0.71294	0.78091	0.42279	0.73190	0.31250	0.40000	0.87070	0.48113	0.40408	0.28947	0.	0.
DIV		0.												
DIV	28	0.91404	0.72706	0.85582	0.28009	0.77480	0.50000	0.25857	0.94626	0.58113	0.32245	0.46491	0.	0.
DIV		0.												
DIV	29	0.96658	0.52235	0.78810	0.57401	0.51653	0.53125	0.34857	0.85390	0.38113	0.13469	0.27193	0.	0.
DIV		0.												
DIV	30	0.87406	0.94118	0.87532	0.24494	0.75246	0.56250	0.35952	0.93031	0.38679	0.42041	0.23684	0.	0.
DIV		0.												
DIV	31	0.91153	0.53412	0.56183	0.35250	0.91242	0.50000	0.50095	0.81696	0.88491	0.37959	0.48246	0.	0.
DIV		0.												
DIV	32	0.91597	0.81412	0.73628	0.36315	0.92315	0.56250	0.26524	0.82284	0.55660	0.28163	0.37719	0.	0.
DIV		0.												
DIV	33	0.90110	0.75765	0.75526	0.38658	0.80250	0.56250	0.37905	0.85139	0.47736	0.32653	0.28947	0.	0.
DIV		0.												
DIV	34	0.98976	0.88000	0.69779	0.19915	1.00000	0.56250	0.24381	0.75819	0.53019	0.33878	0.35965	0.	0.
DIV		0.												
DIV	35	0.80800	0.74353	0.73474	0.51225	0.80250	0.59375	0.44857	0.74139	0.34528	0.31429	0.25439	0.	0.
DIV		0.												
DIV	36	0.93780	0.66588	0.73320	0.52077	0.71850	0.56250	0.30571	0.90344	0.40566	0.22449	0.24561	0.	0.
DIV		0.												
DIV	37	0.93046	0.57412	0.74192	0.59425	0.54066	0.56250	0.33286	0.92611	0.35472	0.11837	0.17544	0.	0.
DIV		0.												
DIV	38	0.95615	0.49412	0.78912	0.48030	0.62466	0.53125	0.34429	0.87657	0.39623	0.15918	0.24561	0.	0.
DIV		0.												
DIV	39	0.90612	0.57412	0.78143	0.58999	0.55228	0.53125	0.35143	0.91520	0.34906	0.07755	0.17544	0.	0.
DIV		0.												
DIV	40	0.92312	0.44706	0.75936	0.28009	0.89723	0.43750	0.32810	0.94962	0.48302	0.38367	0.22807	0.	0.
DIV		0.												
DIV	41	0.96620	0.52471	0.77219	0.40149	0.65862	0.53125	0.33381	0.85390	0.38679	0.13469	0.23684	0.	0.
DIV		0.												
DIV	42	0.96311	0.57176	0.77527	0.38978	0.69884	0.53125	0.28571	0.86818	0.38679	0.10612	0.23684	0.	0.
DIV		0.												
DIV	43	0.93278	0.60235	0.79733	0.34824	0.70420	0.53125	0.36667	0.85726	0.40943	0.11429	0.23684	0.	0.
DIV		0.												
DIV	44	0.97354	0.76706	0.71370	0.19169	0.90170	0.56250	0.31286	0.89421	0.47547	0.28163	0.26316	0.	0.
DIV		0.												
DIV	45	0.88410	0.58118	0.67522	0.31629	0.82842	0.53125	0.55429	0.85894	0.35472	0.11837	0.21053	0.	0.
DIV		0.												

DIV 46	0.87193	0.71529	0.69215	0.38339	0.82842	0.56250	0.47714	0.89001	0.42264	0.32653	0.22807	0.	0.
DIV 0.													
DIV 47	0.95461	0.56941	0.60698	0.40788	0.72207	0.43750	0.57333	0.77918	0.44340	0.24082	0.34211	0.	0.
DIV 0.													
DIV 48	0.95982	0.61176	0.78297	0.33653	0.74620	0.50000	0.30952	0.90512	0.41509	0.15102	0.21930	0.	0.
DIV 0.													
DIV 49	0.84914	0.55529	0.56747	0.56337	0.56926	0.59375	0.61333	0.99748	0.23774	0.23265	0.28070	0.	0.
DIV 0.													
DIV 50	0.96967	0.50588	0.75526	0.35996	0.69616	0.53125	0.37524	0.82368	0.37736	0.14694	0.23684	0.	0.
DIV 0.													
DIV 51	0.96967	0.56471	0.76603	0.38765	0.68543	0.53125	0.34048	0.85306	0.38679	0.12245	0.23684	0.	0.
DIV 0.													
DIV 52	0.93181	0.72706	0.74295	0.38126	0.93119	0.62500	0.28810	0.84131	0.37736	0.19592	0.26316	0.	0.
DIV 0.													
DIV 53	0.98126	0.45412	0.78245	0.30990	0.64611	0.50000	0.39381	0.82536	0.40566	0.11429	0.21930	0.	0.
DIV 0.													
DIV 54	0.94340	0.60706	0.74859	0.29606	0.75514	0.53125	0.34524	0.91520	0.40566	0.17143	0.28947	0.	0.
DIV 0.													
DIV 55	0.95944	0.54824	0.77373	0.30458	0.76586	0.50000	0.32190	0.88245	0.38868	0.13061	0.22807	0.	0.
DIV 0.													
DIV 56	0.91018	0.55059	0.74448	0.46752	0.64433	0.56250	0.51143	0.86986	0.36604	0.10204	0.21930	0.	0.
DIV 0.													
DIV 57	0.89608	0.50118	0.66393	0.21832	0.90795	0.53125	0.54190	0.90764	0.45849	0.37959	0.28070	0.	0.
DIV 0.													
DIV 58	0.93819	0.61412	0.68445	0.31416	0.77391	0.53125	0.49571	0.86146	0.38113	0.20408	0.22807	0.	0.
DIV 0.													
DIV 59	0.89453	0.72941	0.76090	0.43237	0.82752	0.59375	0.32238	0.94878	0.42453	0.08163	0.21930	0.	0.
DIV 0.													
DIV 60	0.91269	0.50824	0.75423	0.41640	0.64969	0.50000	0.49810	0.85810	0.35094	0.09796	0.21930	0.	0.
DIV 0.													
DIV 61	0.90979	0.54353	0.82350	0.33227	0.73905	0.59375	0.33905	1.00000	0.37736	0.07755	0.22807	0.	0.
DIV 0.													
DIV 62	0.98262	0.67294	0.71524	0.19702	0.81055	0.53125	0.35000	0.93115	0.44151	0.20000	0.21930	0.	0.
DIV 0.													
DIV 63	0.95364	0.58824	0.75577	0.18211	0.83914	0.50000	0.32714	0.91184	0.38679	0.16327	0.23684	0.	0.
DIV 0.													
DIV 64	1.00000	0.94353	0.69472	0.07987	0.86059	0.46875	0.34905	0.88749	0.41132	0.18367	0.22807	0.	0.
DIV 0.													
DIV 65	0.89685	0.53882	0.71832	0.35570	0.73012	0.53125	0.54333	0.99580	0.31887	0.20000	0.21930	0.	0.
DIV 0.													
DIV 66	0.96716	0.63529	0.68343	0.20447	0.82931	0.50000	0.38143	0.89337	0.40755	0.18367	0.22807	0.	0.
DIV 0.													
DIV 67	0.97199	0.72941	0.65829	0.18530	0.88740	0.31250	0.35190	0.92863	0.44906	0.16735	0.26316	0.	0.
DIV 0.													
DIV 68	0.97895	0.59765	0.69523	0.14803	0.83557	0.53125	0.40333	0.92191	0.42264	0.18367	0.22807	0.	0.
DIV 0.													
DIV 69	0.94785	0.58353	0.75013	0.21299	0.85076	0.53125	0.37143	0.87154	0.37925	0.12653	0.24561	0.	0.
DIV 0.													
DIV 70	0.91057	0.67765	0.74756	0.22258	0.96962	0.59375	0.39762	0.84719	0.38302	0.13469	0.27193	0.	0.
DIV 0.													
DIV 71	0.89222	0.50588	0.61673	0.43450	0.73190	0.53125	0.60714	0.90092	0.33774	0.15510	0.17544	0.	0.
DIV 0.													
DIV 72	0.97045	0.68706	0.69061	0.12460	0.97766	0.56250	0.33524	0.86482	0.45283	0.21224	0.14912	0.	0.
DIV 0.													
DIV 73	0.98281	0.60941	0.70549	0.07774	0.93119	0.62500	0.37000	0.90344	0.37736	0.21224	0.21053	0.	0.
DIV 0.													
DIV 74	0.96639	0.60471	0.62083	0.22364	0.89097	0.50000	0.45571	0.88833	0.37925	0.17959	0.18421	0.	0.
DIV 0.													
DIV 75	0.97296	0.54824	0.72858	0.13632	0.90259	0.43750	0.36905	0.94374	0.41509	0.22857	0.01754	0.	0.
DIV 0.													
DIV 76	0.97470	0.50353	0.65418	0.08733	0.95442	0.56250	0.46095	0.87573	0.45660	0.20816	0.16667	0.	0.
DIV 0.													
DIV 77	0.88159	0.55059	0.54438	0.32162	0.80608	0.56250	0.68190	0.91352	0.30566	0.18776	0.21930	0.	0.
DIV 0.													
DIV 78	0.85455	0.55059	0.56491	0.35783	0.80161	0.59375	0.69857	0.86986	0.24906	0.12245	0.21930	0.	0.
DIV 0.													
DIV 79	0.90014	0.50588	0.57517	0.21725	0.85880	0.53125	0.71476	0.89001	0.28679	0.22857	0.15789	0.	0.
DIV 0.													
DIV 80	0.87502	0.43529	0.51873	0.39936	0.79625	0.56250	0.85095	0.75231	0.25472	0.12245	0.17544	0.	0.
DIV 0.													
DIV 81	0.89956	0.39294	0.40072	0.25559	0.79625	0.40625	0.94000	0.89421	0.32075	0.13469	0.29825	0.	0.
DIV 0.													
DIV 82	0.88874	0.37882	0.40841	0.27050	0.81233	0.56250	0.96143	0.88077	0.23774	0.11020	0.14912	0.	0.
DIV 0.													
DIV 83	0.89820	0.40000	0.48076	0.26305	0.96425	0.34375	1.00000	0.52477	0.28679	0.08980	0.08772	0.	0.
DIV 0.													
DIV 84	0.90168	0.44941	0.67470	0.50160	0.68097	0.53125	0.52952	0.81276	0.40566	0.20000	0.19298	0.	0.
DIV 0.													

COS	1	0.90994	0.97274	0.97647	0.97462	0.95792	0.98815	0.97843	0.95412
COS	2	0.98856	0.99790	0.92544	0.98857	0.98010	0.97068	0.96695	0.92845
COS	3	0.97155	0.96636	0.96912	0.96180	0.98729	0.95948	0.91401	0.95609
COS	4	0.96945	0.96876	0.95035	0.95698	0.94974	0.96774	0.97569	0.96971
COS	5	0.97271	0.96902	0.97470	0.93956	0.96000	0.93075	0.96467	0.98916
COS	6	0.98848	0.95095	0.96165	0.95921	0.97104	0.96603	0.86414	0.92547
COS	7	0.95125	0.95827	0.88710	0.91357	0.93365	0.94966	0.97311	0.92801
COS	8	0.92058	0.94593	0.97237	0.97161	0.93702	0.93912	0.94043	0.94451
COS	9	0.97864	0.94041	0.90083	0.96821	0.95475	0.94741	0.95102	0.95978
COS	10	0.95327	0.89351	0.97974	0.94900	0.90858	0.95429	0.93015	0.94099
COS	11	0.94662	0.95845	0.95932	0.95104	0.97183	0.92667	0.98836	0.97640
COS	12	0.96129	0.94691	0.97048	0.93108	0.95734	0.96132	0.96834	0.96841
COS	13	0.97182	0.98596	0.94928	0.99056	0.97763	0.94610	0.95722	0.97463
COS	14	0.99161	0.93129	0.93215	0.94679	0.95691	0.96316	0.94586	0.95714
COS	15	0.92101	0.98466	0.97592	0.96294	0.94598	0.96865	0.99240	0.98751
COS	16	0.94859	0.89054	0.93580	0.94417	0.94803	0.92993	0.95117	0.95589
COS	17	0.95101	0.95474	0.96096	0.93827	0.92117	0.95650	0.96312	0.95572
COS	18	0.94380	0.91302	0.94954	0.94077	0.95114	0.92713	0.93055	0.92500
COS	19	0.97965	0.95433	0.95703	0.93013	0.95419	0.96512	0.96758	0.97380
COS	20	0.95971	0.83969	0.95393	0.92977	0.91671	0.91689	0.95964	0.94302
COS	21	0.89067	0.93763	0.90925	0.82598	0.91669	0.95741	0.91511	0.95201
COS	22	0.91949	0.88210	0.90828	0.92762	0.91263	0.94143	0.94753	0.95639
COS	23	0.93460	0.94577	0.93584	0.97784	0.96900	0.95955	0.94832	0.95968
COS	24	0.97660	0.98376	0.98544	0.96702	0.98777	0.93375	0.89499	0.92202
COS	25	0.92336	0.93209	0.93669	0.93672	0.95795	0.91095	0.97844	0.95725
COS	26	0.93866	0.92806	0.96296	0.98801	0.98997	0.98944	0.94743	0.96587
COS	27	0.93621	0.98700	0.89104	0.92991	0.93942	0.93862	0.94830	0.94741
COS	28	0.93312	0.91432	0.96088	0.95102	0.90833	0.95239	0.97153	0.95059
COS	29	0.96875	0.96676	0.93153	0.96496	0.96836	0.98089	0.96555	0.88007
COS	30	0.88480	0.90200	0.91275	0.92309	0.91059	0.91586	0.90562	0.94480
COS	31	0.94027	0.92801	0.95405	0.95729	0.95247	0.95871	0.95850	0.95348
COS	32	0.96152	0.92135	0.97800	0.96104	0.97780	0.86000	0.88685	0.88829
COS	33	0.89868	0.90816	0.90540	0.92166	0.87150	0.95616	0.93629	0.92389
COS	34	0.90616	0.94949	0.97348	0.96823	0.98308	0.92740	0.95693	0.91433
COS	35	0.97895	0.99103	0.96400	0.96389	0.87009	0.91066	0.91739	0.92007
COS	36	0.93099	0.93508	0.92018	0.90219	0.94677	0.93966	0.89901	0.94146
COS	37	0.96040	0.94422	0.95868	0.96095	0.92641	0.95564	0.95408	0.97391
COS	38	0.95999	0.99595	0.98196	0.96733	0.83831	0.88197	0.88615	0.91029
COS	39	0.90974	0.92733	0.92968	0.90134	0.91073	0.93612	0.87154	0.91143
COS	40	0.90265	0.92811	0.94752	0.94138	0.90758	0.89952	0.93223	0.94078
COS	41	0.94625	0.95267	0.92428	0.94622	0.95815	0.87081	0.90061	0.90655
COS	42	0.91681	0.92514	0.91936	0.92886	0.89991	0.95538	0.94476	0.92128
COS	43	0.95062	0.96767	0.96252	0.97184	0.96795	0.94308	0.96024	0.94642
COS	44	0.98480	0.97927	0.98445	0.99284	0.97823	0.98340	0.93881	0.89537
COS	45	0.88557	0.91081	0.91902	0.93101	0.91543	0.92065	0.90487	0.95497
COS	46	0.94958	0.94297	0.93694	0.95165	0.96426	0.96542	0.97852	0.96015
COS	47	0.97507	0.91529	0.98869	0.97520	0.98025	0.98881	0.98378	0.98477

COS	48	0.94539	0.98613	0.85107	0.89630	0.90600	0.90595	0.91489	0.93082
COS	49	0.91429	0.90625	0.92100	0.91981	0.86812	0.92728	0.93682	0.91541
COS	50	0.94140	0.92811	0.92307	0.92952	0.95948	0.95639	0.93546	0.98391
COS	51	0.96911	0.93721	0.98782	0.95406	0.97007	0.96553	0.84509	0.88878
COS	52	0.88427	0.89636	0.90482	0.91082	0.92381	0.87224	0.94813	0.93313
COS	53	0.90832	0.90991	0.94978	0.96677	0.96695	0.97586	0.92316	0.94486
COS	54	0.92955	0.97508	0.98768	0.96993	0.96722	0.99699	0.97499	0.95913
COS	55	0.98275	0.98264	0.95361	0.89976	0.84505	0.90046	0.91317	0.92182
COS	56	0.87683	0.89084	0.89828	0.92626	0.94072	0.93766	0.93870	0.91523
COS	57	0.92518	0.93975	0.94417	0.95112	0.96346	0.89538	0.97458	0.94215
COS	58	0.95442	0.95923	0.93558	0.94352	0.91078	0.96065	0.96594	0.92983
COS	59	0.93130	0.87405	0.87938	0.90115	0.90786	0.91927	0.90334	0.90524
COS	60	0.88475	0.95002	0.94230	0.92439	0.92615	0.94695	0.95366	0.95832
COS	61	0.97142	0.93021	0.97380	0.92425	0.98612	0.97344	0.98333	0.97696
COS	62	0.98388	0.98484	0.94833	0.98281	0.99138	0.96041	0.98206	0.96825
COS	63	0.86844	0.89315	0.90550	0.91427	0.92318	0.91965	0.92480	0.89793
COS	64	0.95226	0.94547	0.91656	0.93287	0.95273	0.95829	0.96940	0.97196
COS	65	0.93734	0.96408	0.94677	0.98788	0.98162	0.98819	0.98040	0.98630
COS	66	0.98889	0.96423	0.99111	0.99026	0.97456	0.99012	0.96474	0.99503
COS	67	0.86121	0.85363	0.87860	0.89068	0.90115	0.87652	0.88925	0.86326
COS	68	0.94090	0.93550	0.92789	0.90669	0.93004	0.95295	0.94790	0.96652
COS	69	0.91731	0.96647	0.89501	0.97871	0.97103	0.96238	0.96247	0.98468
COS	70	0.96496	0.93512	0.97130	0.98254	0.93536	0.97921	0.95868	0.99445
COS	71	0.98614	0.84991	0.89918	0.90152	0.90487	0.91373	0.92129	0.92136
COS	72	0.89550	0.94637	0.92980	0.88770	0.91637	0.94476	0.94252	0.96356
COS	73	0.95719	0.91253	0.95169	0.96288	0.97839	0.97525	0.98614	0.96320
COS	74	0.97466	0.98332	0.96116	0.98172	0.97155	0.97201	0.98088	0.94725
COS	75	0.98430	0.99333	0.97151	0.84996	0.89693	0.90219	0.90559	0.91359
COS	76	0.92693	0.91973	0.89549	0.93768	0.93055	0.88509	0.92989	0.94896
COS	77	0.93830	0.95695	0.95136	0.92557	0.94947	0.95854	0.97262	0.96148
COS	78	0.99073	0.97873	0.96733	0.99497	0.96633	0.98451	0.98145	0.99058
COS	79	0.97740	0.94863	0.98540	0.99313	0.96868	0.98917	0.82172	0.88980
COS	80	0.88843	0.88886	0.89636	0.92419	0.90688	0.88391	0.90959	0.90606
COS	81	0.84446	0.91594	0.93261	0.90737	0.93479	0.92139	0.90605	0.91578
COS	82	0.96261	0.94613	0.93245	0.98077	0.96256	0.93794	0.98691	0.96105
COS	83	0.96695	0.95990	0.99691	0.95628	0.92084	0.95907	0.97436	0.93369
COS	84	0.97337	0.99251	0.85023	0.87943	0.89462	0.90223	0.91125	0.91920
COS	85	0.91123	0.90717	0.92036	0.92559	0.88283	0.92984	0.93067	0.92255
COS	86	0.94484	0.93560	0.93145	0.93570	0.94724	0.96458	0.94470	0.98304
COS	87	0.97749	0.94958	0.98949	0.96212	0.97732	0.97574	0.99692	0.96372
COS	88	0.94353	0.97156	0.98337	0.95133	0.97753	0.99448	0.99463	0.81512
COS	89	0.88181	0.88084	0.88182	0.89131	0.91613	0.89751	0.87861	0.90386
COS	90	0.90004	0.84119	0.91213	0.92879	0.90161	0.92917	0.91790	0.90075
COS	91	0.91215	0.95849	0.94409	0.92914	0.98017	0.96316	0.93682	0.98719
COS	92	0.95622	0.96693	0.95938	0.99668	0.95552	0.91822	0.95805	0.97326
COS	93	0.93179	0.97301	0.99119	0.99930	0.99455	0.85375	0.84346	0.86838
COS	94	0.89348	0.89980	0.88663	0.90588	0.90366	0.92039	0.93492	0.91898

COS	95	0.93596	0.91688	0.93991	0.95011	0.94640	0.94740	0.94434	0.90361
COS	96	0.97214	0.95883	0.96097	0.98434	0.96254	0.96847	0.95036	0.98179
COS	97	0.98100	0.95908	0.96725	0.96479	0.97675	0.98238	0.96929	0.96692
COS	98	0.97727	0.95711	0.97683	0.95599	0.84408	0.86679	0.88449	0.89406
COS	99	0.90403	0.90733	0.90246	0.89665	0.91752	0.92364	0.88644	0.92240
COS	100	0.92582	0.92368	0.94167	0.93768	0.92831	0.93711	0.93737	0.96628
COS	101	0.94739	0.98047	0.97736	0.95676	0.98855	0.96218	0.97795	0.97952
COS	102	0.99317	0.96948	0.94564	0.97720	0.98666	0.96149	0.97868	0.99461
COS	103	0.99127	0.99871	0.99138	0.97983	0.83728	0.86182	0.87803	0.88693
COS	104	0.89793	0.90100	0.89450	0.88547	0.91561	0.91934	0.88396	0.91693
COS	105	0.92547	0.92276	0.93770	0.93846	0.92159	0.93804	0.93147	0.96467
COS	106	0.94668	0.98017	0.97734	0.96049	0.99015	0.96029	0.97710	0.98152
COS	107	0.99004	0.97190	0.94310	0.98110	0.98747	0.96682	0.97838	0.99505
COS	108	0.98951	0.99654	0.98988	0.97915	0.99909	0.83794	0.85804	0.87581
COS	109	0.88657	0.89861	0.89668	0.89409	0.88393	0.91672	0.92063	0.88962
COS	110	0.91560	0.92494	0.92563	0.94036	0.94332	0.92386	0.93836	0.93124
COS	111	0.96905	0.95310	0.98017	0.97720	0.96647	0.98845	0.96085	0.98038
COS	112	0.98357	0.98746	0.97727	0.94854	0.98278	0.99054	0.96964	0.98195
COS	113	0.99345	0.98644	0.99493	0.98759	0.98006	0.99821	0.99854	0.84282
COS	114	0.84788	0.86749	0.88284	0.89237	0.88097	0.89457	0.86656	0.92892
COS	115	0.92894	0.91330	0.90883	0.92607	0.94713	0.94833	0.96057	0.92637
COS	116	0.95305	0.90677	0.97646	0.97067	0.96693	0.97241	0.98569	0.97394
COS	117	0.95416	0.97970	0.98785	0.95567	0.98706	0.95925	0.99322	0.99289
COS	118	0.99374	0.97765	0.98193	0.95687	0.97131	0.95547	0.98390	0.97982
COS	119	0.98330	0.98616	0.80122	0.82119	0.83996	0.85105	0.86298	0.86205
COS	120	0.87031	0.85843	0.89349	0.89196	0.86456	0.88583	0.89703	0.90241
COS	121	0.92404	0.92154	0.90598	0.92325	0.92170	0.95981	0.94627	0.96249
COS	122	0.96108	0.95737	0.96754	0.94715	0.97240	0.96728	0.96956	0.96799
COS	123	0.95186	0.97424	0.98468	0.96413	0.98200	0.98224	0.97119	0.98140
COS	124	0.97269	0.97712	0.98622	0.98540	0.99057	0.98235	0.84260	0.87634
COS	125	0.88481	0.89486	0.90259	0.90616	0.91636	0.88579	0.93690	0.92902
COS	126	0.89630	0.91927	0.93858	0.94482	0.96140	0.95797	0.92820	0.94969
COS	127	0.94717	0.97990	0.97682	0.97976	0.97338	0.98009	0.98026	0.96357
COS	128	0.98802	0.98090	0.97078	0.98637	0.96222	0.98793	0.99714	0.97873
COS	129	0.99376	0.99057	0.97337	0.98115	0.97227	0.98309	0.98430	0.98398
COS	130	0.98834	0.99019	0.99139	0.85463	0.86498	0.88996	0.89358	0.90316
COS	131	0.89508	0.90313	0.89283	0.92782	0.92115	0.89621	0.92032	0.93028
COS	132	0.92554	0.94784	0.93718	0.93487	0.95089	0.94345	0.97729	0.95699
COS	133	0.97472	0.97286	0.95418	0.96990	0.93356	0.98331	0.97191	0.97496
COS	134	0.96196	0.97182	0.97523	0.98552	0.96301	0.98138	0.98186	0.96963
COS	135	0.98126	0.96916	0.97447	0.98266	0.97887	0.98342	0.97497	0.98895
COS	136	0.98859	0.83551	0.85684	0.87219	0.88495	0.89571	0.89489	0.89500
COS	137	0.88029	0.91804	0.92214	0.89244	0.91954	0.92823	0.93050	0.94184
COS	138	0.94518	0.92530	0.94015	0.92633	0.96873	0.95481	0.97845	0.98183
COS	139	0.96938	0.98847	0.95978	0.98295	0.98593	0.98404	0.97913	0.94914
COS	140	0.98507	0.99108	0.97388	0.97952	0.99397	0.98431	0.99339	0.98477
COS	141	0.98542	0.99722	0.99857	0.99868	0.98979	0.98824	0.98855	0.98080

COS	142	0.80127	0.87359	0.86954	0.86042	0.86605	0.90884	0.90807	0.87324
COS	143	0.90122	0.87568	0.82161	0.87806	0.91111	0.89416	0.93178	0.90447
COS	144	0.90887	0.90834	0.96354	0.94134	0.93542	0.95814	0.94171	0.92880
COS	145	0.95668	0.94127	0.95704	0.94078	0.97526	0.94552	0.92271	0.94104
COS	146	0.96411	0.91690	0.97071	0.97492	0.97917	0.97456	0.97712	0.94631
COS	147	0.97053	0.96496	0.96706	0.94366	0.97430	0.97419	0.97669	0.96253
COS	148	0.84251	0.85662	0.87827	0.89013	0.90018	0.89876	0.89869	0.89642
COS	149	0.91511	0.92302	0.89011	0.91857	0.91881	0.92276	0.94061	0.93641
COS	150	0.92888	0.93754	0.93184	0.96836	0.94911	0.97668	0.97579	0.95785
COS	151	0.98406	0.96071	0.97793	0.97888	0.98908	0.96974	0.95023	0.97803
COS	152	0.98748	0.96501	0.97987	0.99237	0.98643	0.99673	0.98664	0.98289
COS	153	0.99912	0.99783	0.99815	0.98264	0.99047	0.98663	0.98626	0.99694
COS	154	0.97021	0.83952	0.86327	0.88036	0.88947	0.90009	0.90236	0.89802
COS	155	0.88920	0.91716	0.92118	0.88559	0.91831	0.92591	0.92381	0.94043
COS	156	0.93881	0.92446	0.93820	0.93580	0.96707	0.94925	0.98057	0.97702
COS	157	0.96055	0.98872	0.96087	0.97894	0.98074	0.99119	0.97249	0.94655
COS	158	0.98029	0.98859	0.96612	0.98063	0.99502	0.98995	0.99737	0.99027
COS	159	0.97971	0.99967	0.99950	0.99913	0.98319	0.98847	0.98636	0.98369
COS	160	0.99827	0.96977	0.99915	0.83456	0.85943	0.87318	0.88143	0.89224
COS	161	0.89203	0.89207	0.87424	0.92627	0.91996	0.88965	0.90356	0.92427
COS	162	0.93230	0.94364	0.94953	0.91000	0.95081	0.92645	0.97199	0.96183
COS	163	0.97733	0.96822	0.97594	0.98444	0.96004	0.97581	0.98119	0.96953
COS	164	0.98039	0.94872	0.99306	0.99330	0.98629	0.98887	0.99120	0.97197
COS	165	0.98100	0.97153	0.97859	0.98674	0.99033	0.99049	0.99270	0.98596
COS	166	0.99096	0.97560	0.99193	0.95542	0.98804	0.98948	0.83808	0.84183
COS	167	0.86850	0.88436	0.89504	0.88798	0.88911	0.89287	0.90267	0.91867
COS	168	0.88926	0.91713	0.90850	0.91423	0.93123	0.92836	0.92889	0.92673
COS	169	0.91970	0.96152	0.93926	0.96911	0.97356	0.94938	0.97790	0.95519
COS	170	0.97302	0.97513	0.98693	0.96291	0.94676	0.96954	0.98051	0.95615
COS	171	0.96947	0.98572	0.98268	0.99491	0.98360	0.98041	0.99742	0.99526
COS	172	0.99630	0.97708	0.98714	0.97953	0.98260	0.99454	0.96394	0.99843
COS	173	0.99694	0.97957	0.84366	0.85574	0.87534	0.88519	0.89628	0.89535
COS	174	0.89904	0.88473	0.92274	0.92217	0.89904	0.91343	0.92571	0.93400
COS	175	0.94541	0.94894	0.93515	0.94799	0.92380	0.97406	0.95994	0.97649
COS	176	0.98080	0.97285	0.98522	0.95838	0.98246	0.98879	0.98113	0.98045
COS	177	0.95574	0.98697	0.99249	0.97710	0.98057	0.99245	0.98029	0.99140
COS	178	0.98026	0.98645	0.99577	0.99671	0.99787	0.99219	0.99073	0.99080
COS	179	0.98447	0.99863	0.96652	0.99656	0.99701	0.99249	0.99370	0.83112
COS	180	0.84248	0.86287	0.87714	0.88842	0.88474	0.88683	0.88046	0.90970
COS	181	0.91659	0.89064	0.91262	0.91577	0.92288	0.93506	0.93771	0.92450
COS	182	0.93681	0.91690	0.96607	0.94915	0.97257	0.97912	0.96420	0.98364
COS	183	0.95645	0.97871	0.98318	0.98169	0.97404	0.94878	0.98212	0.98798
COS	184	0.97183	0.97643	0.99082	0.98089	0.99262	0.98166	0.98678	0.99700
COS	185	0.99799	0.99815	0.98862	0.98995	0.98645	0.98082	0.99921	0.96093
COS	186	0.99782	0.99791	0.99110	0.99613	0.99853	0.82165	0.86058	0.87321
COS	187	0.87830	0.88895	0.89979	0.89415	0.88351	0.90482	0.90404	0.85976
COS	188	0.90568	0.91631	0.90557	0.93340	0.92364	0.91385	0.92214	0.94986

COS	189	0.95827	0.94158	0.97682	0.96430	0.94733	0.98063	0.95763	0.97281
COS	190	0.96606	0.99147	0.96311	0.94169	0.96694	0.98234	0.94692	0.98216
COS	191	0.99030	0.99153	0.99457	0.99259	0.96829	0.99433	0.99142	0.99376
COS	192	0.96919	0.99138	0.98553	0.98708	0.98919	0.98522	0.99435	0.99428
COS	193	0.97948	0.99218	0.98896	0.98883	0.84478	0.83049	0.85997	0.88003
COS	194	0.88715	0.87397	0.90013	0.89256	0.91570	0.92226	0.91034	0.91045
COS	195	0.90250	0.93176	0.94701	0.94189	0.94366	0.94245	0.90618	0.97432
COS	196	0.96341	0.95326	0.96776	0.96365	0.95490	0.94688	0.97580	0.97357
COS	197	0.95033	0.96737	0.97212	0.97415	0.98291	0.96978	0.97263	0.97057
COS	198	0.94823	0.96844	0.94688	0.99087	0.97313	0.97064	0.97655	0.98397
COS	199	0.98730	0.98901	0.98485	0.97792	0.95923	0.97965	0.97433	0.97652
COS	200	0.97629	0.98384	0.98035	0.97193	0.82836	0.84932	0.86626	0.87743
COS	201	0.88704	0.88682	0.89627	0.87769	0.91654	0.91541	0.88678	0.90681
COS	202	0.91929	0.92665	0.94389	0.94057	0.92442	0.93847	0.93319	0.97200
COS	203	0.96115	0.97224	0.97167	0.96893	0.97620	0.95685	0.98229	0.97793
COS	204	0.97658	0.97838	0.95827	0.98188	0.99214	0.97324	0.98617	0.98910
COS	205	0.97688	0.98704	0.97678	0.98333	0.99136	0.99031	0.99432	0.98924
COS	206	0.99761	0.99574	0.99246	0.99333	0.97584	0.99454	0.99311	0.98961
COS	207	0.99100	0.99551	0.99363	0.99225	0.98997	0.81598	0.85578	0.86461
COS	208	0.87041	0.88275	0.88998	0.88210	0.85909	0.91121	0.90554	0.86808
COS	209	0.90183	0.92446	0.91700	0.93282	0.93941	0.90363	0.93560	0.93326
COS	210	0.96143	0.94966	0.98032	0.96977	0.96758	0.98925	0.95983	0.97533
COS	211	0.97926	0.97962	0.97680	0.94351	0.98652	0.99027	0.97234	0.98463
COS	212	0.99435	0.98451	0.98760	0.98535	0.97362	0.99136	0.99461	0.99491
COS	213	0.98632	0.98789	0.98894	0.97536	0.99507	0.96506	0.99015	0.99358
COS	214	0.99476	0.98424	0.99383	0.99298	0.98816	0.96973	0.98980	0.81991
COS	215	0.85012	0.86551	0.87354	0.88488	0.89115	0.88872	0.88297	0.90103
COS	216	0.90268	0.86474	0.90617	0.91238	0.90509	0.93050	0.92158	0.91670
COS	217	0.92137	0.94009	0.95831	0.94017	0.97331	0.96896	0.94732	0.97891
COS	218	0.95218	0.97476	0.96803	0.99006	0.96286	0.94224	0.96638	0.98139
COS	219	0.94790	0.97878	0.98852	0.98876	0.99491	0.99046	0.97313	0.99538
COS	220	0.99249	0.99493	0.97086	0.99254	0.98451	0.98775	0.99116	0.98128
COS	221	0.99604	0.99527	0.97899	0.99523	0.99080	0.99173	0.99908	0.97496
COS	222	0.99324	0.98703	0.81596	0.83701	0.85334	0.86491	0.87690	0.88477
COS	223	0.88201	0.87365	0.89635	0.90127	0.86999	0.89761	0.90394	0.90919
COS	224	0.92599	0.92867	0.91901	0.92282	0.91624	0.95476	0.93965	0.96793
COS	225	0.96989	0.95680	0.98161	0.96188	0.96856	0.97726	0.98275	0.96914
COS	226	0.93638	0.97305	0.98172	0.95754	0.97172	0.98865	0.98462	0.99229
COS	227	0.98578	0.97905	0.99529	0.99616	0.99629	0.98021	0.98738	0.98164
COS	228	0.97212	0.99590	0.96635	0.99463	0.99562	0.98593	0.99339	0.99559
COS	229	0.99654	0.99032	0.97324	0.98907	0.99316	0.99187	0.82809	0.83744
COS	230	0.85675	0.87283	0.88268	0.87658	0.88791	0.86374	0.91403	0.91860
COS	231	0.89864	0.90596	0.91789	0.93393	0.93941	0.94776	0.92564	0.93974
COS	232	0.90863	0.96909	0.96022	0.96578	0.97446	0.97675	0.97542	0.95627
COS	233	0.97925	0.98551	0.96684	0.98307	0.95483	0.98650	0.99061	0.98323
COS	234	0.97478	0.98537	0.96829	0.98097	0.96764	0.98607	0.98834	0.99045
COS	235	0.99292	0.99706	0.98886	0.98998	0.97934	0.99552	0.95480	0.99057

COS	236	0.99080	0.99079	0.98793	0.99694	0.99525	0.97992	0.98529	0.99414
COS	237	0.98997	0.98241	0.98977	0.82224	0.82238	0.84507	0.86277	0.87432
COS	238	0.86593	0.87717	0.86556	0.90461	0.91050	0.89590	0.89901	0.90519
COS	239	0.92497	0.93086	0.93924	0.92342	0.93580	0.89628	0.96505	0.95265
COS	240	0.96049	0.97486	0.97106	0.97315	0.95038	0.97544	0.98370	0.96557
COS	241	0.97748	0.94922	0.98286	0.98627	0.97901	0.97091	0.98242	0.96557
COS	242	0.98131	0.96614	0.98825	0.98878	0.99106	0.99290	0.99404	0.98882
COS	243	0.98569	0.97592	0.99556	0.95029	0.99149	0.99087	0.99019	0.98963
COS	244	0.99686	0.99704	0.97883	0.98490	0.99227	0.98854	0.98295	0.99210
COS	245	0.99818	0.79757	0.81802	0.82851	0.84095	0.85336	0.84367	0.85863
COS	246	0.81103	0.90500	0.89468	0.88471	0.87183	0.91278	0.92871	0.92201
COS	247	0.94287	0.89150	0.92896	0.88459	0.95558	0.95706	0.94712	0.95523
COS	248	0.98186	0.95657	0.92658	0.96733	0.97340	0.93594	0.98355	0.93230
COS	249	0.98007	0.97926	0.98634	0.96189	0.96499	0.93930	0.95110	0.93944
COS	250	0.96054	0.96345	0.96919	0.97436	0.99205	0.97212	0.97672	0.96054
COS	251	0.97797	0.92610	0.96650	0.96914	0.97957	0.96173	0.97990	0.97561
COS	252	0.95431	0.96455	0.97827	0.97561	0.95685	0.96570	0.98949	0.98462
COS	253	0.80908	0.84274	0.85259	0.86216	0.87120	0.88604	0.89510	0.87597
COS	254	0.90142	0.89670	0.86366	0.89593	0.90798	0.91223	0.93585	0.92511
COS	255	0.92352	0.92086	0.93371	0.95901	0.95044	0.96399	0.96785	0.95639
COS	256	0.97061	0.95483	0.97610	0.96891	0.97842	0.96980	0.94408	0.96644
COS	257	0.98280	0.95164	0.97863	0.98541	0.98049	0.98770	0.98086	0.98023
COS	258	0.98929	0.98667	0.99025	0.97651	0.99489	0.98996	0.98661	0.98883
COS	259	0.98568	0.99140	0.98970	0.97936	0.98909	0.99117	0.98964	0.99385
COS	260	0.98585	0.99549	0.98493	0.99510	0.99075	0.98633	0.98627	0.96278
COS	261	0.82282	0.82990	0.85089	0.86616	0.87659	0.86931	0.88173	0.86196
COS	262	0.90996	0.91272	0.89454	0.90130	0.91257	0.92793	0.93551	0.94169
COS	263	0.92256	0.93916	0.90740	0.96856	0.95761	0.96390	0.97376	0.97335
COS	264	0.97284	0.95056	0.97904	0.98286	0.96597	0.97971	0.95652	0.98557
COS	265	0.98982	0.98244	0.97594	0.98443	0.96681	0.98062	0.96658	0.98678
COS	266	0.98806	0.98980	0.99259	0.99612	0.99222	0.99069	0.98298	0.99481
COS	267	0.95724	0.99128	0.99066	0.99115	0.98840	0.99672	0.99545	0.98132
COS	268	0.98807	0.99590	0.98934	0.98424	0.98906	0.99932	0.99844	0.98835
COS	269	0.98827	0.80791	0.81522	0.83326	0.84634	0.85915	0.84497	0.85894
COS	270	0.83091	0.90353	0.89708	0.89099	0.89584	0.91714	0.92263	0.92289
COS	271	0.93539	0.90998	0.93800	0.88927	0.96134	0.95034	0.95549	0.97751
COS	272	0.97071	0.96467	0.91775	0.98000	0.98006	0.94924	0.97365	0.95323
COS	273	0.98242	0.98161	0.98161	0.96288	0.97307	0.95002	0.96506	0.95106
COS	274	0.97976	0.97392	0.97795	0.98100	0.99118	0.98062	0.98091	0.97501
COS	275	0.98615	0.93808	0.97678	0.97791	0.98120	0.97372	0.98724	0.98551
COS	276	0.96457	0.97729	0.98474	0.98027	0.96954	0.97475	0.99238	0.99115
COS	277	0.99070	0.97448	0.99350	0.81978	0.81634	0.84206	0.86039	0.87067
COS	278	0.86086	0.87669	0.86086	0.90129	0.90928	0.89477	0.89534	0.90031
COS	279	0.92284	0.93000	0.93702	0.92479	0.93297	0.89596	0.96463	0.95292
COS	280	0.95581	0.96912	0.96921	0.96591	0.95033	0.97324	0.98019	0.96107
COS	281	0.97570	0.95563	0.98054	0.98546	0.97848	0.96944	0.97894	0.96145
COS	282	0.97748	0.96113	0.98666	0.98553	0.98676	0.99020	0.99424	0.99103

COS	283	0.98720	0.97977	0.99225	0.95370	0.98954	0.98789	0.98689	0.98808
COS	284	0.99507	0.99391	0.97855	0.98933	0.99420	0.98506	0.98212	0.98845
COS	285	0.99853	0.99830	0.98566	0.98754	0.99915	0.99078	0.82030	0.82041
COS	286	0.84526	0.86105	0.87352	0.86418	0.87287	0.86593	0.90197	0.90731
COS	287	0.89051	0.89457	0.90092	0.91832	0.92785	0.93525	0.91838	0.93522
COS	288	0.90077	0.96512	0.95009	0.96242	0.97092	0.96790	0.97355	0.95079
COS	289	0.97348	0.98099	0.96816	0.97497	0.95067	0.98310	0.98687	0.97810
COS	290	0.97499	0.98349	0.96776	0.98295	0.96878	0.98545	0.99022	0.99205
COS	291	0.99447	0.99269	0.99289	0.98715	0.97967	0.99539	0.95475	0.99346
COS	292	0.99245	0.99200	0.99120	0.99701	0.99737	0.98324	0.98544	0.99453
COS	293	0.99038	0.98660	0.99286	0.99711	0.99909	0.98278	0.98812	0.99825
COS	294	0.98893	0.99790	0.81570	0.81697	0.84111	0.85471	0.86833	0.85676
COS	295	0.86572	0.85603	0.90355	0.90246	0.88762	0.88263	0.89715	0.91678
COS	296	0.92611	0.93741	0.90677	0.93880	0.89826	0.96598	0.95357	0.96063
COS	297	0.96202	0.97223	0.96969	0.94768	0.96923	0.97779	0.95694	0.97601
COS	298	0.95091	0.98690	0.98746	0.98415	0.97956	0.97947	0.95795	0.97320
COS	299	0.95919	0.97938	0.98185	0.98508	0.98887	0.99346	0.99191	0.98819
COS	300	0.97617	0.98928	0.94905	0.98617	0.98540	0.99471	0.98088	0.99215
COS	301	0.99101	0.97694	0.98405	0.99179	0.98959	0.97891	0.98587	0.99352
COS	302	0.99488	0.98453	0.98208	0.99530	0.98648	0.99407	0.99713	0.79621
COS	303	0.83518	0.84737	0.85505	0.86338	0.87648	0.88209	0.86672	0.88911
COS	304	0.88695	0.84459	0.89108	0.89869	0.89292	0.92428	0.90815	0.90582
COS	305	0.91112	0.94094	0.95069	0.93705	0.96141	0.95565	0.93966	0.96337
COS	306	0.94779	0.96843	0.95421	0.97604	0.95515	0.94606	0.95955	0.97689
COS	307	0.94271	0.97818	0.98148	0.97876	0.98348	0.97895	0.97060	0.98409
COS	308	0.98025	0.98413	0.96688	0.99486	0.98686	0.98946	0.98094	0.98840
COS	309	0.98709	0.98464	0.97406	0.98388	0.98278	0.98202	0.99426	0.98123
COS	310	0.99296	0.98023	0.99389	0.98182	0.97733	0.97576	0.95154	0.99599
COS	311	0.98104	0.96560	0.97935	0.98042	0.97593	0.80702	0.80477	0.82844
COS	312	0.85240	0.86209	0.84504	0.86268	0.84250	0.89643	0.90825	0.89275
COS	313	0.88912	0.89366	0.92145	0.92344	0.93708	0.90286	0.92838	0.88260
COS	314	0.95895	0.95170	0.94888	0.95851	0.97192	0.95935	0.94881	0.96616
COS	315	0.97364	0.94285	0.97527	0.95011	0.98321	0.98284	0.98688	0.96763
COS	316	0.97163	0.94620	0.96306	0.94564	0.98191	0.97377	0.97771	0.98112
COS	317	0.99600	0.98319	0.98360	0.96689	0.98520	0.93220	0.97867	0.97765
COS	318	0.98861	0.97447	0.98668	0.98626	0.96362	0.98301	0.98624	0.98152
COS	319	0.96667	0.97756	0.99483	0.99385	0.98882	0.97330	0.99511	0.98881
COS	320	0.99494	0.99322	0.99446	0.96568	0.80878	0.79917	0.82615	0.84803
COS	321	0.85765	0.84702	0.86717	0.85269	0.89242	0.90253	0.89043	0.87695
COS	322	0.88128	0.91789	0.92208	0.93197	0.91314	0.92576	0.87785	0.95744
COS	323	0.94949	0.94222	0.95441	0.96805	0.95446	0.95130	0.96023	0.97226
COS	324	0.94549	0.97245	0.94476	0.97658	0.97930	0.97973	0.96419	0.96956
COS	325	0.94713	0.96562	0.94623	0.98176	0.97599	0.97846	0.98188	0.99304
COS	326	0.98495	0.98143	0.96722	0.98464	0.93988	0.98152	0.97902	0.98584
COS	327	0.97852	0.98849	0.98748	0.96673	0.98600	0.98753	0.97852	0.97027
COS	328	0.98174	0.99450	0.99534	0.98387	0.97866	0.99513	0.98367	0.99698
COS	329	0.99502	0.99432	0.96901	0.99688	0.80119	0.81222	0.83260	0.84888

COS	330	0.85844	0.85298	0.86870	0.84966	0.89513	0.89812	0.87684	0.88919
COS	331	0.89776	0.91251	0.92485	0.92618	0.90908	0.92753	0.90472	0.96028
COS	332	0.94937	0.95521	0.96463	0.96365	0.96289	0.94475	0.97335	0.97135
COS	333	0.95902	0.97128	0.95508	0.97901	0.98494	0.97642	0.97471	0.97951
COS	334	0.96162	0.97518	0.96136	0.98452	0.98278	0.98382	0.98731	0.99151
COS	335	0.99509	0.99018	0.98404	0.98933	0.96005	0.98768	0.98570	0.98804
COS	336	0.98405	0.99169	0.99106	0.98018	0.99030	0.99590	0.98539	0.98297
COS	337	0.98411	0.99532	0.99458	0.98319	0.98910	0.99783	0.99059	0.99719
COS	338	0.99570	0.99419	0.98597	0.99405	0.99396	0.78081	0.78912	0.80566
COS	339	0.83857	0.84592	0.83500	0.85713	0.83855	0.87450	0.89646	0.87483
COS	340	0.89451	0.88350	0.90801	0.91342	0.91784	0.89848	0.90101	0.87815
COS	341	0.94316	0.93799	0.93827	0.96167	0.95655	0.95243	0.94540	0.96609
COS	342	0.96300	0.94486	0.96632	0.93705	0.96530	0.97278	0.96529	0.95592
COS	343	0.96713	0.94954	0.96569	0.94981	0.98676	0.97408	0.97580	0.97869
COS	344	0.98494	0.98095	0.97742	0.96268	0.98420	0.93452	0.97850	0.97631
COS	345	0.97596	0.97816	0.98270	0.98594	0.96476	0.98162	0.98342	0.97433
COS	346	0.97038	0.97862	0.99046	0.99149	0.97635	0.97817	0.99100	0.98512
COS	347	0.99200	0.98901	0.98344	0.96964	0.99228	0.99026	0.99151	0.80305
COS	348	0.77929	0.81505	0.84269	0.85170	0.83026	0.85469	0.85106	0.87763
COS	349	0.89875	0.88819	0.88264	0.86850	0.90362	0.91253	0.91863	0.91153
COS	350	0.91653	0.87085	0.95259	0.93827	0.93522	0.95222	0.95329	0.94455
COS	351	0.94224	0.95781	0.96395	0.93981	0.95891	0.95611	0.96905	0.97326
COS	352	0.97103	0.95767	0.96236	0.94033	0.96186	0.93983	0.98412	0.97147
COS	353	0.97198	0.97687	0.98645	0.98632	0.97868	0.97140	0.97926	0.93791
COS	354	0.97879	0.97405	0.97732	0.97780	0.98303	0.98341	0.96546	0.99085
COS	355	0.98658	0.97109	0.97001	0.97585	0.98983	0.99088	0.97398	0.97827
COS	356	0.99214	0.98139	0.99510	0.99144	0.98962	0.97330	0.99393	0.99593
COS	357	0.99457	0.99201	0.78313	0.81173	0.82716	0.83409	0.84268	0.85389
COS	358	0.86985	0.84809	0.88144	0.87274	0.84191	0.86553	0.88163	0.88869
COS	359	0.91688	0.90369	0.90134	0.90888	0.92187	0.94779	0.93856	0.94484
COS	360	0.94302	0.94209	0.94592	0.93638	0.96002	0.94847	0.95583	0.95385
COS	361	0.94598	0.95624	0.97217	0.94615	0.97258	0.96903	0.95913	0.96742
COS	362	0.95875	0.96557	0.97115	0.96781	0.97432	0.96812	0.99410	0.98507
COS	363	0.98635	0.97139	0.98221	0.97707	0.97316	0.96985	0.97274	0.97711
COS	364	0.97364	0.98328	0.98549	0.99079	0.97148	0.98327	0.97214	0.97582
COS	365	0.97359	0.95672	0.99194	0.98065	0.96633	0.98045	0.97841	0.97764
COS	366	0.99544	0.96879	0.97390	0.98800	0.96820	0.97844	0.76956	0.80520
COS	367	0.81881	0.82258	0.83283	0.84759	0.85835	0.84068	0.87150	0.85945
COS	368	0.82469	0.85045	0.87115	0.87452	0.90636	0.89265	0.88595	0.89982
COS	369	0.92214	0.93986	0.92948	0.94206	0.93303	0.93448	0.94354	0.93308
COS	370	0.95169	0.94001	0.95576	0.94777	0.93406	0.95050	0.96719	0.93846
COS	371	0.97259	0.96642	0.95936	0.96564	0.95999	0.95568	0.96912	0.96587
COS	372	0.97245	0.96085	0.99320	0.98063	0.98220	0.96751	0.98250	0.97493
COS	373	0.97128	0.96813	0.96998	0.97294	0.97022	0.98411	0.97753	0.98755
COS	374	0.97057	0.98328	0.97058	0.96943	0.96830	0.95009	0.98943	0.97497
COS	375	0.95805	0.97422	0.97504	0.97564	0.99467	0.96224	0.96825	0.98303
COS	376	0.96007	0.97152	0.99836	0.76838	0.78437	0.80291	0.81964	0.82752

COS	377	0.83048	0.85664	0.83960	0.86637	0.86666	0.84281	0.85682	0.86221
COS	378	0.88275	0.90726	0.89470	0.89418	0.89453	0.89907	0.94003	0.93349
COS	379	0.92788	0.93583	0.93786	0.93087	0.92968	0.95355	0.94022	0.94049
COS	380	0.94941	0.93912	0.94725	0.96432	0.94264	0.96274	0.95651	0.94320
COS	381	0.95682	0.94330	0.96657	0.96260	0.95889	0.96703	0.96558	0.99067
COS	382	0.97914	0.97906	0.96508	0.96783	0.97094	0.96486	0.96260	0.96833
COS	383	0.97086	0.96902	0.97327	0.98728	0.98665	0.96075	0.97561	0.96505
COS	384	0.97330	0.97271	0.95542	0.98707	0.97883	0.96469	0.98046	0.97673
COS	385	0.97563	0.98913	0.97103	0.97677	0.98776	0.97426	0.98381	0.99677
COS	386	0.99385	0.74724	0.77445	0.79545	0.80261	0.81169	0.81806	0.83230
COS	387	0.82975	0.84013	0.83708	0.79871	0.83355	0.83765	0.83868	0.87959
COS	388	0.85571	0.86048	0.86938	0.90824	0.91644	0.89966	0.91684	0.90495
COS	389	0.89652	0.91252	0.90641	0.92815	0.90539	0.93543	0.91289	0.92144
COS	390	0.91965	0.94125	0.90650	0.95271	0.94015	0.93625	0.94460	0.93741
COS	391	0.93327	0.94659	0.93965	0.94835	0.93044	0.97842	0.95938	0.97232
COS	392	0.94048	0.96923	0.95520	0.94808	0.93985	0.95183	0.94608	0.94523
COS	393	0.96884	0.96253	0.96958	0.94140	0.96826	0.94293	0.94154	0.94072
COS	394	0.91648	0.97181	0.95009	0.92980	0.95000	0.95060	0.95075	0.98531
COS	395	0.93565	0.94224	0.96362	0.93746	0.95400	0.98940	0.99251	0.98765
COS	396	0.73194	0.73150	0.76304	0.76786	0.77798	0.77711	0.80444	0.79834
COS	397	0.81657	0.80755	0.79468	0.81120	0.81608	0.82065	0.85615	0.83457
COS	398	0.86760	0.85949	0.86663	0.90146	0.88073	0.88559	0.89894	0.87802
COS	399	0.88095	0.86058	0.91579	0.89492	0.90596	0.89055	0.92429	0.89923
COS	400	0.91915	0.88936	0.91892	0.91238	0.90416	0.91894	0.90510	0.92393
COS	401	0.92243	0.91481	0.92560	0.91594	0.96254	0.93985	0.96327	0.92021
COS	402	0.95220	0.93289	0.92432	0.91139	0.93288	0.93018	0.92621	0.94448
COS	403	0.95763	0.95365	0.91508	0.94746	0.92181	0.92894	0.92787	0.90670
COS	404	0.95841	0.93870	0.92878	0.94122	0.93496	0.93176	0.96906	0.92042
COS	405	0.92933	0.95311	0.92607	0.94663	0.98067	0.97803	0.98150	0.98586
COS	406	0.69700	0.71630	0.73995	0.74966	0.75733	0.76824	0.79414	0.78476
COS	407	0.79350	0.79212	0.76163	0.78878	0.79079	0.80108	0.84214	0.81677
COS	408	0.83927	0.83050	0.86639	0.88266	0.86867	0.87413	0.87484	0.86771
COS	409	0.87212	0.87758	0.89826	0.87618	0.90140	0.88506	0.90112	0.88726
COS	410	0.91173	0.87768	0.91832	0.90849	0.90487	0.91492	0.90527	0.91385
COS	411	0.91879	0.91103	0.92155	0.90870	0.96174	0.93619	0.95099	0.91476
COS	412	0.95274	0.92968	0.92065	0.91013	0.92862	0.92336	0.92142	0.94433
COS	413	0.95030	0.95031	0.91367	0.94520	0.92110	0.92323	0.92214	0.89809
COS	414	0.95686	0.93271	0.91302	0.93607	0.93103	0.92951	0.97010	0.91864
COS	415	0.92914	0.95001	0.92533	0.94503	0.98150	0.98231	0.98380	0.99225
COS	416	0.99292	0.68006	0.67400	0.70894	0.73020	0.74207	0.71179	0.74133
COS	417	0.75708	0.77063	0.78061	0.76326	0.78188	0.76757	0.77564	0.81099
COS	418	0.79208	0.78996	0.81265	0.82935	0.86711	0.84472	0.85207	0.85488
COS	419	0.84390	0.84408	0.82657	0.88307	0.84735	0.86325	0.85727	0.88868
COS	420	0.87092	0.88890	0.86955	0.90075	0.87478	0.86007	0.88010	0.86456
COS	421	0.89039	0.88715	0.88009	0.89423	0.88633	0.93969	0.91091	0.93390
COS	422	0.88650	0.89822	0.90238	0.89106	0.88852	0.90156	0.89145	0.89457
COS	423	0.91183	0.92699	0.92538	0.88263	0.91601	0.88020	0.89490	0.89629

COS	424	0.88099	0.91859	0.90824	0.89822	0.90880	0.90799	0.91205	0.93874
COS	425	0.90239	0.90285	0.92879	0.90649	0.92616	0.95014	0.95251	0.96009
COS	426	0.97555	0.97043	0.97280	0.83530	0.86447	0.88229	0.89211	0.89942
COS	427	0.90404	0.90416	0.90146	0.90944	0.91633	0.87006	0.92274	0.91650
COS	428	0.90864	0.94033	0.92259	0.92200	0.92600	0.95347	0.96202	0.94247
COS	429	0.97535	0.96520	0.93953	0.97477	0.95709	0.97434	0.96115	0.98673
COS	430	0.95456	0.95480	0.96449	0.98066	0.94456	0.98176	0.98714	0.98550
COS	431	0.99158	0.98524	0.97471	0.98976	0.98487	0.98698	0.96533	0.98899
COS	432	0.98586	0.99085	0.98340	0.98418	0.99131	0.98885	0.97515	0.98851
COS	433	0.98341	0.98380	0.99579	0.97864	0.99044	0.98001	0.99505	0.98185
COS	434	0.97466	0.97330	0.94289	0.99137	0.97732	0.95961	0.97472	0.97787
COS	435	0.97159	0.99554	0.96094	0.96285	0.97922	0.96451	0.96733	0.98468
COS	436	0.98343	0.97662	0.97487	0.95194	0.95102	0.92452	0.	0.

PRINCIPAL COMPONENTS ANALYSIS

THOLEIITIC - ALKALIC BASALT PROBLEM Q-MODE FACTOR ANALYSIS

PROBLEM NAME QMODFVNT 84 VARIABLES, 5 FACTORS

	SYMMETRIC		%CORRELATION		MATRIX		-LOWER HALF		-ELEMENT		% 1, 10 TO ELEMENT % 84, 84				
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	1.000														
2	0.910	1.000													
3	0.973	0.976	1.000												
4	0.975	0.958	0.988	1.000											
5	0.978	0.954	0.989	0.998	1.000										
6	0.925	0.989	0.980	0.971	0.967	1.000									
7	0.928	0.972	0.966	0.969	0.962	0.987	1.000								
8	0.959	0.914	0.956	0.969	0.969	0.950	0.957	1.000							
9	0.950	0.968	0.976	0.970	0.973	0.969	0.975	0.940	1.000						
10	0.960	0.931	0.965	0.989	0.988	0.951	0.962	0.959	0.971	1.000					
11	0.966	0.864	0.925	0.951	0.958	0.887	0.914	0.934	0.950	0.973	1.000				
12	0.928	0.921	0.946	0.972	0.972	0.937	0.939	0.940	0.945	0.979	0.940	1.000			
13	0.901	0.968	0.955	0.947	0.951	0.960	0.953	0.894	0.980	0.949	0.909	0.954	1.000		
14	0.930	0.941	0.947	0.958	0.959	0.951	0.972	0.927	0.988	0.976	0.961	0.947	0.970	1.000	
15	0.931	0.957	0.961	0.968	0.968	0.972	0.986	0.949	0.991	0.978	0.946	0.957	0.975	0.992	1.000
16	0.931	0.932	0.947	0.957	0.963	0.946	0.957	0.921	0.985	0.976	0.963	0.946	0.969	0.992	0.988
17	0.949	0.891	0.936	0.944	0.948	0.930	0.951	0.956	0.951	0.955	0.961	0.938	0.921	0.956	0.963
18	0.944	0.913	0.950	0.941	0.951	0.927	0.931	0.925	0.980	0.954	0.957	0.930	0.954	0.965	0.968
19	0.840	0.954	0.930	0.917	0.917	0.960	0.943	0.891	0.938	0.909	0.826	0.917	0.957	0.915	0.952
20	0.928	0.913	0.941	0.948	0.956	0.935	0.946	0.936	0.978	0.969	0.960	0.948	0.960	0.977	0.984
21	0.895	0.922	0.923	0.932	0.937	0.937	0.958	0.911	0.978	0.957	0.939	0.928	0.963	0.988	0.990
22	0.891	0.930	0.939	0.939	0.948	0.947	0.933	0.914	0.961	0.951	0.908	0.952	0.972	0.951	0.969
23	0.880	0.885	0.902	0.913	0.923	0.911	0.916	0.906	0.945	0.940	0.928	0.954	0.957	0.952	0.959
24	0.860	0.887	0.888	0.899	0.908	0.905	0.922	0.871	0.956	0.936	0.924	0.906	0.949	0.973	0.968
25	0.870	0.911	0.917	0.920	0.931	0.935	0.920	0.902	0.947	0.940	0.899	0.941	0.960	0.944	0.959
26	0.838	0.882	0.886	0.910	0.910	0.927	0.930	0.901	0.911	0.936	0.872	0.911	0.903	0.928	0.948
27	0.871	0.901	0.907	0.917	0.925	0.919	0.929	0.900	0.955	0.945	0.921	0.951	0.968	0.963	0.972
28	0.895	0.886	0.911	0.919	0.931	0.915	0.921	0.905	0.955	0.950	0.943	0.937	0.952	0.964	0.965
29	0.851	0.896	0.906	0.906	0.915	0.931	0.914	0.906	0.921	0.920	0.868	0.927	0.937	0.915	0.941
30	0.845	0.889	0.884	0.896	0.905	0.911	0.924	0.872	0.948	0.933	0.908	0.920	0.950	0.967	0.967
31	0.900	0.845	0.900	0.913	0.922	0.877	0.891	0.898	0.926	0.941	0.938	0.939	0.915	0.925	0.940
32	0.874	0.879	0.901	0.908	0.919	0.903	0.905	0.885	0.950	0.942	0.924	0.926	0.947	0.954	0.958
33	0.868	0.893	0.905	0.914	0.923	0.920	0.925	0.898	0.952	0.945	0.917	0.933	0.953	0.958	0.969
34	0.861	0.854	0.879	0.891	0.901	0.877	0.889	0.863	0.941	0.936	0.928	0.907	0.930	0.953	0.948
35	0.850	0.899	0.902	0.905	0.914	0.921	0.921	0.895	0.946	0.930	0.888	0.916	0.945	0.943	0.964
36	0.850	0.897	0.902	0.906	0.914	0.927	0.920	0.895	0.938	0.931	0.885	0.930	0.949	0.938	0.957
37	0.822	0.890	0.888	0.889	0.896	0.924	0.907	0.884	0.910	0.906	0.844	0.916	0.933	0.907	0.935
38	0.850	0.879	0.895	0.902	0.911	0.919	0.911	0.907	0.920	0.926	0.883	0.930	0.931	0.923	0.945
39	0.815	0.882	0.881	0.882	0.891	0.916	0.898	0.879	0.904	0.900	0.841	0.912	0.929	0.902	0.929
40	0.854	0.843	0.868	0.893	0.900	0.887	0.906	0.904	0.920	0.935	0.919	0.936	0.917	0.940	0.950
41	0.844	0.867	0.884	0.894	0.904	0.907	0.902	0.897	0.918	0.924	0.886	0.922	0.926	0.924	0.942
42	0.837	0.862	0.878	0.887	0.898	0.901	0.894	0.885	0.916	0.919	0.884	0.917	0.925	0.923	0.938
43	0.838	0.858	0.876	0.887	0.899	0.897	0.894	0.884	0.917	0.921	0.890	0.916	0.925	0.926	0.940
44	0.843	0.848	0.867	0.883	0.892	0.881	0.895	0.867	0.929	0.929	0.913	0.909	0.926	0.947	0.948
45	0.801	0.821	0.840	0.851	0.863	0.862	0.870	0.858	0.893	0.892	0.865	0.886	0.897	0.902	0.924
46	0.843	0.876	0.885	0.895	0.903	0.906	0.916	0.886	0.937	0.929	0.896	0.919	0.939	0.945	0.961
47	0.855	0.865	0.890	0.894	0.903	0.895	0.903	0.893	0.928	0.921	0.896	0.920	0.930	0.926	0.948
48	0.836	0.857	0.872	0.885	0.896	0.895	0.895	0.880	0.918	0.922	0.892	0.920	0.928	0.931	0.942
49	0.801	0.874	0.870	0.860	0.866	0.909	0.908	0.873	0.901	0.876	0.822	0.878	0.911	0.894	0.932
50	0.843	0.857	0.878	0.890	0.900	0.899	0.899	0.896	0.915	0.923	0.890	0.919	0.919	0.923	0.941
51	0.840	0.863	0.880	0.889	0.900	0.902	0.898	0.889	0.917	0.921	0.886	0.918	0.926	0.924	0.940
52	0.835	0.859	0.873	0.881	0.892	0.892	0.892	0.874	0.926	0.920	0.890	0.904	0.924	0.932	0.944
53	0.838	0.842	0.869	0.884	0.895	0.888	0.889	0.893	0.903	0.919	0.889	0.917	0.909	0.914	0.931
54	0.844	0.856	0.875	0.885	0.896	0.895	0.899	0.885	0.923	0.922	0.899	0.913	0.926	0.934	0.945
55	0.831	0.842	0.863	0.877	0.888	0.885	0.887	0.880	0.910	0.917	0.891	0.913	0.916	0.923	0.935
56	0.822	0.861	0.873	0.878	0.889	0.900	0.894	0.884	0.905	0.904	0.860	0.906	0.916	0.906	0.933
57	0.845	0.830	0.860	0.880	0.887	0.874	0.900	0.893	0.916	0.922	0.910	0.910	0.903	0.932	0.947
58	0.828	0.849	0.866	0.877	0.887	0.887	0.896	0.878	0.917	0.915	0.887	0.907	0.919	0.927	0.944
59	0.816	0.856	0.865	0.870	0.883	0.890	0.882	0.859	0.911	0.906	0.868	0.902	0.924	0.917	0.933
60	0.820	0.850	0.866	0.874	0.885	0.891	0.889	0.883	0.901	0.903	0.865	0.906	0.912	0.905	0.931
61	0.816	0.837	0.853	0.865	0.877	0.885	0.882	0.874	0.896	0.901	0.870	0.898	0.904	0.909	0.926
62	0.828	0.837	0.857	0.873	0.883	0.877	0.888	0.864	0.914	0.919	0.899	0.906	0.918	0.934	0.939
63	0.822	0.822	0.845	0.863	0.874	0.866	0.877	0.866	0.905	0.910	0.896	0.899	0.905	0.925	0.931
64	0.798	0.818	0.829	0.841	0.853	0.844	0.859	0.811	0.905	0.895	0.885	0.872	0.913	0.929	0.922
65	0.809	0.843	0.853	0.862	0.871	0.886	0.895	0.876	0.901	0.897	0.864	0.896	0.908	0.912	0.936
66	0.823	0.830	0.851	0.866	0.877	0.869	0.882	0.862	0.910	0.913	0.895	0.901	0.913	0.928	0.936
67	0.808	0.815	0.833	0.846	0.859	0.845	0.859	0.831	0.904	0.897	0.891	0.896	0.917	0.923	0.923
68	0.820	0.816	0.842	0.860	0.871	0.861	0.877	0.861	0.901	0.909	0.895	0.895	0.900	0.923	0.930
69	0.820	0.820	0.845	0.861	0.874	0.864	0.873	0.866	0.902	0.907	0.891	0.895	0.901	0.918	0.928
70	0.816	0.817	0.841	0.855	0.868	0.857	0.866	0.856	0.904	0.902	0.888	0.883	0.897	0.917	0.926
71	0.796	0.835	0.847	0.855	0.863	0.876	0.882	0.867	0.889	0.887	0.845	0.891	0.899	0.893	0.924
72	0.807	0.805	0.828	0.852	0.862	0.845	0.863	0.843	0.896	0.908	0.893	0.889	0.894	0.921	0.923
73	0.809	0.799	0.826	0.848	0.858	0.847	0.867	0.853	0.892	0.903	0.890	0.877	0.881	0.918	0.922
74	0.801	0.812	0.833	0.849	0.858	0.853	0.869	0.850	0.895	0.898	0.877	0.889	0.898	0.913	0.925
75	0.781	0.789	0.806	0.839	0.846	0.835	0.857	0.839	0.875	0.896	0.875	0.895	0.884	0.908	0.913
76	0.803	0.779	0.815	0.843	0.852	0.830	0.855	0.851	0.878	0.899	0.888	0.883	0.869	0.904	0.913
77	0.783	0.812	0.827	0.834	0.843	0.854	0.870	0.848	0.881	0.873	0.842	0.866	0.882	0.889	0.917
78	0.770	0.805	0.819	0.823	0.833	0.848	0.858	0.841	0.871	0.859	0.825				

	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
16	1.000														
17	0.956	1.000													
18	0.974	0.960	1.000												
19	0.919	0.882	0.908	1.000											
20	0.985	0.967	0.988	0.934	1.000										
21	0.989	0.947	0.966	0.936	0.987	1.000									
22	0.967	0.932	0.965	0.968	0.981	0.966	1.000								
23	0.959	0.953	0.962	0.921	0.978	0.961	0.978	1.000							
24	0.983	0.927	0.957	0.914	0.979	0.991	0.964	0.964	1.000						
25	0.961	0.926	0.956	0.954	0.974	0.960	0.996	0.982	0.967	1.000					
26	0.941	0.908	0.900	0.932	0.941	0.946	0.953	0.924	0.946	0.958	1.000				
27	0.968	0.943	0.960	0.946	0.985	0.979	0.984	0.993	0.978	0.983	0.939	1.000			
28	0.979	0.960	0.975	0.915	0.989	0.975	0.980	0.989	0.984	0.985	0.945	0.986	1.000		
29	0.928	0.923	0.930	0.959	0.956	0.935	0.984	0.969	0.937	0.988	0.954	0.970	0.988	0.954	1.000
30	0.976	0.923	0.945	0.930	0.975	0.988	0.970	0.967	0.997	0.975	0.959	0.983	0.983	0.954	1.000
31	0.944	0.951	0.963	0.895	0.975	0.942	0.954	0.959	0.936	0.944	0.911	0.961	0.966	0.930	0.931
32	0.971	0.930	0.974	0.924	0.986	0.973	0.983	0.977	0.984	0.985	0.948	0.983	0.991	0.960	0.982
33	0.972	0.937	0.964	0.947	0.988	0.982	0.988	0.980	0.986	0.989	0.964	0.991	0.990	0.975	0.990
34	0.967	0.917	0.966	0.895	0.979	0.971	0.962	0.962	0.985	0.965	0.935	0.971	0.983	0.935	0.979
35	0.957	0.913	0.952	0.963	0.978	0.975	0.986	0.963	0.975	0.983	0.961	0.982	0.972	0.972	0.981
36	0.951	0.926	0.949	0.959	0.973	0.961	0.991	0.979	0.967	0.995	0.966	0.985	0.981	0.991	0.977
37	0.921	0.906	0.916	0.963	0.946	0.932	0.981	0.963	0.938	0.987	0.961	0.967	0.960	0.997	0.956
38	0.936	0.931	0.936	0.947	0.965	0.945	0.983	0.977	0.950	0.989	0.962	0.977	0.976	0.997	0.964
39	0.918	0.901	0.912	0.958	0.944	0.929	0.980	0.963	0.937	0.987	0.956	0.967	0.959	0.997	0.956
40	0.946	0.947	0.944	0.904	0.972	0.959	0.961	0.984	0.963	0.968	0.950	0.982	0.981	0.959	0.967
41	0.938	0.928	0.937	0.937	0.966	0.947	0.980	0.977	0.957	0.989	0.962	0.978	0.980	0.993	0.969
42	0.938	0.922	0.938	0.931	0.965	0.947	0.980	0.977	0.960	0.990	0.960	0.977	0.982	0.990	0.972
43	0.943	0.924	0.938	0.931	0.969	0.953	0.980	0.977	0.966	0.988	0.961	0.980	0.984	0.987	0.977
44	0.961	0.926	0.953	0.907	0.976	0.971	0.967	0.972	0.986	0.974	0.954	0.980	0.988	0.956	0.987
45	0.922	0.906	0.923	0.922	0.960	0.946	0.962	0.961	0.957	0.968	0.947	0.972	0.967	0.970	0.968
46	0.958	0.928	0.950	0.947	0.980	0.977	0.980	0.973	0.980	0.980	0.964	0.988	0.981	0.971	0.986
47	0.937	0.935	0.951	0.943	0.977	0.957	0.975	0.973	0.954	0.970	0.934	0.983	0.972	0.975	0.962
48	0.945	0.925	0.940	0.926	0.969	0.955	0.978	0.982	0.969	0.988	0.960	0.983	0.986	0.984	0.979
49	0.904	0.909	0.908	0.964	0.941	0.935	0.958	0.942	0.929	0.957	0.941	0.957	0.941	0.975	0.946
50	0.936	0.929	0.938	0.932	0.968	0.949	0.977	0.976	0.958	0.984	0.961	0.978	0.979	0.989	0.970
51	0.939	0.924	0.938	0.936	0.967	0.949	0.981	0.977	0.961	0.989	0.961	0.979	0.981	0.991	0.972
52	0.950	0.910	0.951	0.926	0.972	0.962	0.977	0.968	0.976	0.984	0.960	0.976	0.981	0.970	0.980
53	0.928	0.929	0.927	0.920	0.962	0.939	0.969	0.974	0.949	0.978	0.955	0.973	0.975	0.987	0.963
54	0.949	0.935	0.948	0.924	0.974	0.960	0.976	0.981	0.973	0.985	0.958	0.982	0.989	0.981	0.980
55	0.938	0.925	0.937	0.917	0.966	0.949	0.973	0.979	0.964	0.984	0.956	0.979	0.983	0.982	0.974
56	0.924	0.914	0.922	0.950	0.958	0.942	0.977	0.964	0.947	0.981	0.958	0.973	0.966	0.991	0.963
57	0.942	0.944	0.942	0.906	0.974	0.963	0.953	0.968	0.964	0.955	0.947	0.976	0.974	0.950	0.967
58	0.941	0.924	0.938	0.933	0.972	0.961	0.972	0.972	0.969	0.976	0.957	0.982	0.978	0.977	0.978
59	0.939	0.904	0.936	0.933	0.961	0.950	0.980	0.970	0.968	0.989	0.960	0.975	0.979	0.980	0.977
60	0.922	0.917	0.921	0.940	0.958	0.940	0.973	0.969	0.947	0.979	0.952	0.975	0.968	0.990	0.963
61	0.929	0.919	0.923	0.916	0.955	0.940	0.968	0.970	0.957	0.982	0.962	0.969	0.977	0.983	0.969
62	0.948	0.926	0.940	0.909	0.969	0.960	0.966	0.974	0.977	0.975	0.956	0.979	0.986	0.967	0.983
63	0.939	0.923	0.936	0.896	0.965	0.953	0.960	0.975	0.971	0.973	0.950	0.975	0.984	0.966	0.977
64	0.943	0.891	0.929	0.885	0.956	0.957	0.947	0.955	0.982	0.957	0.927	0.967	0.973	0.936	0.984
65	0.925	0.924	0.921	0.934	0.959	0.950	0.964	0.968	0.956	0.971	0.955	0.976	0.969	0.978	0.970
66	0.942	0.923	0.939	0.907	0.969	0.958	0.964	0.974	0.973	0.973	0.951	0.979	0.983	0.966	0.980
67	0.935	0.910	0.938	0.889	0.961	0.950	0.955	0.978	0.971	0.965	0.918	0.980	0.980	0.949	0.974
68	0.937	0.925	0.933	0.896	0.965	0.953	0.956	0.969	0.969	0.966	0.950	0.973	0.980	0.961	0.976
69	0.935	0.918	0.935	0.901	0.965	0.950	0.962	0.971	0.968	0.974	0.951	0.973	0.981	0.968	0.975
70	0.937	0.907	0.939	0.898	0.966	0.954	0.961	0.962	0.972	0.970	0.948	0.969	0.978	0.957	0.976
71	0.908	0.906	0.911	0.941	0.951	0.937	0.961	0.956	0.940	0.963	0.948	0.968	0.954	0.976	0.955
72	0.937	0.903	0.928	0.883	0.959	0.952	0.949	0.959	0.972	0.959	0.949	0.966	0.974	0.943	0.975
73	0.932	0.913	0.926	0.878	0.957	0.949	0.942	0.954	0.968	0.954	0.951	0.960	0.972	0.945	0.972
74	0.926	0.909	0.928	0.905	0.960	0.949	0.955	0.965	0.964	0.963	0.945	0.973	0.971	0.959	0.971
75	0.918	0.898	0.901	0.878	0.943	0.938	0.938	0.962	0.957	0.952	0.945	0.966	0.963	0.945	0.966
76	0.919	0.912	0.917	0.871	0.953	0.938	0.935	0.952	0.953	0.945	0.942	0.958	0.964	0.940	0.959
77	0.904	0.901	0.909	0.922	0.948	0.939	0.945	0.943	0.942	0.946	0.936	0.960	0.948	0.956	0.954
78	0.893	0.886	0.900	0.922	0.940	0.929	0.942	0.933	0.934	0.944	0.933	0.952	0.940	0.956	0.948
79	0.895	0.894	0.895	0.899	0.940	0.933	0.928	0.936	0.938	0.931	0.930	0.954	0.940	0.940	0.949
80	0.856	0.860	0.869	0.908	0.916	0.900	0.917	0.905	0.897	0.913	0.906	0.928	0.905	0.935	0.913
81	0.835	0.868	0.859	0.867	0.901	0.881	0.886	0.899	0.878	0.881	0.861	0.916	0.895	0.906	0.891
82	0.817	0.839	0.831	0.866	0.883	0.869	0.874	0.875	0.868	0.872	0.878	0.898	0.876	0.901	0.885
83	0.792	0.790	0.813	0.829	0.867	0.845	0.852	0.855	0.844	0.844	0.827	0.883	0.847	0.863	0.857
84	0.923	0.922	0.926	0.953	0.962	0.942	0.975	0.965	0.940	0.975	0.957	0.974	0.961	0.987	0.955

	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45
31	1.000														
32	0.968	1.000													
33	0.965	0.995	1.000												
34	0.959	0.994	0.986	1.000											
35	0.947	0.984	0.993	0.972	1.000										
36	0.949	0.985	0.993	0.969	0.989	1.000									
37	0.921	0.959	0.974	0.934	0.973	0.993	1.000								
38	0.944	0.972	0.983	0.951	0.978	0.994	0.995	1.000							
39	0.918	0.958	0.973	0.932	0.973	0.991	0.999	0.995	1.000						
40	0.965	0.977	0.982	0.969	0.967	0.977	0.957	0.977	0.956	1.000					
41	0.946	0.977	0.987	0.961	0.979	0.995	0.991	0.999	0.991	0.980	1.000				
42	0.943	0.981	0.987	0.967	0.978	0.995	0.990	0.997	0.990	0.979	0.999	1.000			
43	0.949	0.983	0.991	0.970	0.982	0.993	0.986	0.995	0.988	0.980	0.998	0.999	1.000		
44	0.959	0.993	0.993	0.994	0.978	0.982	0.957	0.971	0.955	0.984	0.980	0.983	0.986	1.000	
45	0.952	0.974	0.985	0.964	0.982	0.982	0.971	0.981	0.973	0.977	0.986	0.985	0.991	0.982	1.000
46	0.962	0.988	0.997	0.979	0.994	0.991	0.973	0.981	0.972	0.983	0.984	0.984	0.988	0.990	0.991
47	0.972	0.975	0.986	0.963	0.981	0.982	0.970	0.981	0.969	0.974	0.983	0.979	0.983	0.975	0.989
48	0.949	0.985	0.991	0.974	0.980	0.994	0.984	0.993	0.985	0.985	0.997	0.999	0.999	0.990	0.988
49	0.923	0.941	0.964	0.917	0.971	0.975	0.979	0.975	0.977	0.946	0.971	0.965	0.967	0.944	0.974
50	0.950	0.978	0.987	0.965	0.980	0.992	0.986	0.997	0.987	0.983	0.999	0.998	0.998	0.983	0.990
51	0.947	0.980	0.989	0.966	0.981	0.995	0.990	0.997	0.990	0.980	1.000	0.999	0.999	0.983	0.988
52	0.949	0.993	0.993	0.986	0.989	0.991	0.972	0.981	0.972	0.979	0.987	0.990	0.990	0.993	0.986
53	0.947	0.970	0.981	0.956	0.969	0.986	0.983	0.995	0.984	0.980	0.997	0.995	0.996	0.977	0.987
54	0.956	0.987	0.992	0.977	0.981	0.992	0.980	0.991	0.980	0.986	0.996	0.997	0.998	0.992	0.991
55	0.949	0.982	0.988	0.972	0.976	0.991	0.981	0.993	0.982	0.987	0.997	0.998	0.998	0.989	0.990
56	0.942	0.967	0.982	0.947	0.982	0.990	0.992	0.995	0.993	0.968	0.994	0.991	0.994	0.969	0.991
57	0.972	0.974	0.983	0.970	0.973	0.971	0.948	0.968	0.947	0.991	0.973	0.971	0.977	0.984	0.987
58	0.958	0.982	0.992	0.973	0.986	0.989	0.977	0.987	0.977	0.983	0.991	0.990	0.994	0.989	0.998
59	0.944	0.987	0.990	0.972	0.985	0.994	0.985	0.988	0.985	0.974	0.991	0.995	0.995	0.986	0.988
60	0.942	0.966	0.981	0.948	0.979	0.989	0.989	0.995	0.990	0.973	0.995	0.992	0.995	0.971	0.993
61	0.936	0.973	0.982	0.958	0.972	0.989	0.985	0.992	0.986	0.979	0.995	0.996	0.996	0.980	0.987
62	0.955	0.987	0.991	0.983	0.975	0.985	0.968	0.981	0.968	0.986	0.988	0.990	0.993	0.997	0.989
63	0.949	0.983	0.986	0.979	0.971	0.982	0.966	0.981	0.966	0.988	0.989	0.991	0.993	0.994	0.989
64	0.932	0.980	0.979	0.986	0.962	0.965	0.939	0.951	0.939	0.961	0.963	0.969	0.974	0.992	0.972
65	0.944	0.966	0.983	0.952	0.979	0.985	0.980	0.988	0.981	0.980	0.989	0.987	0.990	0.977	0.995
66	0.957	0.986	0.990	0.982	0.976	0.984	0.967	0.981	0.967	0.987	0.988	0.990	0.993	0.996	0.992
67	0.953	0.982	0.982	0.982	0.963	0.973	0.950	0.965	0.951	0.980	0.974	0.978	0.981	0.991	0.981
68	0.956	0.981	0.985	0.978	0.969	0.979	0.961	0.977	0.961	0.987	0.986	0.987	0.990	0.994	0.991
69	0.951	0.983	0.987	0.978	0.975	0.983	0.968	0.983	0.969	0.985	0.990	0.992	0.994	0.993	0.993
70	0.951	0.987	0.987	0.984	0.980	0.979	0.958	0.973	0.959	0.979	0.982	0.985	0.989	0.993	0.992
71	0.946	0.960	0.977	0.943	0.978	0.981	0.979	0.983	0.979	0.971	0.984	0.980	0.984	0.967	0.995
72	0.950	0.983	0.983	0.987	0.968	0.972	0.946	0.963	0.946	0.982	0.974	0.978	0.981	0.996	0.983
73	0.945	0.977	0.979	0.980	0.964	0.970	0.947	0.966	0.946	0.982	0.976	0.978	0.982	0.993	0.985
74	0.955	0.979	0.985	0.976	0.975	0.980	0.962	0.975	0.961	0.985	0.983	0.984	0.987	0.992	0.995
75	0.937	0.965	0.973	0.965	0.956	0.967	0.950	0.966	0.950	0.987	0.974	0.976	0.979	0.985	0.981
76	0.956	0.969	0.973	0.971	0.958	0.962	0.940	0.962	0.940	0.984	0.971	0.972	0.977	0.986	0.986
77	0.946	0.956	0.972	0.946	0.973	0.969	0.959	0.967	0.959	0.966	0.971	0.968	0.974	0.968	0.994
78	0.934	0.951	0.967	0.938	0.973	0.966	0.959	0.966	0.960	0.956	0.969	0.966	0.972	0.961	0.993
79	0.939	0.947	0.964	0.943	0.963	0.957	0.943	0.957	0.943	0.967	0.963	0.959	0.967	0.966	0.991
80	0.921	0.920	0.941	0.906	0.953	0.940	0.936	0.945	0.937	0.933	0.947	0.940	0.948	0.930	0.978
81	0.924	0.899	0.919	0.889	0.919	0.912	0.904	0.919	0.905	0.924	0.922	0.915	0.926	0.916	0.963
82	0.901	0.887	0.912	0.878	0.918	0.908	0.905	0.915	0.905	0.914	0.919	0.911	0.922	0.909	0.962
83	0.889	0.871	0.889	0.870	0.901	0.875	0.860	0.880	0.865	0.890	0.887	0.880	0.894	0.886	0.940
84	0.955	0.964	0.981	0.945	0.982	0.987	0.986	0.992	0.985	0.975	0.990	0.985	0.987	0.965	0.989

	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60
46	1.000														
47	0.989	1.000													
48	0.989	0.981	1.000												
49	0.974	0.977	0.963	1.000											
50	0.987	0.986	0.997	0.970	1.000										
51	0.986	0.984	0.998	0.970	0.999	1.000									
52	0.991	0.976	0.992	0.955	0.988	0.989	1.000								
53	0.980	0.983	0.995	0.964	0.998	0.997	0.980	1.000							
54	0.991	0.984	0.999	0.967	0.997	0.997	0.992	0.994	1.000						
55	0.986	0.981	0.999	0.961	0.998	0.998	0.991	0.996	0.999	1.000					
56	0.986	0.987	0.989	0.985	0.994	0.994	0.979	0.992	0.989	0.989	1.000				
57	0.989	0.985	0.978	0.959	0.980	0.974	0.977	0.976	0.984	0.980	0.972	1.000			
58	0.996	0.992	0.993	0.976	0.995	0.993	0.990	0.991	0.996	0.994	0.992	0.990	1.000		
59	0.989	0.975	0.995	0.965	0.990	0.994	0.995	0.984	0.994	0.993	0.988	0.970	0.990	1.000	
60	0.985	0.988	0.991	0.981	0.996	0.995	0.979	0.995	0.991	0.992	0.999	0.975	0.993	0.987	1.000
61	0.982	0.972	0.996	0.966	0.995	0.996	0.986	0.993	0.996	0.997	0.990	0.973	0.989	0.993	0.992
62	0.990	0.979	0.996	0.955	0.991	0.991	0.991	0.988	0.997	0.995	0.980	0.985	0.994	0.990	0.982
63	0.986	0.976	0.996	0.950	0.991	0.991	0.990	0.990	0.997	0.997	0.979	0.985	0.992	0.989	0.983
64	0.977	0.961	0.978	0.926	0.966	0.969	0.980	0.962	0.980	0.976	0.954	0.965	0.978	0.976	0.957
65	0.990	0.987	0.989	0.986	0.991	0.990	0.979	0.989	0.991	0.990	0.994	0.986	0.995	0.985	0.995
66	0.991	0.983	0.995	0.957	0.991	0.991	0.991	0.988	0.997	0.995	0.981	0.988	0.996	0.989	0.984
67	0.981	0.975	0.986	0.938	0.977	0.978	0.981	0.974	0.987	0.986	0.965	0.977	0.985	0.980	0.970
68	0.987	0.980	0.992	0.954	0.990	0.988	0.987	0.988	0.995	0.994	0.979	0.989	0.994	0.985	0.982
69	0.987	0.980	0.995	0.955	0.993	0.992	0.992	0.991	0.997	0.997	0.983	0.985	0.995	0.990	0.987
70	0.988	0.976	0.989	0.949	0.986	0.985	0.995	0.981	0.992	0.991	0.977	0.984	0.992	0.990	0.979
71	0.987	0.989	0.981	0.988	0.987	0.985	0.974	0.984	0.983	0.982	0.994	0.981	0.993	0.980	0.994
72	0.984	0.967	0.985	0.932	0.979	0.978	0.989	0.974	0.987	0.986	0.964	0.983	0.986	0.982	0.967
73	0.981	0.967	0.985	0.940	0.982	0.979	0.986	0.979	0.988	0.987	0.967	0.986	0.988	0.979	0.970
74	0.990	0.984	0.989	0.960	0.988	0.986	0.988	0.984	0.992	0.991	0.980	0.990	0.996	0.985	0.983
75	0.977	0.963	0.984	0.935	0.979	0.976	0.976	0.978	0.983	0.986	0.965	0.982	0.983	0.974	0.970
76	0.979	0.971	0.979	0.938	0.979	0.974	0.977	0.978	0.983	0.983	0.965	0.991	0.987	0.971	0.970
77	0.985	0.986	0.971	0.982	0.977	0.973	0.970	0.973	0.977	0.974	0.983	0.985	0.991	0.971	0.983
78	0.981	0.982	0.968	0.982	0.975	0.971	0.968	0.970	0.973	0.970	0.984	0.978	0.988	0.971	0.983
79	0.979	0.979	0.965	0.968	0.971	0.965	0.963	0.968	0.971	0.969	0.973	0.987	0.987	0.961	0.976
80	0.959	0.972	0.940	0.969	0.955	0.948	0.940	0.952	0.946	0.945	0.969	0.963	0.970	0.941	0.968
81	0.940	0.963	0.920	0.952	0.933	0.924	0.911	0.933	0.930	0.926	0.944	0.958	0.954	0.915	0.947
82	0.936	0.951	0.915	0.953	0.930	0.921	0.910	0.929	0.923	0.921	0.944	0.950	0.950	0.914	0.945
83	0.911	0.934	0.887	0.898	0.902	0.891	0.889	0.902	0.891	0.895	0.912	0.927	0.925	0.883	0.916
84	0.986	0.991	0.983	0.984	0.991	0.989	0.975	0.989	0.983	0.984	0.996	0.979	0.990	0.980	0.995

	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75
61	1.000														
62	0.990	1.000													
63	0.992	0.998	1.000												
64	0.966	0.989	0.985	1.000											
65	0.991	0.986	0.986	0.963	1.000										
66	0.989	0.999	0.998	0.988	0.988	1.000									
67	0.975	0.992	0.991	0.991	0.974	0.993	1.000								
68	0.988	0.999	0.998	0.986	0.988	0.999	0.991	1.000							
69	0.993	0.997	0.999	0.983	0.988	0.998	0.989	0.998	1.000						
70	0.986	0.994	0.995	0.985	0.982	0.995	0.986	0.994	0.997	1.000					
71	0.982	0.977	0.976	0.952	0.996	0.981	0.966	0.979	0.980	0.976	1.000				
72	0.978	0.995	0.994	0.989	0.973	0.995	0.989	0.995	0.993	0.994	0.966	1.000			
73	0.982	0.994	0.995	0.984	0.979	0.995	0.984	0.997	0.995	0.994	0.969	0.997	1.000		
74	0.984	0.995	0.995	0.983	0.989	0.998	0.991	0.997	0.996	0.994	0.986	0.994	0.994	1.000	
75	0.979	0.990	0.991	0.976	0.978	0.991	0.985	0.992	0.989	0.983	0.970	0.992	0.990	0.992	1.000
76	0.976	0.990	0.991	0.974	0.978	0.992	0.981	0.995	0.991	0.990	0.973	0.994	0.996	0.995	0.992
77	0.972	0.976	0.974	0.957	0.992	0.981	0.966	0.980	0.978	0.978	0.995	0.969	0.974	0.988	0.968
78	0.971	0.969	0.968	0.950	0.989	0.975	0.958	0.974	0.975	0.976	0.995	0.962	0.968	0.983	0.960
79	0.965	0.973	0.973	0.955	0.987	0.979	0.965	0.980	0.977	0.976	0.989	0.971	0.977	0.988	0.974
80	0.943	0.942	0.941	0.916	0.972	0.950	0.930	0.950	0.951	0.951	0.985	0.936	0.942	0.964	0.937
81	0.922	0.929	0.928	0.907	0.958	0.939	0.929	0.941	0.935	0.932	0.969	0.920	0.929	0.953	0.926
82	0.921	0.923	0.922	0.898	0.957	0.933	0.913	0.936	0.931	0.930	0.970	0.919	0.929	0.950	0.925
83	0.880	0.895	0.896	0.881	0.919	0.908	0.898	0.909	0.908	0.912	0.939	0.902	0.903	0.929	0.906
84	0.982	0.975	0.973	0.943	0.991	0.977	0.960	0.975	0.978	0.972	0.996	0.961	0.963	0.979	0.965

	76	77	78	79	80	81	82	83	84
76	1.000								
77	0.978	1.000							
78	0.972	0.998	1.000						
79	0.984	0.997	0.994	1.000					
80	0.954	0.989	0.993	0.988	1.000				
81	0.947	0.981	0.978	0.981	0.986	1.000			
82	0.945	0.982	0.982	0.984	0.992	0.993	1.000		
83	0.926	0.950	0.953	0.960	0.976	0.970	0.973	1.000	
84	0.967	0.985	0.983	0.977	0.975	0.952	0.951	0.925	1.000

FACTOR NUMBER	TEST NUMBER	FACTOR LOADING	VARIANCE %EIGENVALUE	EIGENVECTOR	ITERATIONS REQUIRED
1	1	0.87756	79.23934	0.09858	6
	2	0.89289		0.10031	
	3	0.91070		0.10231	
	4	0.92054		0.10341	
	5	0.92855		0.10431	
	6	0.92499		0.10391	
	7	0.93124		0.10461	
	8	0.91428		0.10271	
	9	0.95043		0.10677	
	10	0.94916		0.10663	
	11	0.92056		0.10341	
	12	0.93973		0.10557	
	13	0.94888		0.10660	
	14	0.95622		0.10742	
	15	0.97043		0.10902	
	16	0.96721		0.10866	
	17	0.95019		0.10674	
	18	0.96320		0.10820	
	19	0.94767		0.10646	
	20	0.98855		0.11105	
	21	0.97738		0.10980	
	22	0.98736		0.11092	
	23	0.98418		0.11056	
	24	0.97839		0.10991	
	25	0.98821		0.11101	
	26	0.96545		0.10846	
	27	0.99134		0.11137	
	28	0.99019		0.11124	
	29	0.98215		0.11033	
	30	0.98432		0.11058	
	31	0.96795		0.10874	
	32	0.98990		0.11120	
	33	0.99782		0.11209	
	34	0.97883		0.10996	
	35	0.98994		0.11121	
	36	0.99398		0.11166	
	37	0.97931		0.11001	
	38	0.99019		0.11124	
	39	0.97792		0.10986	
	40	0.98708		0.11089	
	41	0.99197		0.11144	
	42	0.99066		0.11129	
	43	0.99304		0.11156	
	44	0.98950		0.11116	
	45	0.98641		0.11081	
	46	0.99564		0.11185	
	47	0.99034		0.11125	
	48	0.99297		0.11155	
	49	0.97070		0.10905	
	50	0.99297		0.11155	
	51	0.99254		0.11150	
	52	0.98977		0.11119	
	53	0.98820		0.11101	
	54	0.99475		0.11175	
	55	0.99121		0.11135	
	56	0.98752		0.11094	
	57	0.98684		0.11086	
	58	0.99423		0.11169	
	59	0.98775		0.11096	
	60	0.98759		0.11094	
	61	0.98549		0.11071	
	62	0.99060		0.11128	
	63	0.98763		0.11095	
	64	0.97198		0.10919	
	65	0.98797		0.11099	
	66	0.99028		0.11125	
	67	0.97922		0.11000	
	68	0.98723		0.11090	
	69	0.98822		0.11102	
	70	0.98493		0.11065	
	71	0.98225		0.11035	
	72	0.97954		0.11004	
	73	0.97932		0.11002	
	74	0.98553		0.11071	
	75	0.97391		0.10941	
	76	0.97566		0.10960	
	77	0.97581		0.10962	
	78	0.97040		0.10901	
	79	0.96858		0.10881	
	80	0.94796		0.10649	
	81	0.92873		0.10433	
	82	0.92044		0.10340	
	83	0.89386		0.10042	
	84	0.98778		0.11097	

FACTOR NUMBER	TEST NUMBER	FACTOR LOADING	VARIANCE %EIGENVALUE	EIGENVECTOR	ITERATIONS REQUIRED
2	1	0.42176	2.47862	0.26789	14
	2	0.38767		0.24624	
	3	0.38798		0.24644	
	4	0.36881		0.23426	
	5	0.34968		0.22211	
	6	0.32477		0.20629	
	7	0.30336		0.19269	
	8	0.29612		0.18809	
	9	0.28326		0.17992	
	10	0.27289		0.17333	
	11	0.26552		0.16865	
	12	0.24616		0.15636	
	13	0.23655		0.15025	
	14	0.23909		0.15187	
	15	0.21204		0.13469	
	16	0.20298		0.12893	
	17	0.18776		0.11926	
	18	0.17467		0.11095	
	19	0.11282		0.07166	
	20	0.10692		0.06791	
	21	0.11610		0.07374	
	22	0.08405		0.05338	
	23	0.04185		0.02659	
	24	0.03992		0.02536	
	25	0.04345		0.02760	
	26	0.02923		0.01856	
	27	0.02906		0.01846	
	28	0.04674		0.02969	
	29	-0.00338		-0.00214	
	30	0.00936		0.00594	
	31	0.03012		0.01913	
	32	0.00991		0.00629	
	33	-0.00142		-0.00090	
	34	-0.00581		-0.00369	
	35	-0.01161		-0.00737	
	36	-0.01629		-0.01035	
	37	-0.03563		-0.02263	
	38	-0.03332		-0.02116	
	39	-0.04984		-0.03166	
	40	-0.04190		-0.02661	
	41	-0.05656		-0.03593	
	42	-0.06370		-0.04046	
	43	-0.07346		-0.04666	
	44	-0.05812		-0.03692	
	45	-0.15869		-0.10080	
	46	-0.05242		-0.03330	
	47	-0.06163		-0.03915	
	48	-0.07050		-0.04478	
	49	-0.08539		-0.05424	
	50	-0.07427		-0.04718	
	51	-0.06696		-0.04253	
	52	-0.06479		-0.04115	
	53	-0.08566		-0.05441	
	54	-0.07102		-0.04511	
	55	-0.09129		-0.05799	
	56	-0.09533		-0.06055	
	57	-0.08565		-0.05440	
	58	-0.10452		-0.06639	
	59	-0.08875		-0.05637	
	60	-0.10692		-0.06791	
	61	-0.10595		-0.06730	
	62	-0.09430		-0.05990	
	63	-0.11216		-0.07124	
	64	-0.10870		-0.06904	
	65	-0.12496		-0.07937	
	66	-0.11327		-0.07195	
	67	-0.11830		-0.07514	
	68	-0.12597		-0.08001	
	69	-0.12479		-0.07926	
	70	-0.12884		-0.08184	
	71	-0.14852		-0.09434	
	72	-0.12758		-0.08104	
	73	-0.13848		-0.08796	
	74	-0.15536		-0.09868	
	75	-0.15865		-0.10077	
	76	-0.16449		-0.10448	
	77	-0.18149		-0.11528	
	78	-0.20008		-0.12709	
	79	-0.20923		-0.13290	
	80	-0.22954		-0.14580	
	81	-0.26095		-0.16575	
	82	-0.30303		-0.19248	
	83	-0.31306		-0.19885	
	84	-0.07608		-0.04832	

FACTOR NUMBER	TEST NUMBER	FACTOR LOADING	VARIANCE %EIGENVALUE	EIGENVECTOR	ITERATIONS REQUIRED
3	1	-0.06333	0.72735	-0.07426	26
	2	0.17120		0.20073	
	3	0.09463		0.11096	
	4	0.03542		0.04153	
	5	0.02063		0.02419	
	6	0.16733		0.19621	
	7	0.09626		0.11287	
	8	0.08620		0.10107	
	9	-0.02242		-0.02629	
	10	-0.06236		-0.07312	
	11	-0.22702		-0.26619	
	12	0.01003		0.01176	
	13	0.03215		0.03770	
	14	-0.10465		-0.12271	
	15	0.00673		0.00789	
	16	-0.10960		-0.12851	
	17	-0.04945		-0.05798	
	18	-0.09364		-0.10980	
	19	0.26016		0.30505	
	20	-0.05708		-0.06692	
	21	-0.06411		-0.07517	
	22	0.05903		0.06922	
	23	-0.04704		-0.05516	
	24	-0.12653		-0.14836	
	25	0.03137		0.03678	
	26	0.05296		0.06210	
	27	-0.01628		-0.01909	
	28	-0.09775		-0.11462	
	29	0.13662		0.16019	
	30	-0.07246		-0.08496	
	31	-0.07322		-0.08585	
	32	-0.09241		-0.10836	
	33	-0.02533		-0.02970	
	34	-0.16951		-0.19876	
	35	0.04941		0.05793	
	36	0.05126		0.06011	
	37	0.14650		0.17178	
	38	0.07977		0.09354	
	39	0.14435		0.16926	
	40	-0.07156		-0.08390	
	41	0.04059		0.04759	
	42	0.01527		0.01790	
	43	0.00713		0.00836	
	44	-0.11786		-0.13820	
	45	0.01833		0.02149	
	46	0.00234		0.00274	
	47	0.04758		0.05579	
	48	-0.01894		-0.02220	
	49	0.19723		0.23126	
	50	0.02673		0.03135	
	51	0.02764		0.03240	
	52	-0.04332		-0.05080	
	53	0.02258		0.02647	
	54	-0.02784		-0.03265	
	55	-0.02435		-0.02855	
	56	0.10850		0.12723	
	57	-0.05153		-0.06043	
	58	0.00724		0.00849	
	59	0.00330		0.00387	
	60	0.08701		0.10203	
	61	0.01063		0.01247	
	62	-0.07844		-0.09197	
	63	-0.08648		-0.10140	
	64	-0.15216		-0.17842	
	65	0.05964		0.06994	
	66	-0.07173		-0.08411	
	67	-0.12367		-0.14501	
	68	-0.08302		-0.09735	
	69	-0.06572		-0.07706	
	70	-0.08454		-0.09913	
	71	0.10684		0.12527	
	72	-0.13738		-0.16109	
	73	-0.11997		-0.14067	
	74	-0.05308		-0.06224	
	75	-0.10115		-0.11861	
	76	-0.10893		-0.12773	
	77	0.06340		0.07434	
	78	0.09120		0.10694	
	79	0.02362		0.02770	
	80	0.14531		0.17038	
	81	0.09049		0.10610	
	82	0.12951		0.15186	
	83	0.06388		0.07491	
	84	0.11878		0.13927	

FACTOR NUMBER	TEST NUMBER	FACTOR LOADING	VARIANCE %EIGENVALUE	EIGENVECTOR	ITERATIONS REQUIRED
4	1	-0.15647	0.54935	-0.21111	20
	2	0.08268		0.11156	
	3	-0.03805		-0.05133	
	4	-0.06148		-0.08295	
	5	-0.05280		-0.07123	
	6	0.05599		0.07554	
	7	-0.03825		-0.05161	
	8	-0.15123		-0.20404	
	9	-0.01679		-0.02266	
	10	-0.05678		-0.07661	
	11	-0.14544		-0.19623	
	12	-0.03108		-0.04194	
	13	0.09049		0.12209	
	14	-0.00080		-0.00108	
	15	-0.03377		-0.04556	
	16	0.01570		0.02118	
	17	-0.13886		-0.18735	
	18	-0.05386		-0.07267	
	19	0.05178		0.06986	
	20	-0.06410		-0.08648	
	21	-0.02098		-0.02830	
	22	0.06893		0.09299	
	23	0.02946		0.03975	
	24	0.06025		0.08129	
	25	0.12252		0.16530	
	26	0.07685		0.10368	
	27	0.01077		0.01454	
	28	0.03722		0.05022	
	29	0.08310		0.11212	
	30	0.08026		0.10828	
	31	-0.16070		-0.21681	
	32	0.04277		0.05770	
	33	0.02740		0.03697	
	34	0.02520		0.03401	
	35	0.02167		0.02924	
	36	0.08573		0.11566	
	37	0.12217		0.16483	
	38	0.06088		0.08214	
	39	0.12687		0.17118	
	40	-0.02852		-0.03847	
	41	0.06345		0.08560	
	42	0.09125		0.12311	
	43	0.06467		0.08726	
	44	0.03551		0.04791	
	45	-0.01804		-0.02433	
	46	-0.00151		-0.00204	
	47	-0.07995		-0.10787	
	48	0.07782		0.10500	
	49	-0.01214		-0.01638	
	50	0.03198		0.04314	
	51	0.06716		0.09062	
	52	0.07169		0.09672	
	53	0.02367		0.03193	
	54	0.04604		0.06212	
	55	0.05870		0.07919	
	56	0.02848		0.03843	
	57	-0.10797		-0.14567	
	58	-0.00830		-0.01120	
	59	0.11036		0.14890	
	60	0.02089		0.02818	
	61	0.08589		0.11589	
	62	0.04255		0.05740	
	63	0.04173		0.05631	
	64	0.07790		0.10510	
	65	-0.00324		-0.00437	
	66	0.02213		0.02986	
	67	0.03784		0.05105	
	68	0.00485		0.00655	
	69	0.02971		0.04009	
	70	0.02280		0.03076	
	71	-0.03418		-0.04612	
	72	0.02586		0.03488	
	73	0.00473		0.00638	
	74	-0.00903		-0.01219	
	75	0.02680		0.03615	
	76	-0.05663		-0.07641	
	77	-0.07990		-0.10780	
	78	-0.06653		-0.08977	
	79	-0.11010		-0.14855	
	80	-0.15213		-0.20525	
	81	-0.22433		-0.30266	
	82	-0.19763		-0.26664	
	83	-0.25505		-0.34411	
	84	-0.03348		-0.04517	

FACTOR NUMBER	TEST NUMBER	FACTOR LOADING	VARIANCE %EIGENVALUE	EIGENVECTOR	ITERATIONS REQUIRED
5	1	0.10868	0.35204	0.18316	20
	2	-0.12329		-0.20780	
	3	0.00803		0.01354	
	4	0.05877		0.09905	
	5	0.06784		0.11434	
	6	-0.02828		-0.04766	
	7	-0.07200		-0.12136	
	8	0.15152		0.25537	
	9	-0.10769		-0.18150	
	10	0.05290		0.08916	
	11	0.07503		0.12646	
	12	0.10930		0.18422	
	13	-0.11533		-0.19437	
	14	-0.09803		-0.16521	
	15	-0.08571		-0.14446	
	16	-0.07713		-0.13000	
	17	0.08951		0.15086	
	18	-0.02908		-0.04902	
	19	-0.12032		-0.20279	
	20	-0.02978		-0.05020	
	21	-0.14725		-0.24817	
	22	-0.00294		-0.00495	
	23	0.05017		0.08456	
	24	-0.13010		-0.21928	
	25	0.02905		0.04897	
	26	0.02184		0.03680	
	27	-0.04292		-0.07233	
	28	0.02129		0.03589	
	29	0.08466		0.14269	
	30	-0.11076		-0.18668	
	31	0.04048		0.06822	
	32	-0.03163		-0.05331	
	33	-0.04347		-0.07327	
	34	-0.06361		-0.10721	
	35	-0.08665		-0.14604	
	36	0.00631		0.01064	
	37	0.05180		0.08730	
	38	0.08862		0.14935	
	39	0.05791		0.09761	
	40	0.06091		0.10265	
	41	0.07898		0.13311	
	42	0.07125		0.12008	
	43	0.05073		0.08551	
	44	-0.03115		-0.05250	
	45	-0.00862		-0.01452	
	46	-0.06594		-0.11114	
	47	-0.01262		-0.02126	
	48	0.04830		0.08141	
	49	-0.05545		-0.09346	
	50	0.07278		0.12266	
	51	0.06335		0.10676	
	52	-0.01765		-0.02975	
	53	0.10875		0.18329	
	54	0.03437		0.05793	
	55	0.06733		0.11347	
	56	0.03565		0.06009	
	57	-0.00600		-0.01011	
	58	-0.01194		-0.02012	
	59	0.00494		0.00833	
	60	0.05263		0.08870	
	61	0.07819		0.13178	
	62	0.00764		0.01288	
	63	0.03986		0.06719	
	64	-0.09022		-0.15206	
	65	0.00314		0.00529	
	66	0.00517		0.00872	
	67	-0.02303		-0.03882	
	68	0.02267		0.03822	
	69	0.03884		0.06547	
	70	-0.00693		-0.01168	
	71	-0.00327		-0.00551	
	72	-0.00855		-0.01441	
	73	0.01079		0.01818	
	74	-0.01139		-0.01919	
	75	0.03238		0.05458	
	76	0.03704		0.06244	
	77	-0.05444		-0.09176	
	78	-0.05548		-0.09351	
	79	-0.04902		-0.08262	
	80	-0.04206		-0.07089	
	81	-0.04369		-0.07363	
	82	-0.05137		-0.08659	
	83	-0.05828		-0.09823	
	84	0.04419		0.07448	

PRINT OUT OF RESIDUAL MATRIX -LOWER HALF -ELEMENT%1,10 TO ELEMENT % 84, 840

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	0.012														
2	0.000	0.001													
3	0.009	0.001	0.010												
4	-0.003	-0.001	0.001	0.008											
5	0.002	-0.001	0.003	0.006	0.008										
6	-0.001	-0.000	-0.002	-0.001	-0.004	0.007									
7	-0.009	0.000	-0.009	-0.002	-0.008	0.011	0.025								
8	-0.002	-0.001	-0.007	-0.003	-0.004	0.007	0.013	0.023							
9	0.004	0.001	0.003	-0.004	-0.002	-0.000	-0.003	0.002	0.004						
10	-0.007	-0.001	-0.002	0.010	0.006	-0.001	0.003	-0.001	-0.005	0.015					
11	0.001	-0.001	-0.001	0.001	0.003	-0.002	-0.003	-0.000	0.000	0.001	0.004				
12	-0.017	0.000	-0.008	0.008	0.004	-0.009	-0.005	-0.014	-0.007	0.013	-0.000	0.043			
13	-0.003	0.002	0.000	-0.002	-0.001	-0.008	-0.010	-0.016	0.001	-0.003	0.001	0.019	0.021		
14	-0.006	0.000	-0.006	-0.001	-0.003	0.004	0.012	0.005	-0.001	0.002	0.001	0.001	-0.001	0.008	
15	-0.006	-0.000	-0.006	-0.000	-0.003	0.004	0.010	0.007	-0.001	0.002	-0.000	0.001	-0.003	0.005	0.005
16	0.001	-0.002	-0.001	0.001	0.002	0.001	0.000	0.000	-0.003	0.001	0.002	-0.003	-0.004	-0.000	0.001
17	0.001	0.000	-0.004	-0.012	-0.012	0.009	0.015	0.001	0.001	-0.014	-0.002	-0.014	-0.000	0.007	0.005
18	0.014	0.002	0.012	-0.009	-0.003	-0.003	-0.015	-0.003	0.009	-0.015	-0.003	-0.016	0.003	-0.010	-0.008
19	-0.002	0.000	0.001	0.004	0.003	-0.003	-0.005	-0.006	-0.001	0.005	-0.001	0.011	0.005	-0.003	-0.002
20	0.005	-0.000	0.003	-0.002	0.001	-0.002	-0.006	0.000	0.002	-0.004	0.001	-0.005	0.001	-0.003	-0.003
21	-0.003	-0.001	-0.005	-0.001	-0.001	0.003	0.007	0.008	-0.001	0.000	0.002	-0.003	-0.005	0.004	0.004
22	0.004	-0.000	0.005	0.001	0.005	-0.007	-0.015	-0.008	0.001	-0.001	0.001	0.006	0.006	-0.008	-0.006
23	-0.005	0.002	-0.005	-0.008	-0.006	-0.006	-0.004	-0.006	0.002	-0.009	0.001	0.015	0.018	0.001	0.000
24	0.000	-0.002	-0.003	-0.001	0.000	0.002	0.004	0.005	-0.001	-0.001	0.002	-0.006	-0.005	0.002	0.002
25	0.003	-0.000	0.002	-0.001	0.002	-0.004	-0.009	-0.003	0.001	-0.003	0.001	0.002	0.004	-0.005	-0.003
26	-0.008	-0.004	-0.007	0.012	0.005	0.012	0.021	0.014	-0.010	0.018	-0.003	-0.004	-0.027	0.006	0.009
27	-0.006	0.001	-0.005	-0.003	-0.002	-0.006	-0.004	-0.006	0.000	-0.002	0.002	0.017	0.015	0.002	0.000
28	0.004	-0.000	0.001	-0.005	-0.002	-0.001	-0.003	-0.003	0.001	-0.008	0.001	-0.005	0.003	-0.002	-0.002
29	0.003	0.001	0.002	-0.002	-0.000	-0.002	-0.003	-0.003	0.002	-0.003	0.002	-0.003	0.004	-0.000	-0.002
30	-0.003	-0.002	-0.005	0.001	0.001	0.002	0.006	0.005	-0.002	0.002	0.003	-0.002	-0.004	0.005	0.003
31	0.003	-0.000	0.008	0.001	0.003	-0.006	-0.016	-0.020	-0.002	-0.002	-0.004	0.013	0.011	-0.011	-0.007
32	0.005	0.000	0.006	0.001	0.003	-0.003	-0.011	-0.004	0.002	-0.002	-0.002	-0.001	0.001	-0.008	-0.005
33	0.001	-0.001	0.001	0.001	0.002	-0.001	-0.004	-0.001	-0.000	0.001	-0.000	0.001	-0.000	-0.002	-0.001
34	0.005	0.001	0.007	0.003	0.003	-0.002	-0.008	-0.002	0.002	0.002	-0.002	-0.002	-0.002	-0.006	-0.004
35	0.002	-0.001	0.001	0.003	0.005	-0.003	-0.007	0.006	0.001	0.002	0.000	-0.001	-0.005	-0.005	-0.002
36	0.001	0.001	0.002	-0.000	-0.001	-0.000	-0.002	-0.001	0.001	-0.001	-0.002	0.001	0.001	-0.002	-0.001
37	0.000	0.000	0.001	-0.000	-0.001	0.000	0.000	-0.003	-0.000	-0.000	-0.000	0.001	0.002	-0.000	-0.000
38	0.000	0.000	-0.000	-0.001	-0.001	-0.000	0.000	0.001	0.001	-0.001	0.000	-0.001	0.001	0.001	0.000
39	0.001	-0.000	0.000	-0.001	0.000	-0.002	-0.003	-0.003	0.000	-0.001	0.001	0.002	0.003	-0.001	-0.001
40	-0.010	0.000	-0.009	-0.003	-0.006	0.002	0.010	0.006	-0.001	0.000	-0.004	0.012	0.002	0.005	0.006
41	0.001	0.001	0.001	-0.000	-0.000	0.000	0.000	0.001	0.001	-0.001	0.001	-0.003	0.000	0.001	-0.000
42	0.002	0.001	0.002	-0.001	-0.000	-0.000	-0.002	0.000	0.002	-0.001	0.000	-0.003	-0.000	-0.001	-0.001
43	0.003	-0.000	0.001	0.000	0.002	-0.001	-0.003	-0.001	0.000	-0.000	0.002	-0.003	-0.000	-0.001	-0.001
44	0.000	0.000	0.002	0.002	0.000	0.001	0.001	-0.001	-0.000	0.002	-0.001	-0.001	-0.002	-0.001	-0.000
45	0.002	-0.001	0.001	0.000	0.002	-0.001	-0.003	0.001	0.000	-0.000	0.001	-0.002	-0.001	-0.002	-0.001
46	-0.002	-0.001	-0.001	0.001	0.001	0.000	0.000	0.001	-0.002	0.002	-0.001	0.004	-0.001	-0.001	0.001
47	0.003	0.002	0.005	-0.001	0.001	-0.005	-0.009	-0.009	0.002	-0.003	0.001	0.003	0.009	-0.003	-0.004
48	-0.000	0.000	-0.000	-0.001	-0.000	-0.001	-0.000	-0.001	0.000	-0.000	0.000	0.001	0.002	-0.001	0.000
49	0.002	0.000	-0.000	-0.006	-0.006	0.005	0.007	0.001	0.001	-0.008	-0.002	-0.009	-0.001	0.002	0.001
50	0.001	0.001	0.001	0.000	0.000	0.000	0.000	0.002	0.001	0.000	0.001	-0.003	-0.001	0.001	-0.000
51	0.002	0.001	0.002	-0.000	0.001	-0.001	-0.001	-0.000	0.001	-0.000	0.001	-0.003	0.000	-0.000	-0.001
52	0.004	0.000	0.004	0.001	0.002	0.000	-0.004	0.006	0.002	0.000	-0.002	-0.006	-0.007	-0.005	-0.002
53	0.000	0.000	-0.000	0.001	0.001	-0.000	0.001	-0.000	0.000	0.001	0.003	-0.002	0.001	0.003	0.000
54	0.002	0.000	0.001	-0.003	-0.002	0.001	0.001	0.000	0.001	-0.004	-0.000	-0.006	-0.001	0.000	-0.000
55	0.000	0.000	-0.000	-0.001	-0.001	0.000	0.001	0.002	0.001	-0.001	0.000	-0.002	0.000	0.001	0.000
56	0.003	-0.001	0.001	0.000	0.002	-0.001	-0.003	-0.002	0.000	-0.001	0.002	-0.003	-0.000	-0.001	-0.001
57	-0.005	-0.000	-0.005	-0.001	-0.003	0.003	0.008	0.005	-0.002	-0.000	-0.002	0.002	-0.003	0.003	0.004
58	0.000	0.000	0.000	0.001	0.001	0.000	0.000	-0.000	-0.000	0.001	0.001	-0.001	-0.000	0.001	-0.000
59	0.004	-0.001	0.003	0.000	0.002	-0.001	-0.007	-0.002	0.000	-0.002	-0.001	-0.002	-0.001	-0.005	-0.003
60	0.001	-0.000	-0.000	-0.001	0.001	-0.002	-0.002	-0.001	0.001	-0.002	0.003	-0.002	0.002	0.001	-0.001
61	0.001	-0.001	-0.001	-0.003	-0.002	0.003	0.004	0.004	-0.000	-0.004	-0.000	-0.008	-0.005	0.001	0.002
62	-0.001	0.000	0.000	0.001	-0.001	0.002	0.004	-0.002	-0.001	0.001	-0.000	-0.000	-0.000	0.002	0.001
63	-0.000	0.000	-0.001	-0.002	-0.002	0.002	0.004	0.004	0.001	-0.001	-0.000	-0.004	-0.002	0.002	0.002
64	0.003	0.001	0.004	0.002	0.002	-0.002	-0.002	-0.007	0.000	0.001	0.002	-0.001	0.004	0.001	-0.002
65	-0.002	-0.001	-0.004	-0.004	-0.004	0.003	0.007	0.004	-0.001	-0.004	0.000	-0.003	-0.001	0.004	0.003
66	-0.000	0.001	0.001	-0.000	-0.001	0.001	0.002	-0.001	0.000	0.000	-0.000	-0.001	0.001	0.001	0.000
67	-0.001	0.002	0.001	-0.003	-0.003	-0.004	-0.005	-0.009	0.002	-0.004	0.000	0.010	0.014	-0.001	-0.002
68	-0.000	0.000	-0.000	-0.000	-0.002	0.003	0.005	0.000	-0.001	0.001	-0.000	-0.003	-0.002	0.002	0.001
69	0.002	-0.000	0.001	-0.001	-0.000	0.001	0.001	0.004	0.001	-0.001	0.000	-0.006	-0.003	0.000	0.000
70	0.005	-0.001	0.003	0.000	0.002	0.000	-0.004	0.005	0.002	-0.001	-0.000	-0.009	-0.007	-0.004	-0.002
71	-0.001	-0.000	-0.001	-0.000	-0.001	0.000	0.001	-0.001	-0.001	0.000	-0.001	0.003	0.001	0.000	0.000
72	-0.003	-0.000	-0.000	0.005	0.002	0.002	0.003	0.002	-0.002	0.007	-0.002	0.003	-0.005	0.000	0.001
73	-0.000	-0.000	-0.001	0.002	-0.001	0.006	0.010	0.008	-0.001	0.003	-0.002	-0.009	-0.011	0.003	0.003
74	-0.002	0.001	0.000	0.001	-0.001	0.001	0.002	-0.000	-0.000	0.002	-0.002	0.003	0.001	0.001	0.000
75	-0.013	0.000	-0.009	0.004	-0.002	0.002	0.011	0.003	-0.005	0.009	-0.001	0.017	0.001	0.007	0.006
76	-0.004	-0.000	-0.002	0.003	0.000	0.004	0.007	0.003	-0.002	0.006	-0.002	0.002	-0.005	0.002	0.003
77	0.001	-0.000	0.000	-0.001	-0.002	0.003	0.003	0.000	-0.000	-0.002	-0.001	-0.004	-0.002	0.000	0.001
78	0.004	-0.001	0.002	-0.001	0.000	0.002	0.000	0.003	0.001	-0.002	-0.000	-0.009	-0.006	-0.001	-0.001
79	-0.004	-0.000	-0.004	0.000	-0.002	0.003	0.008	0.005	-0.002	0.002	-0.000	-0.000	-0.004	0.004	

	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
16	0.005														
17	0.002	0.032													
18	-0.005	0.002	0.029												
19	-0.002	-0.009	-0.001	0.004											
20	0.000	-0.001	0.007	-0.001	0.003										
21	0.002	0.004	-0.007	-0.003	-0.001	0.005									
22	-0.000	-0.010	0.008	0.004	0.004	-0.004	0.010								
23	-0.004	0.008	0.005	0.001	0.001	-0.001	0.003	0.024							
24	0.004	0.004	-0.005	-0.003	0.000	0.004	-0.002	-0.002	0.005						
25	0.000	-0.005	0.007	0.002	0.003	-0.002	0.006	0.004	-0.001	0.005					
26	0.008	-0.004	-0.026	-0.001	-0.008	0.007	-0.011	-0.028	0.005	-0.009	0.058				
27	-0.002	0.000	-0.002	0.002	0.000	-0.000	0.003	0.017	-0.001	0.003	-0.018	0.014			
28	0.002	0.009	0.007	-0.002	0.002	-0.000	0.002	0.006	0.001	0.002	-0.010	0.002	0.006		
29	-0.001	0.001	0.004	-0.001	0.001	-0.001	0.001	0.002	-0.000	0.000	-0.010	0.001	0.002	0.003	
30	0.004	0.004	-0.011	-0.003	-0.001	0.005	-0.004	-0.002	0.005	-0.002	0.009	-0.000	-0.000	-0.000	0.007
31	-0.001	-0.004	0.012	0.007	0.001	-0.010	0.012	0.005	-0.007	0.006	-0.009	0.002	0.004	-0.001	-0.010
32	-0.001	-0.008	0.011	0.003	0.003	-0.005	0.008	-0.002	-0.003	0.005	-0.005	-0.002	0.001	-0.000	-0.006
33	0.001	-0.004	0.001	0.001	0.001	-0.001	0.003	-0.001	-0.000	0.002	0.001	-0.001	-0.000	-0.001	-0.001
34	-0.003	-0.011	0.008	0.003	0.002	-0.005	0.004	-0.006	-0.004	0.002	-0.001	-0.005	-0.003	0.000	-0.006
35	0.000	-0.013	0.003	0.002	0.003	-0.000	0.005	-0.005	0.000	0.004	0.003	-0.002	-0.002	-0.002	-0.001
36	-0.002	-0.002	0.005	0.001	0.000	-0.002	0.002	0.001	-0.002	0.001	-0.002	-0.000	-0.000	-0.000	-0.003
37	-0.000	0.002	0.001	0.000	-0.000	-0.001	-0.000	0.001	-0.001	-0.000	-0.002	0.000	0.001	0.000	-0.001
38	-0.001	0.001	0.001	-0.001	0.000	0.000	-0.000	0.002	0.000	-0.000	-0.004	0.001	0.000	0.001	0.000
39	0.000	0.000	0.001	0.000	0.001	-0.000	0.002	0.003	0.000	0.001	-0.005	0.002	0.002	0.001	0.000
40	-0.003	0.004	-0.006	0.000	-0.003	0.003	-0.004	0.009	-0.001	-0.001	0.003	0.006	-0.002	-0.004	-0.000
41	-0.001	0.000	0.001	-0.001	0.000	-0.000	-0.001	-0.000	0.000	-0.001	-0.003	-0.000	-0.000	0.001	0.000
42	-0.001	-0.001	0.003	-0.000	0.001	-0.001	0.000	-0.001	-0.001	0.000	-0.004	-0.001	0.000	0.001	-0.001
43	0.001	-0.001	0.000	-0.001	0.001	0.000	0.001	-0.001	0.001	0.001	-0.002	-0.000	0.001	0.001	0.001
44	-0.001	-0.001	0.000	0.001	-0.001	-0.001	-0.001	-0.004	-0.001	-0.001	0.005	-0.003	-0.001	-0.001	-0.001
45	0.001	-0.002	0.001	-0.000	0.001	0.000	0.002	-0.001	0.001	0.002	0.000	-0.001	0.001	-0.000	0.000
46	0.001	-0.002	-0.002	0.001	-0.001	0.000	0.001	-0.001	-0.000	0.001	0.005	-0.000	-0.001	-0.002	-0.000
47	-0.003	-0.002	0.008	0.002	0.002	-0.004	0.005	0.006	-0.003	0.003	-0.017	0.004	0.002	0.003	-0.004
48	-0.001	0.001	-0.000	-0.000	0.000	0.000	-0.000	0.002	-0.000	-0.000	-0.003	0.002	0.000	0.001	0.000
49	0.000	0.016	0.004	-0.004	-0.000	0.001	-0.004	0.002	0.001	-0.002	-0.002	-0.002	0.005	0.000	-0.000
50	-0.001	-0.001	0.000	-0.001	0.000	0.000	-0.001	-0.002	0.000	-0.001	-0.001	-0.001	-0.001	0.001	0.000
51	-0.001	-0.001	0.002	-0.000	0.001	-0.001	0.000	-0.001	-0.000	-0.000	-0.003	-0.001	-0.000	0.001	-0.000
52	-0.002	-0.009	0.008	0.001	0.002	-0.002	0.003	-0.006	-0.002	0.002	0.004	-0.006	-0.002	-0.001	-0.004
53	0.000	0.001	-0.004	-0.001	-0.000	0.001	-0.002	-0.001	0.002	-0.002	-0.002	0.001	-0.000	0.002	0.003
54	0.000	0.005	0.003	-0.002	0.001	0.000	-0.001	0.000	0.001	-0.000	-0.003	-0.001	0.002	0.001	0.000
55	-0.001	0.001	0.001	-0.001	0.000	0.001	-0.001	0.001	0.000	-0.000	-0.003	0.001	-0.000	0.001	0.000
56	0.002	-0.000	0.000	-0.001	0.001	0.000	0.002	-0.001	0.002	0.001	-0.002	-0.000	0.001	0.001	0.001
57	0.000	0.005	-0.004	-0.001	-0.002	0.002	-0.003	0.001	0.001	-0.002	0.008	0.000	-0.000	-0.003	0.001
58	0.000	-0.000	-0.001	-0.000	-0.000	0.000	-0.001	-0.001	0.000	-0.001	0.001	-0.001	-0.000	0.000	0.001
59	0.001	-0.003	0.006	0.001	0.002	-0.002	0.005	-0.002	-0.001	0.003	0.000	-0.002	0.001	-0.001	-0.003
60	0.001	0.001	-0.000	-0.001	0.001	0.001	0.001	0.002	0.002	0.001	-0.006	0.002	0.002	0.002	0.002
61	0.003	0.008	-0.006	-0.004	0.000	0.003	-0.003	-0.002	0.003	-0.001	0.005	-0.003	0.003	-0.001	0.003
62	0.000	0.003	-0.003	-0.000	-0.002	-0.000	-0.003	-0.002	-0.000	-0.002	0.003	-0.001	-0.000	0.000	0.001
63	-0.000	0.004	-0.001	-0.002	-0.000	0.002	-0.003	0.000	0.001	-0.002	0.001	-0.001	0.000	0.000	0.001
64	-0.000	-0.000	-0.001	0.000	-0.000	-0.002	-0.000	-0.002	-0.000	-0.001	-0.005	-0.000	0.000	0.003	0.001
65	0.002	0.010	-0.003	-0.003	-0.001	0.004	-0.004	0.003	0.003	-0.002	0.002	0.001	0.002	-0.000	0.003
66	-0.001	0.002	-0.000	-0.000	-0.001	-0.000	-0.002	-0.000	-0.001	-0.001	-0.000	-0.001	-0.000	0.001	-0.000
67	-0.004	0.003	0.005	0.002	0.001	-0.004	0.003	0.013	-0.004	0.002	-0.020	0.009	0.003	0.003	-0.004
68	0.000	0.005	-0.003	-0.001	-0.002	0.001	-0.004	-0.002	0.000	-0.003	0.004	-0.002	-0.000	0.000	0.001
69	0.000	0.000	0.002	-0.001	0.001	0.001	-0.001	-0.002	0.001	-0.000	0.001	-0.002	-0.000	0.000	0.001
70	0.001	-0.005	0.006	-0.001	0.003	-0.000	0.002	-0.006	0.001	0.002	0.003	-0.005	-0.000	-0.001	-0.001
71	0.000	0.001	-0.001	0.000	-0.001	-0.000	0.000	0.001	-0.000	0.000	0.001	0.001	0.000	-0.001	-0.000
72	-0.001	-0.006	-0.005	0.002	-0.002	-0.000	-0.001	-0.007	-0.001	-0.002	0.012	-0.004	-0.005	-0.002	-0.001
73	0.000	0.002	-0.004	-0.002	-0.002	0.002	-0.006	-0.010	0.001	-0.004	0.016	-0.008	-0.003	-0.002	0.002
74	-0.002	-0.001	-0.000	0.001	-0.001	-0.001	-0.001	-0.000	-0.002	-0.001	0.002	-0.000	-0.002	-0.000	-0.002
75	-0.001	-0.001	-0.016	0.002	-0.006	0.003	-0.006	0.003	-0.000	-0.004	0.012	0.005	-0.006	-0.003	0.003
76	0.000	-0.001	-0.007	0.001	-0.003	0.001	-0.004	-0.006	-0.000	-0.003	0.014	-0.004	-0.004	-0.003	0.001
77	0.001	0.005	0.001	-0.001	-0.001	0.000	-0.002	-0.002	0.000	-0.001	0.004	-0.003	0.001	-0.001	0.000
78	0.001	0.002	0.003	-0.002	0.001	0.001	-0.000	-0.005	0.001	0.000	0.004	-0.005	0.001	-0.000	0.000
79	0.001	0.003	-0.007	-0.002	-0.002	0.003	-0.005	-0.002	0.002	-0.003	0.009	-0.001	-0.002	-0.001	0.003
80	0.000	-0.007	0.001	0.001	0.001	-0.000	0.002	-0.005	0.000	0.001	0.003	-0.003	-0.002	-0.000	0.000
81	-0.001	0.011	0.006	-0.001	0.001	-0.002	0.001	0.009	-0.001	0.000	-0.015	0.005	0.006	0.003	-0.001
82	0.001	0.005	-0.003	-0.001	-0.002	0.001	-0.003	-0.004	0.001	-0.003	0.007	-0.003	0.000	-0.001	0.001
83	-0.002	-0.028	-0.003	0.007	0.003	-0.002	0.009	0.002	-0.002	0.005	-0.010	0.007	-0.006	0.002	-0.001
84	-0.000	-0.005	-0.002	0.002	-0.000	-0.001	0.002	0.001	-0.001	0.001	0.001	0.002	-0.001	-0.001	-0.001

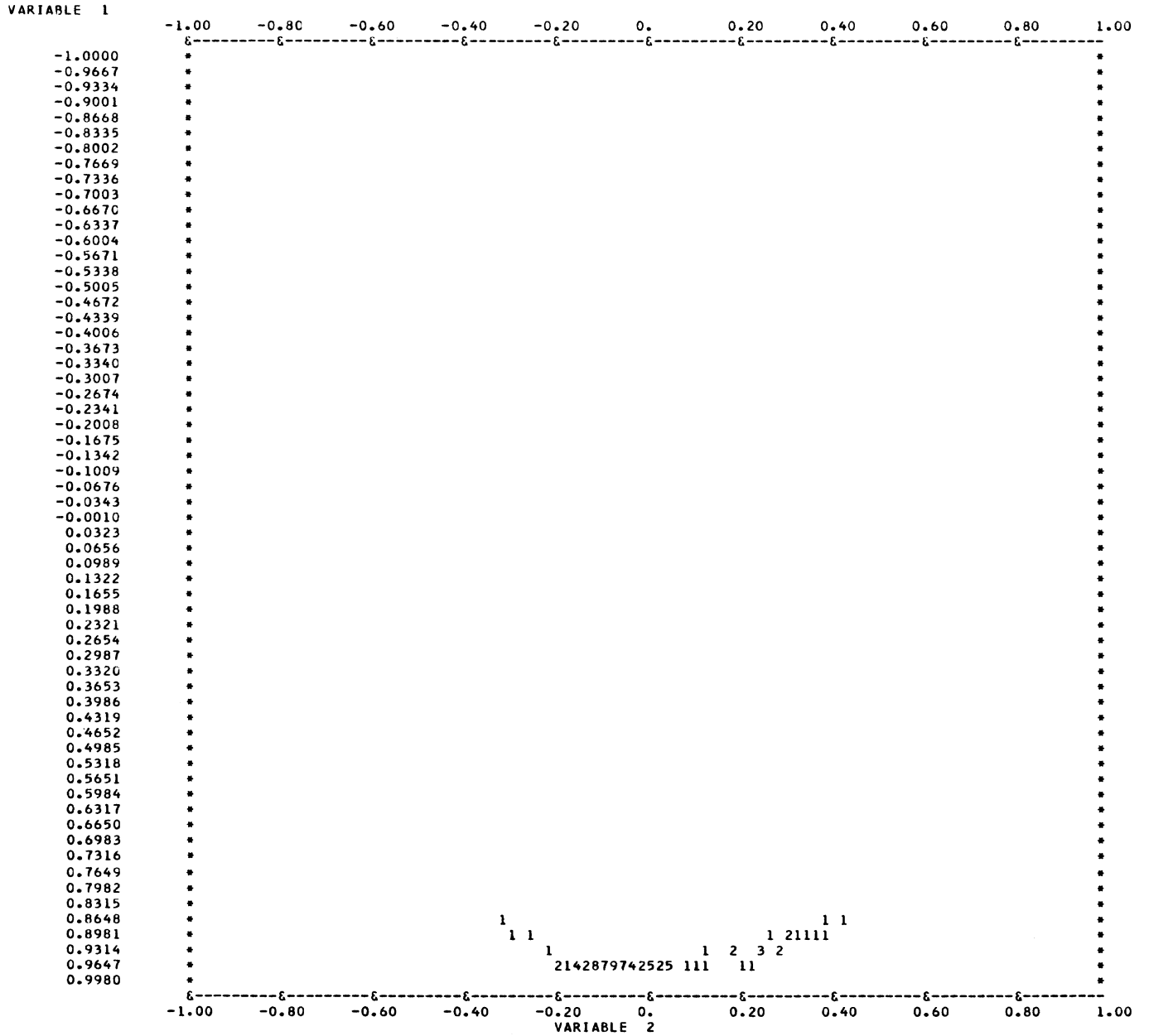
	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45
31	0.029														
32	0.011	0.009													
33	0.003	0.002	0.001												
34	0.006	0.007	0.002	0.008											
35	-0.000	0.005	0.002	0.005	0.009										
36	0.004	0.003	0.001	0.003	0.001	0.002									
37	0.002	-0.000	-0.000	-0.000	-0.002	0.000	0.001								
38	-0.002	-0.001	-0.001	-0.000	-0.001	-0.000	0.000	0.000							
39	0.002	0.000	0.000	-0.001	-0.001	-0.000	0.000	0.000	0.001						
40	-0.002	-0.003	-0.001	-0.005	-0.001	0.001	-0.000	0.000	-0.001	0.014					
41	-0.003	-0.001	-0.001	0.000	-0.001	-0.000	0.000	0.000	0.000	-0.002	0.001				
42	-0.001	0.001	-0.000	0.002	0.000	0.000	-0.000	0.000	0.000	-0.002	0.001	0.001			
43	-0.002	-0.000	0.000	-0.000	0.001	-0.001	-0.000	0.000	0.001	-0.004	0.001	0.000	0.002		
44	0.002	0.001	0.000	0.002	-0.000	0.001	0.000	-0.000	-0.001	-0.001	-0.000	0.000	-0.001	0.001	
45	0.001	0.002	0.001	0.001	0.002	-0.000	-0.001	-0.000	0.000	-0.002	-0.000	0.000	-0.002	-0.000	0.001
46	0.003	0.001	0.001	0.000	0.002	0.000	-0.000	-0.001	-0.000	0.002	-0.001	-0.001	-0.001	0.000	0.000
47	0.006	0.003	0.000	0.003	-0.001	0.001	0.001	0.001	0.002	-0.004	0.001	0.001	0.001	-0.000	-0.000
48	-0.001	-0.001	-0.000	-0.001	-0.001	-0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	-0.000	-0.000
49	0.000	-0.002	-0.002	-0.004	-0.006	-0.000	0.001	0.000	-0.000	0.002	-0.000	-0.000	-0.001	0.000	-0.001
50	-0.005	-0.001	-0.000	0.001	0.000	-0.000	-0.000	0.000	-0.000	-0.002	0.001	0.001	0.001	0.000	-0.000
51	-0.002	0.000	-0.000	0.001	-0.000	-0.000	0.000	0.000	0.000	-0.003	0.001	0.001	0.001	0.000	0.000
52	0.002	0.006	0.002	0.007	0.007	0.003	-0.001	-0.001	-0.001	-0.001	-0.000	0.001	-0.001	0.001	0.001
53	-0.006	-0.003	-0.001	-0.001	-0.002	-0.002	0.000	0.001	0.000	-0.003	0.001	0.001	0.001	-0.001	-0.000
54	-0.001	-0.000	-0.001	-0.001	-0.002	-0.000	0.000	0.000	0.000	-0.001	0.000	0.000	0.000	-0.000	-0.000
55	-0.003	-0.001	-0.001	-0.000	-0.000	-0.000	-0.000	0.000	-0.000	0.000	0.001	0.000	0.000	-0.000	-0.000
56	-0.000	0.000	0.000	-0.000	0.001	-0.001	-0.000	0.000	0.001	-0.004	0.000	0.000	0.002	-0.001	0.001
57	-0.001	-0.002	-0.000	-0.003	-0.001	0.000	-0.000	-0.000	-0.001	0.007	-0.001	-0.001	-0.002	0.000	-0.001
58	-0.001	-0.001	-0.000	0.000	-0.000	-0.000	0.000	0.000	-0.000	-0.001	0.000	0.000	0.000	0.000	-0.000
59	0.008	0.005	0.002	0.003	0.004	0.001	-0.000	-0.001	0.000	-0.002	-0.001	-0.000	0.000	0.000	0.001
60	-0.003	-0.001	-0.000	-0.002	-0.000	-0.001	-0.000	0.001	0.001	-0.003	0.001	0.000	0.002	-0.001	0.001
61	-0.003	-0.002	-0.000	-0.003	-0.001	-0.001	-0.000	-0.000	-0.000	0.000	-0.000	-0.000	0.000	-0.000	0.000
62	-0.000	-0.002	-0.001	-0.001	-0.003	-0.000	0.001	-0.000	-0.000	-0.001	0.000	-0.000	-0.000	0.001	-0.001
63	-0.005	-0.002	-0.001	-0.002	-0.001	-0.000	-0.000	0.000	-0.000	0.001	0.000	0.000	-0.000	-0.000	-0.000
64	-0.000	-0.001	-0.001	0.001	-0.004	-0.001	0.001	0.000	0.001	-0.007	0.001	0.001	0.002	0.000	-0.000
65	-0.005	-0.005	-0.001	-0.006	-0.003	-0.001	0.000	0.000	0.000	0.004	-0.000	-0.001	-0.000	-0.001	-0.001
66	-0.001	-0.001	-0.001	0.000	-0.002	0.000	0.001	0.000	-0.000	-0.000	0.000	0.000	-0.000	0.001	-0.001
67	0.007	0.000	-0.001	-0.001	-0.005	0.001	0.002	0.001	0.002	0.002	0.000	0.000	-0.000	-0.001	-0.001
68	-0.002	-0.003	-0.001	-0.001	-0.003	-0.001	0.001	0.000	-0.001	-0.000	0.000	-0.000	-0.000	0.001	-0.001
69	-0.004	-0.000	-0.000	0.001	0.001	-0.000	-0.000	0.000	-0.000	-0.001	0.001	0.001	0.001	0.000	0.000
70	-0.001	0.004	0.001	0.004	0.006	0.001	-0.001	-0.000	-0.001	-0.003	0.000	0.001	0.001	0.000	0.002
71	0.002	-0.000	0.000	-0.001	-0.001	0.000	0.000	-0.000	0.000	0.002	-0.001	-0.001	-0.001	0.000	-0.000
72	0.000	0.001	0.001	0.003	0.002	0.001	-0.000	-0.001	0.002	0.001	-0.001	-0.000	-0.001	0.002	-0.000
73	-0.007	-0.002	-0.001	0.001	-0.000	-0.000	-0.000	-0.000	-0.002	0.000	0.000	0.000	-0.001	0.002	-0.001
74	0.001	0.000	-0.000	0.001	-0.001	0.001	0.000	-0.000	-0.001	0.002	-0.000	0.000	-0.001	0.001	-0.001
75	-0.005	-0.007	-0.001	-0.005	-0.003	-0.001	-0.000	-0.000	-0.001	0.010	-0.001	-0.002	-0.003	0.000	-0.002
76	-0.002	-0.002	-0.000	0.000	-0.000	0.000	-0.000	-0.001	-0.002	0.003	-0.001	-0.001	-0.002	0.002	-0.001
77	0.001	-0.000	-0.000	-0.001	-0.002	0.000	0.000	-0.000	-0.000	0.000	-0.000	-0.000	-0.001	0.001	-0.000
78	-0.001	0.001	0.000	0.001	0.002	-0.000	-0.000	-0.000	-0.000	-0.003	0.000	0.000	0.001	0.000	0.001
79	-0.006	-0.004	-0.001	-0.003	-0.002	-0.001	-0.000	-0.000	-0.001	0.003	-0.000	-0.001	-0.001	0.000	-0.001
80	-0.001	0.002	0.001	0.003	0.004	0.000	-0.001	-0.000	-0.000	-0.003	0.000	0.001	0.001	0.000	0.001
81	0.006	-0.001	-0.001	-0.003	-0.007	-0.000	0.002	0.001	0.002	-0.001	0.000	0.000	0.000	-0.001	-0.001
82	-0.001	-0.002	-0.001	-0.001	-0.003	-0.001	0.001	-0.000	-0.001	-0.001	-0.000	-0.000	-0.000	0.001	-0.001
83	-0.001	0.004	0.003	0.006	0.010	0.000	-0.002	0.000	0.001	-0.004	0.001	0.001	0.003	-0.002	0.002
84	0.002	0.001	0.001	0.001	0.002	0.001	-0.000	-0.000	0.000	0.001	-0.001	-0.000	-0.000	0.000	0.000

	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60
46	0.002														
47	-0.002	0.007													
48	-0.000	0.001	0.000												
49	-0.001	-0.001	-0.000	0.008											
50	-0.001	0.001	0.000	-0.001	0.001										
51	-0.001	0.001	0.000	-0.001	0.001	0.001									
52	0.001	-0.001	-0.001	-0.002	0.001	0.000	0.009								
53	-0.002	0.001	0.001	-0.001	0.002	0.001	-0.003	0.003							
54	-0.001	0.000	0.000	0.003	0.000	0.000	-0.001	0.000	0.001						
55	-0.001	0.000	0.000	0.000	0.001	0.000	0.000	0.001	0.000	0.001					
56	-0.001	0.001	0.000	-0.001	0.000	0.001	-0.001	0.001	0.000	-0.000	0.002				
57	0.002	-0.004	-0.000	0.003	-0.001	-0.002	-0.000	-0.002	-0.000	-0.000	-0.002	0.004			
58	-0.000	0.000	0.000	-0.000	0.000	0.000	-0.001	0.001	0.000	0.000	0.000	-0.001	0.000		
59	0.001	0.000	-0.001	-0.000	-0.001	-0.001	0.004	-0.003	-0.000	-0.001	0.001	-0.001	-0.001	0.004	
60	-0.001	0.001	0.000	-0.000	0.001	0.001	-0.002	0.002	0.000	0.000	0.002	-0.002	0.000	-0.001	0.002
61	0.000	-0.003	-0.000	0.004	-0.001	-0.001	-0.001	-0.000	0.001	-0.000	0.001	0.002	-0.000	0.000	0.000
62	-0.000	-0.000	0.000	0.002	0.000	0.000	-0.002	0.001	0.000	-0.000	-0.000	0.000	0.000	-0.001	-0.000
63	-0.001	-0.001	0.000	0.002	0.001	0.000	-0.001	0.001	0.001	0.001	-0.000	0.001	0.000	-0.001	0.000
64	-0.002	0.004	0.001	-0.001	0.001	0.002	-0.003	0.003	0.001	0.000	0.002	-0.004	0.001	-0.002	0.002
65	-0.000	-0.003	0.000	0.004	-0.001	-0.001	-0.004	0.000	0.001	0.000	-0.000	0.003	-0.000	-0.002	0.001
66	-0.001	0.001	0.000	0.001	0.000	0.000	-0.001	0.001	0.000	0.000	-0.000	-0.000	0.000	-0.001	-0.000
67	-0.001	0.007	0.001	0.001	-0.001	0.000	-0.004	0.000	0.000	0.000	-0.001	-0.002	-0.000	-0.001	0.001
68	-0.001	-0.001	0.000	0.002	0.000	0.000	-0.002	0.001	0.001	0.000	-0.000	0.001	0.000	-0.002	-0.000
69	-0.001	-0.001	-0.000	0.000	0.001	0.001	0.002	0.001	0.001	0.000	0.000	-0.000	0.000	-0.000	0.000
70	0.001	-0.001	-0.001	-0.001	0.001	0.000	0.006	-0.001	0.000	0.000	0.001	-0.001	-0.000	0.003	-0.000
71	0.001	-0.000	-0.000	0.001	-0.001	-0.001	-0.001	-0.001	-0.000	-0.000	-0.000	0.001	-0.000	0.000	-0.000
72	0.001	-0.003	-0.001	-0.003	0.000	-0.001	0.003	-0.001	-0.002	-0.001	-0.001	0.001	0.000	0.000	-0.002
73	0.000	-0.005	-0.001	0.002	0.001	0.000	0.002	0.000	0.001	0.000	-0.001	0.002	0.000	-0.001	-0.002
74	0.000	0.000	0.000	-0.000	0.000	-0.000	0.001	-0.001	-0.000	0.000	-0.001	0.001	-0.000	-0.001	-0.002
75	0.002	-0.004	0.000	-0.002	-0.001	-0.002	-0.004	0.000	-0.003	-0.000	-0.003	0.005	-0.000	-0.005	-0.002
76	0.001	-0.004	-0.001	-0.000	-0.000	-0.001	0.001	-0.001	-0.001	-0.001	-0.002	0.002	0.000	-0.001	-0.002
77	0.000	-0.001	-0.000	0.003	-0.001	-0.000	-0.000	-0.001	0.001	-0.000	-0.000	0.001	-0.000	0.000	-0.001
78	0.000	-0.002	-0.001	0.002	0.000	0.000	0.002	-0.001	0.001	-0.000	0.001	-0.000	-0.000	0.002	-0.000
79	0.000	-0.004	-0.000	0.001	0.000	-0.001	-0.002	0.001	-0.000	0.000	-0.001	0.003	0.000	-0.002	-0.001
80	0.000	-0.000	-0.000	-0.003	0.001	0.001	0.003	0.000	-0.001	-0.000	0.001	-0.002	0.000	0.001	0.000
81	-0.002	0.005	0.001	0.005	-0.001	0.000	-0.006	0.001	0.002	0.000	0.001	-0.001	-0.000	-0.001	0.001
82	-0.000	-0.002	-0.000	0.003	-0.000	-0.000	-0.002	0.000	0.001	-0.000	-0.000	0.001	0.000	-0.001	-0.001
83	0.000	0.005	0.001	-0.015	0.002	0.002	0.004	0.002	-0.004	0.000	0.002	-0.007	0.001	0.000	0.003
84	0.001	0.000	-0.000	-0.003	-0.000	-0.000	0.001	-0.001	-0.001	-0.000	-0.000	0.000	-0.000	0.001	-0.001

	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75
61	0.004														
62	0.000	0.002													
63	0.001	0.000	0.001												
64	-0.002	0.002	-0.000	0.006											
65	-0.003	0.001	0.002	-0.001	0.005										
66	-0.000	0.001	0.000	0.001	0.000	0.001									
67	-0.003	0.000	-0.001	0.002	-0.000	0.001	0.010								
68	0.001	0.002	0.001	0.001	0.001	0.001	-0.001	0.002							
69	0.001	-0.000	0.001	-0.000	0.000	-0.000	-0.002	0.000	0.001						
70	0.001	-0.002	-0.000	-0.002	-0.002	-0.001	-0.005	-0.001	0.002						
71	0.000	0.000	-0.000	-0.001	0.001	-0.000	0.001	0.000	-0.001	0.006					
72	-0.001	0.001	-0.001	-0.001	-0.002	0.000	-0.004	0.000	-0.000	0.001	0.000	0.005			
73	0.002	0.002	0.002	-0.001	0.001	0.001	-0.006	0.002	0.002	0.002	-0.000	0.003	0.007		
74	-0.001	0.001	0.000	-0.000	-0.001	0.001	0.001	0.001	-0.000	-0.001	0.000	0.002	0.001	0.002	
75	-0.002	0.001	0.001	-0.002	0.002	0.001	-0.000	0.001	-0.002	-0.005	0.001	0.004	0.002	0.002	0.014
76	0.000	0.001	0.000	-0.001	0.000	0.001	-0.004	0.002	-0.000	-0.000	0.000	0.004	0.004	0.002	0.005
77	0.002	0.001	0.000	-0.001	0.001	0.000	-0.001	0.001	0.000	-0.000	0.000	0.000	0.002	0.000	-0.001
78	0.002	-0.000	0.000	-0.001	0.000	-0.000	-0.003	0.000	0.001	0.003	-0.000	-0.000	0.002	-0.001	-0.004
79	0.001	0.001	0.001	-0.001	0.002	0.000	-0.003	0.002	0.000	-0.001	0.000	0.001	0.003	0.000	0.005
80	-0.001	-0.001	-0.001	0.000	-0.002	-0.001	-0.003	-0.001	0.001	0.003	-0.001	0.001	0.001	-0.000	-0.002
81	0.001	0.001	0.000	0.003	0.002	0.001	0.007	0.001	-0.001	-0.004	0.001	-0.005	-0.004	-0.000	-0.003
82	0.002	0.002	0.001	0.001	0.001	0.001	-0.002	0.002	-0.000	-0.001	0.000	0.001	0.003	0.000	0.001
83	-0.008	-0.004	-0.003	0.002	-0.008	-0.002	0.002	-0.005	-0.000	0.002	-0.001	0.002	-0.006	-0.000	0.001
84	-0.001	-0.001	-0.001	-0.001	-0.001	-0.000	0.000	-0.001	-0.001	-0.000	0.000	0.001	-0.001	0.000	0.002

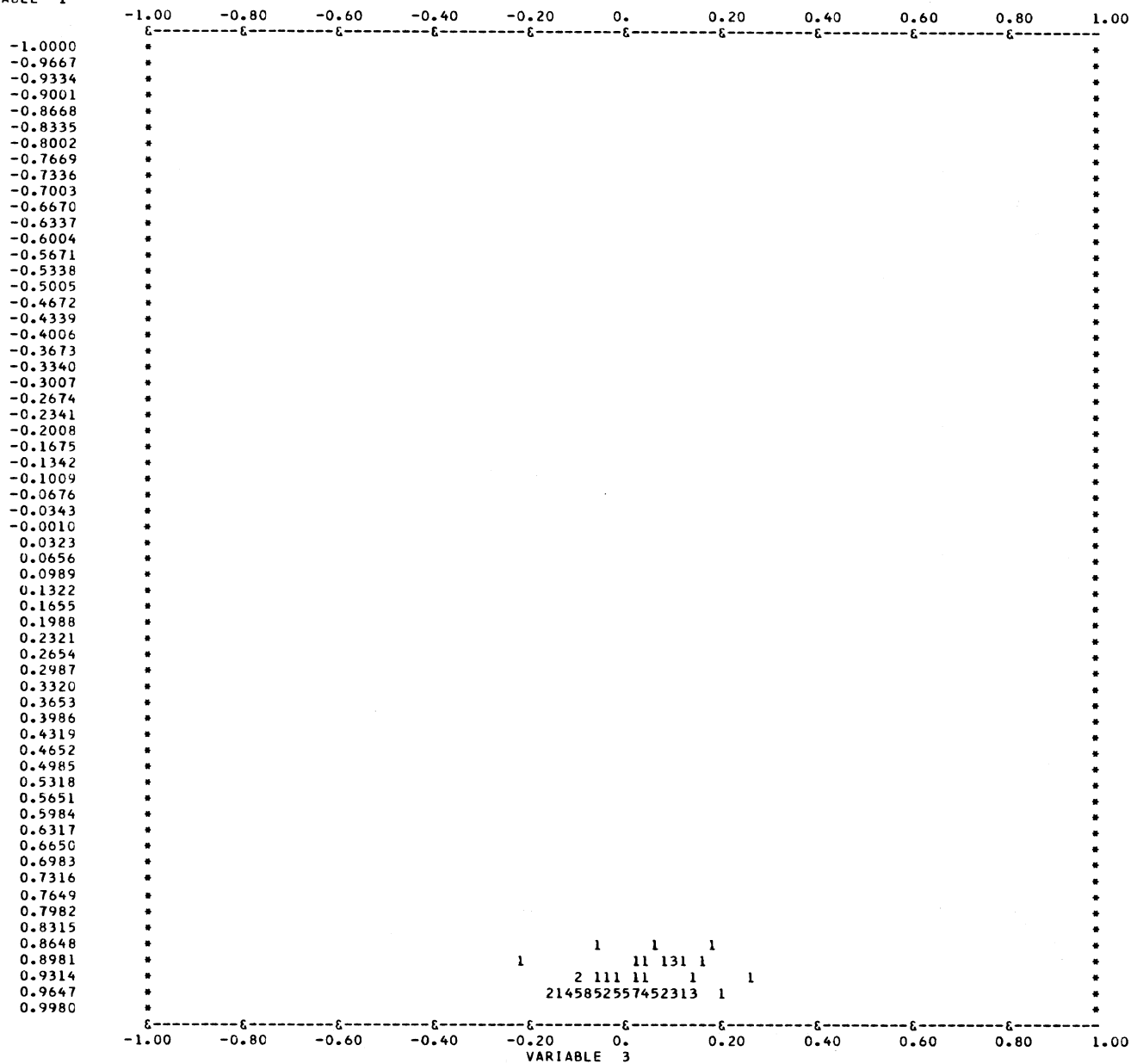
	76	77	78	79	80	81	82	83	84
76	0.005								
77	0.001	0.001							
78	0.000	0.001	0.002						
79	0.003	0.001	-0.000	0.003					
80	0.000	-0.001	0.001	-0.001	0.003				
81	-0.004	0.001	-0.001	-0.002	-0.004	0.009			
82	0.002	0.002	0.001	0.002	-0.001	0.001	0.003		
83	-0.003	-0.007	-0.004	-0.004	0.006	-0.007	-0.006	0.030	
84	0.000	-0.001	-0.001	-0.000	0.001	-0.002	-0.001	0.004	0.001

SCATTERGRAM OF FACTOR LOADING
 FACTOR 1 VS. 2

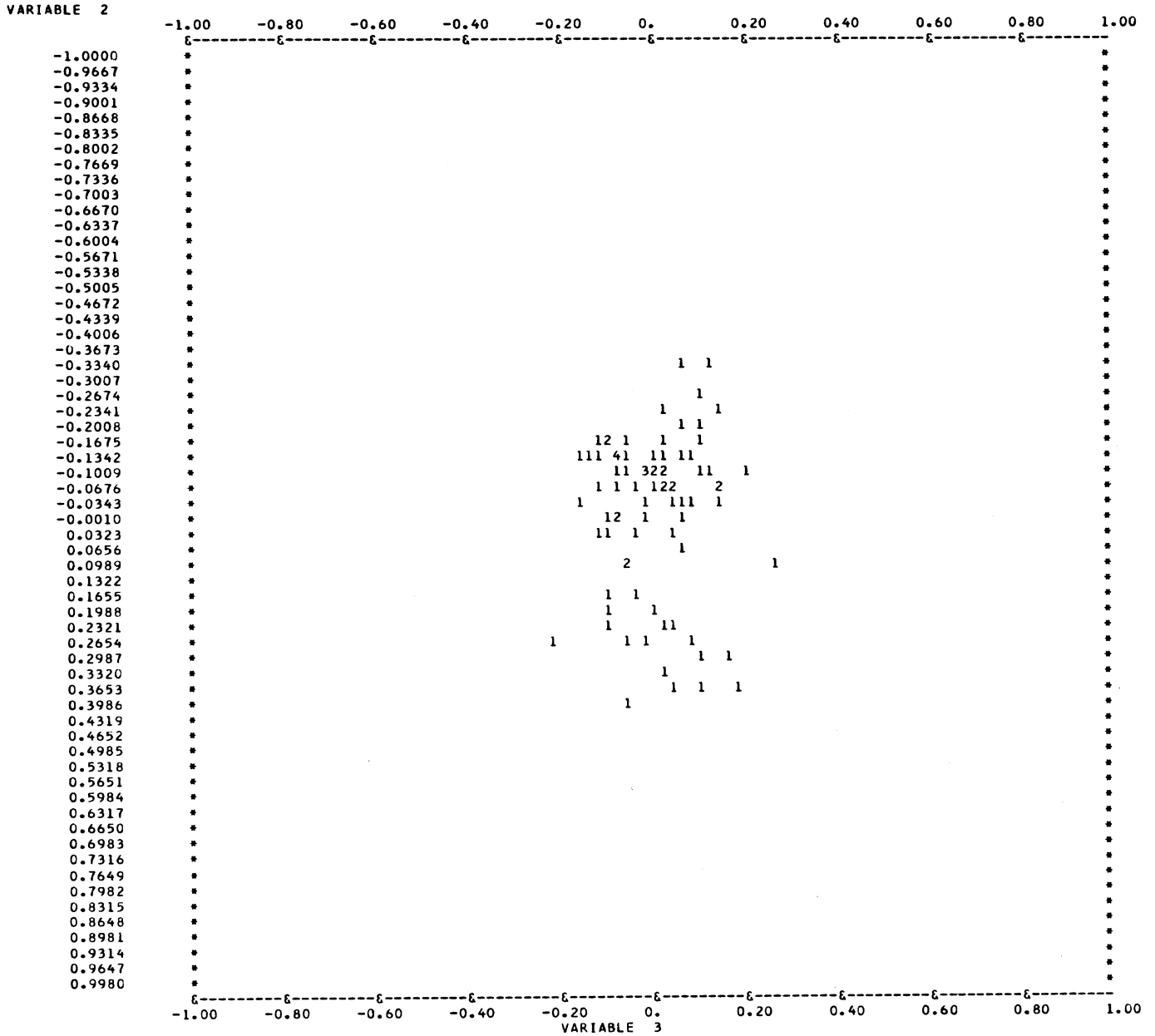


SCATTERGRAM OF FACTOR LOADING
 FACTOR 1 VS. 3

VARIABLE 1



SCATTERGRAM OF FACTOR LOADING
 FACTOR 2 VS. 3



VARIMAX ROTATION

THOLEIITIC - ALKALIC BASALT PROBLEM Q-MODE FACTOR ANALYSIS

PROBLEM NAME QMODFNV1 84 VARIABLES , 3 FACTORS

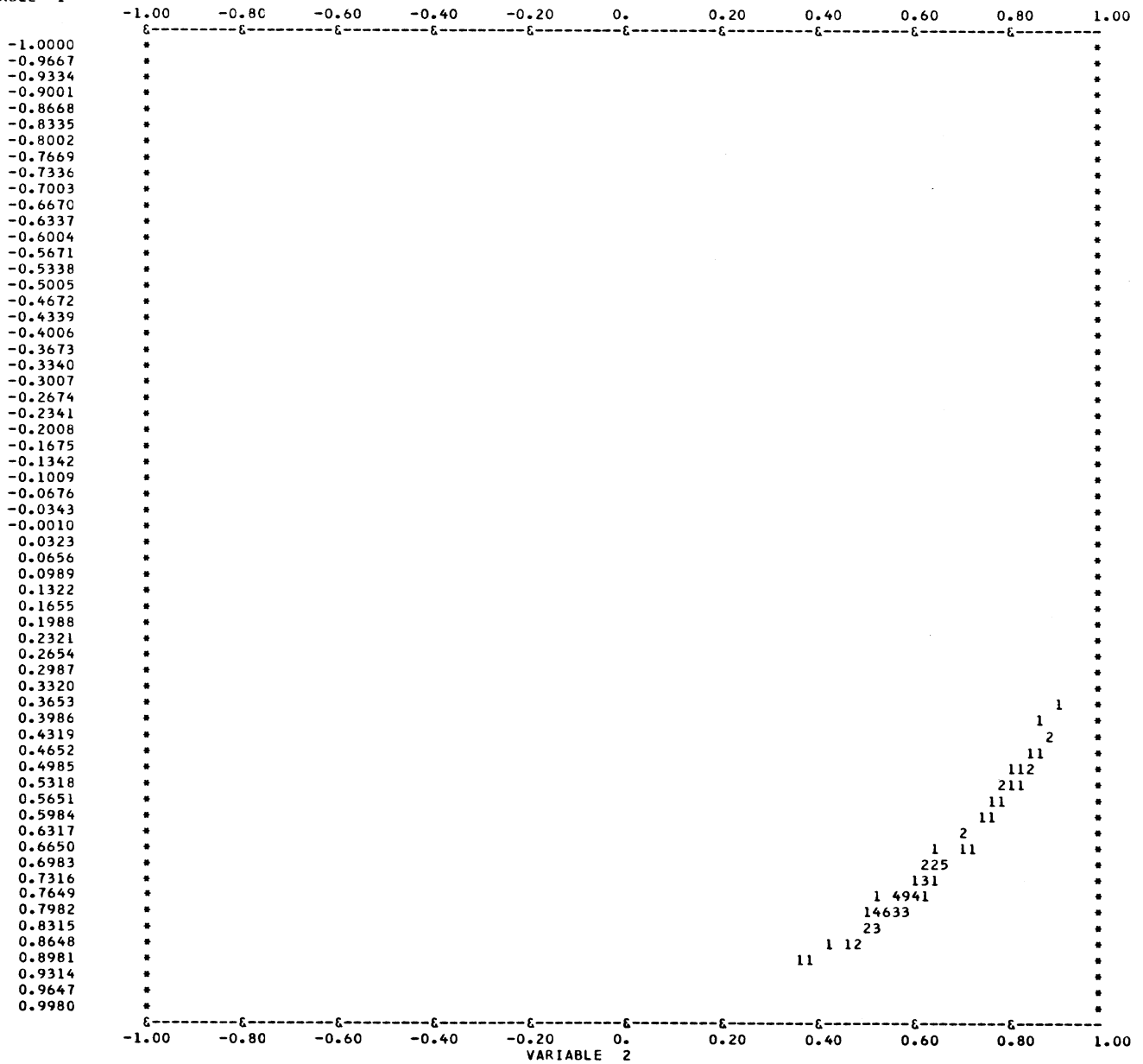
THE ORIGINAL MATRIX OF FACTOR LOADINGS											
	F 1	F 2	F 3	F 4	F 5	F 6	F 7	F 8	F 9	F 10	COMMUNALITIES
1	0.87756	0.42176	-0.06333	-0.15647	0.10868						1 0.98830
2	0.89289	0.38767	0.17120	0.08268	-0.12329						2 0.99889
3	0.91070	0.38798	0.09463	-0.03805	0.00803						3 0.99036
4	0.92054	0.36881	0.03542	-0.06148	0.05877						4 0.99190
5	0.92855	0.34968	0.02063	-0.05280	0.06784						5 0.99229
6	0.92499	0.32477	0.16733	0.05599	-0.02828						6 0.99301
7	0.93124	0.30336	0.09626	-0.03825	-0.07200						7 0.97515
8	0.91428	0.29612	0.08620	-0.15123	0.15152						8 0.97686
9	0.95043	0.28326	-0.02242	-0.01679	-0.10769						9 0.99593
10	0.94916	0.27289	-0.06236	-0.05678	0.05290						10 0.98528
11	0.92056	0.26552	-0.22702	-0.14544	0.07503						11 0.99626
12	0.93973	0.24616	0.01003	-0.03108	0.10930						12 0.95670
13	0.94888	0.23655	0.03215	0.09049	-0.11533						13 0.97885
14	0.95622	0.23909	-0.10465	-0.00080	-0.09803						14 0.99208
15	0.97043	0.21204	0.00673	-0.03377	-0.08571						15 0.99524
16	0.96721	0.20298	-0.10960	0.01570	-0.07713						16 0.99491
17	0.95019	0.18776	-0.04945	-0.13886	0.08951						17 0.96786
18	0.96320	0.17467	-0.09364	-0.05386	-0.02908						18 0.97078
19	0.94767	0.11282	0.26016	0.05178	-0.12032						19 0.99565
20	0.98855	0.10692	-0.05708	-0.06410	-0.02978						20 0.99692
21	0.97738	0.11610	-0.06411	-0.02098	-0.14725						21 0.99499
22	0.98736	0.08405	0.05903	0.06893	-0.00294						22 0.99019
23	0.98418	0.04185	-0.04704	0.02946	0.05017						23 0.97596
24	0.97839	0.03992	-0.12653	0.06025	-0.13010						24 0.99540
25	0.98821	0.04345	0.03137	0.12252	0.02905						25 0.99528
26	0.96545	0.02923	0.05296	0.07685	0.02184						26 0.94214
27	0.99134	0.02906	-0.01628	0.01077	-0.04292						27 0.98583
28	0.99019	0.04674	-0.09775	0.03722	0.02129						28 0.99405
29	0.98215	-0.00338	0.13662	0.08310	0.08466						29 0.99736
30	0.98432	0.00936	-0.07246	0.08026	-0.11076						30 0.99294
31	0.96795	0.03012	-0.07322	-0.16070	0.04048						31 0.97066
32	0.98990	0.00991	-0.09241	0.04277	-0.03163						32 0.99137
33	0.97982	-0.00142	-0.02533	0.02740	-0.04347						33 0.99892
34	0.97883	-0.00581	-0.16951	0.02520	-0.06361						34 0.99157
35	0.98994	-0.01161	0.04941	0.02167	-0.08665						35 0.99054
36	0.99398	-0.01629	0.05126	0.08573	0.00631						36 0.99827
37	0.97931	-0.03563	0.14650	0.12217	0.05180						37 0.99940
38	0.99019	-0.03332	0.07977	0.06088	0.08862						38 0.99951
39	0.97792	-0.04984	0.14435	-0.12687	0.05791						39 0.99910
40	0.98708	-0.04190	-0.07156	-0.02852	0.06091						40 0.98572
41	0.99197	-0.05656	0.04059	0.06345	0.07898						41 0.99911
42	0.99066	-0.06370	0.01527	0.09125	0.07125						42 0.99911
43	0.99304	-0.07346	0.00713	0.06467	0.05073						43 0.99833
44	0.98950	-0.05812	-0.11786	0.03551	-0.03115						44 0.99861
45	0.98641	-0.15869	0.01833	-0.01804	-0.00862						45 0.99891
46	0.99564	-0.05242	0.00234	-0.00151	-0.06594						46 0.99840
47	0.99034	-0.06163	0.04758	-0.07995	-0.01262						47 0.99339
48	0.99297	-0.07050	-0.01894	0.07782	0.04830						48 0.99971
49	0.97070	-0.08539	0.19723	-0.01214	-0.05545						49 0.99166
50	0.99297	-0.07427	0.02673	0.03198	0.07278						50 0.99854
51	0.99254	-0.06696	0.02764	0.06716	0.06335						51 0.99890
52	0.98977	-0.06479	-0.04332	0.07169	-0.01765						52 0.99116
53	0.98820	-0.08566	0.02258	0.02367	0.10875						53 0.99678
54	0.99475	-0.07102	-0.02784	0.04604	0.03437						54 0.99866
55	0.99121	-0.09129	-0.02435	0.05870	0.06733						55 0.99941
56	0.98752	-0.09533	0.10850	0.02848	0.03565						56 0.99814
57	0.98684	-0.08565	-0.05153	-0.10797	-0.00600						57 0.99553
58	0.99423	-0.10452	0.00724	-0.00830	-0.01194						58 0.99968
59	0.98775	-0.08875	0.00330	0.11036	0.00494						59 0.99575
60	0.98759	-0.10692	0.08701	0.02089	0.05263						60 0.99754
61	0.98549	-0.10595	0.01063	0.08589	0.07819						61 0.99602
62	0.99060	-0.09430	-0.07844	0.04255	0.00764						62 0.99821
63	0.98763	-0.11216	-0.08648	0.04173	0.03986						63 0.99880
64	0.97198	-0.10870	-0.15216	0.07790	-0.09022						64 0.99392
65	0.98797	-0.12496	0.05964	-0.00324	0.00314						65 0.99527
66	0.99028	-0.11327	-0.07173	0.02213	0.00517						66 0.99914
67	0.97922	-0.11830	-0.12367	0.03784	-0.02303						67 0.99013
68	0.98723	-0.12597	-0.08302	0.00485	0.02267						68 0.99792
69	0.98822	-0.12479	-0.06572	0.02971	0.03884						69 0.99887
70	0.98493	-0.12884	-0.08454	0.02280	-0.00693						70 0.99441
71	0.98225	-0.14852	0.10684	-0.03418	-0.00327						71 0.99948
72	0.97954	-0.12758	-0.13738	0.02586	-0.00855						72 0.99540
73	0.97932	-0.13848	-0.11997	0.00473	0.01079						73 0.99278
74	0.98553	-0.15536	-0.05308	-0.00903	-0.01139						74 0.99844
75	0.97391	-0.15865	-0.10115	0.02680	0.03238						75 0.98566
76	0.97566	-0.16449	-0.10893	-0.05663	0.03704						76 0.99541
77	0.97581	-0.18149	0.06340	-0.07990	-0.05444						77 0.99850
78	0.97040	-0.20008	0.09120	-0.06653	-0.05548						78 0.99753
79	0.96858	-0.20923	0.02362	-0.11010	-0.04902						79 0.99701
80	0.94796	-0.22954	0.14531	-0.15213	-0.04206						80 0.99734
81	0.92873	-0.26095	0.09049	-0.22433	-0.04369						81 0.99104
82	0.92044	-0.30303	0.12951	-0.19763	-0.05137						82 0.99750
83	0.89386	-0.31306	0.06388	-0.25505	-0.05828						83 0.96952
84	0.98778	-0.07608	0.11878	-0.03348	0.04419						84 0.99868
SUM SQ	79.23934	2.47862	0.72735	0.54935	0.35204						
VAREXP	94.33255	2.95074	0.86589	0.65399	0.41909						
CUMPER	94.33255	97.28329	98.14919	98.80318	99.22227						

THE ROTATED MATRIX OF FACTOR LOADINGS

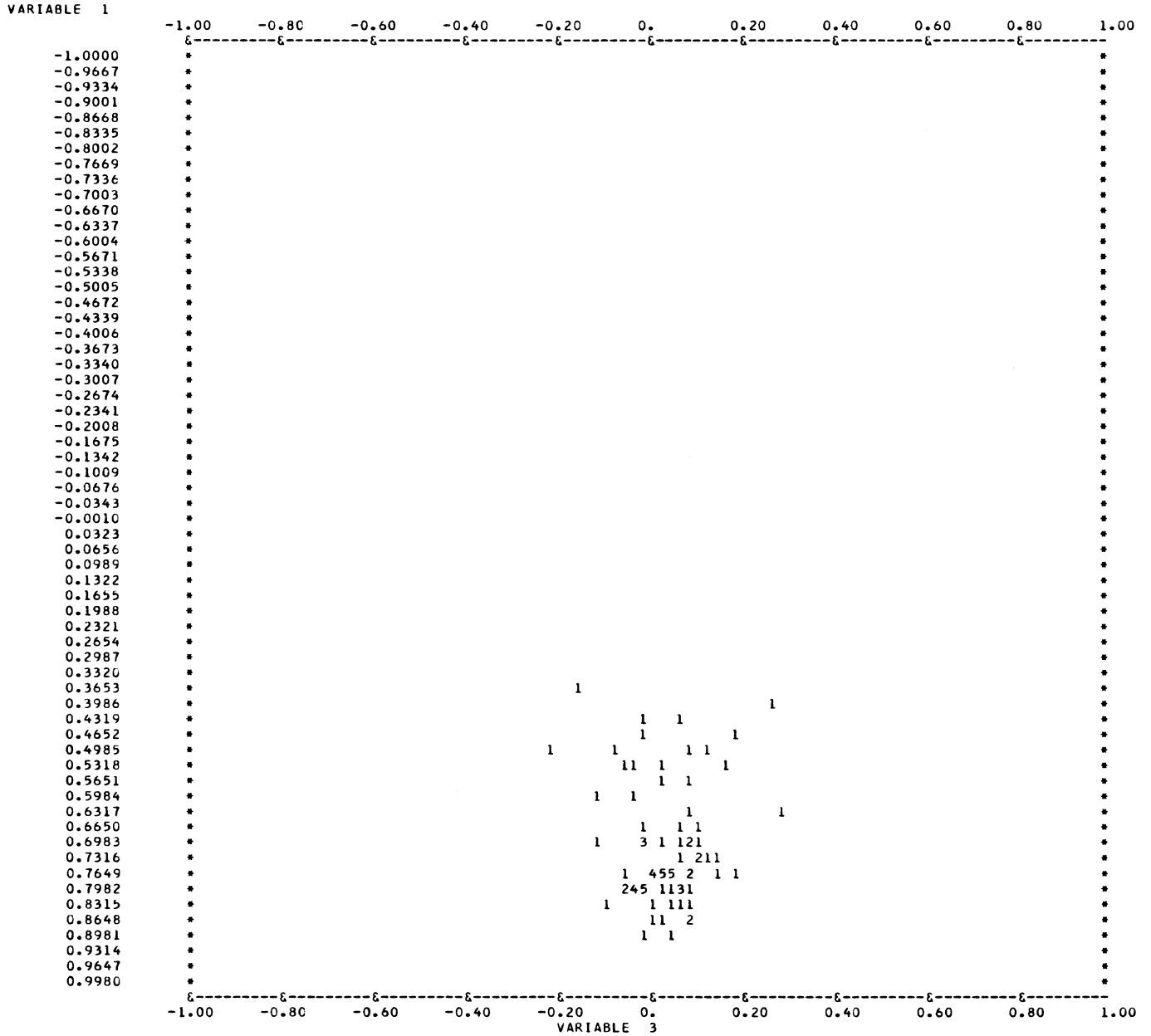
	F 1	F 2	F 3	F 4	F 5	F 6	F 7	F 8	F 9	F 10	COMMUNALITIES
1	0.39572	0.89730	-0.15018								1 0.98429
2	0.41882	0.86475	0.25231								2 0.98687
3	0.44062	0.88731	0.06616								3 0.98584
4	0.45959	0.87944	-0.01346								4 0.98481
5	0.47641	0.86864	-0.02439								5 0.98209
6	0.48821	0.84230	0.17678								6 0.97907
7	0.50938	0.83444	0.11803								7 0.96969
8	0.51622	0.83400	-0.08412								8 0.96911
9	0.52560	0.82220	0.07830								9 0.95839
10	0.53596	0.81918	-0.06788								10 0.96291
11	0.51622	0.79568	-0.22462								11 0.95004
12	0.55041	0.79556	-0.04856								12 0.93822
13	0.54873	0.77798	0.16520								13 0.93366
14	0.55160	0.78668	0.02860								14 0.92394
15	0.59111	0.78473	0.07396								15 0.97068
16	0.58197	0.76495	0.01956								16 0.92422
17	0.60145	0.76485	-0.12212								17 0.96164
18	0.60602	0.74972	-0.03387								18 0.93048
19	0.64807	0.69914	0.28895								19 0.99228
20	0.67267	0.71749	-0.01580								20 0.96752
21	0.65113	0.70986	0.07492								21 0.93349
22	0.68339	0.69319	0.09878								22 0.95729
23	0.70576	0.65862	-0.01910								23 0.93224
24	0.68999	0.64183	0.06192								24 0.89186
25	0.70431	0.65698	0.08532								25 0.93495
26	0.70207	0.63704	0.08146								26 0.90535
27	0.72120	0.65472	0.05107								27 0.95139
28	0.70209	0.66201	-0.02786								28 0.93196
29	0.74267	0.62837	0.09533								29 0.95549
30	0.71681	0.62383	0.09160								30 0.91138
31	0.71655	0.65630	-0.11665								31 0.95778
32	0.72449	0.63234	0.01150								32 0.92488
33	0.74371	0.63362	0.05330								33 0.95742
34	0.72179	0.61016	-0.02379								34 0.89384
35	0.74929	0.62434	0.12391								35 0.96659
36	0.75180	0.61945	0.09471								36 0.95788
37	0.75790	0.59799	0.13993								37 0.95158
38	0.76627	0.61004	0.04760								38 0.96158
39	0.76567	0.58588	0.13662								39 0.94817
40	0.76627	0.60155	-0.06856								40 0.95373
41	0.77948	0.59097	0.03070								41 0.95777
42	0.77861	0.58046	0.03275								42 0.94424
43	0.78813	0.57624	0.02871								43 0.95402
44	0.76734	0.57983	-0.00860								44 0.92509
45	0.84563	0.51458	0.03458								45 0.98108
46	0.77938	0.59728	0.07077								46 0.96919
47	0.79306	0.59828	0.02805								47 0.98766
48	0.78303	0.57572	0.02035								48 0.94500
49	0.79725	0.56796	0.17757								49 0.98972
50	0.79351	0.58036	0.01158								50 0.96661
51	0.78505	0.58201	0.03439								51 0.95621
52	0.77419	0.57570	0.04494								52 0.93283
53	0.79865	0.57013	-0.01818								53 0.96322
54	0.78666	0.57876	0.00932								54 0.95388
55	0.79706	0.56085	-0.00427								55 0.94987
56	0.80842	0.56469	0.08357								56 0.97940
57	0.80172	0.57542	-0.05023								57 0.97639
58	0.81447	0.55907	0.03527								58 0.97717
59	0.78860	0.55547	0.07639								59 0.93627
60	0.81557	0.55595	0.05586								60 0.97736
61	0.80257	0.54552	0.02232								61 0.94221
62	0.79479	0.55543	-0.00654								62 0.94024
63	0.80444	0.54040	-0.03286								63 0.94024
64	0.77943	0.52281	0.02662								64 0.88154
65	0.82670	0.54221	0.05961								65 0.98099
66	0.80919	0.54312	-0.01044								66 0.94988
67	0.79838	0.52723	-0.01735								67 0.91567
68	0.81636	0.53305	-0.03677								68 0.95193
69	0.81566	0.53346	-0.02512								69 0.95051
70	0.81406	0.52684	-0.01056								70 0.94037
71	0.84381	0.52606	0.07804								71 0.99485
72	0.80512	0.52118	-0.04066								72 0.92150
73	0.81567	0.51624	-0.05223								73 0.93455
74	0.83683	0.51179	-0.00329								74 0.96222
75	0.82457	0.49682	-0.04486								75 0.92875
76	0.83687	0.50138	-0.09087								76 0.96000
77	0.86034	0.49783	0.06275								77 0.99195
78	0.86912	0.48040	0.08621								78 0.99359
79	0.87304	0.47311	0.02048								79 0.98645
80	0.88348	0.45525	0.07055								80 0.99277
81	0.89218	0.42319	0.00395								81 0.97508
82	0.91352	0.38522	0.04430								82 0.98487
83	0.90054	0.36253	-0.01870								83 0.94275
84	0.80268	0.58630	0.05624								84 0.99120
SUM SQ	45.60176	34.01126	0.59869								
VAREXP	54.28781	40.48959	0.71273								
CUMPER	54.28781	94.77740	95.49013								

SCATTERGRAM OF ROTATED FACTORS
 FACTOR 1 VS. 2

VARIABLE 1

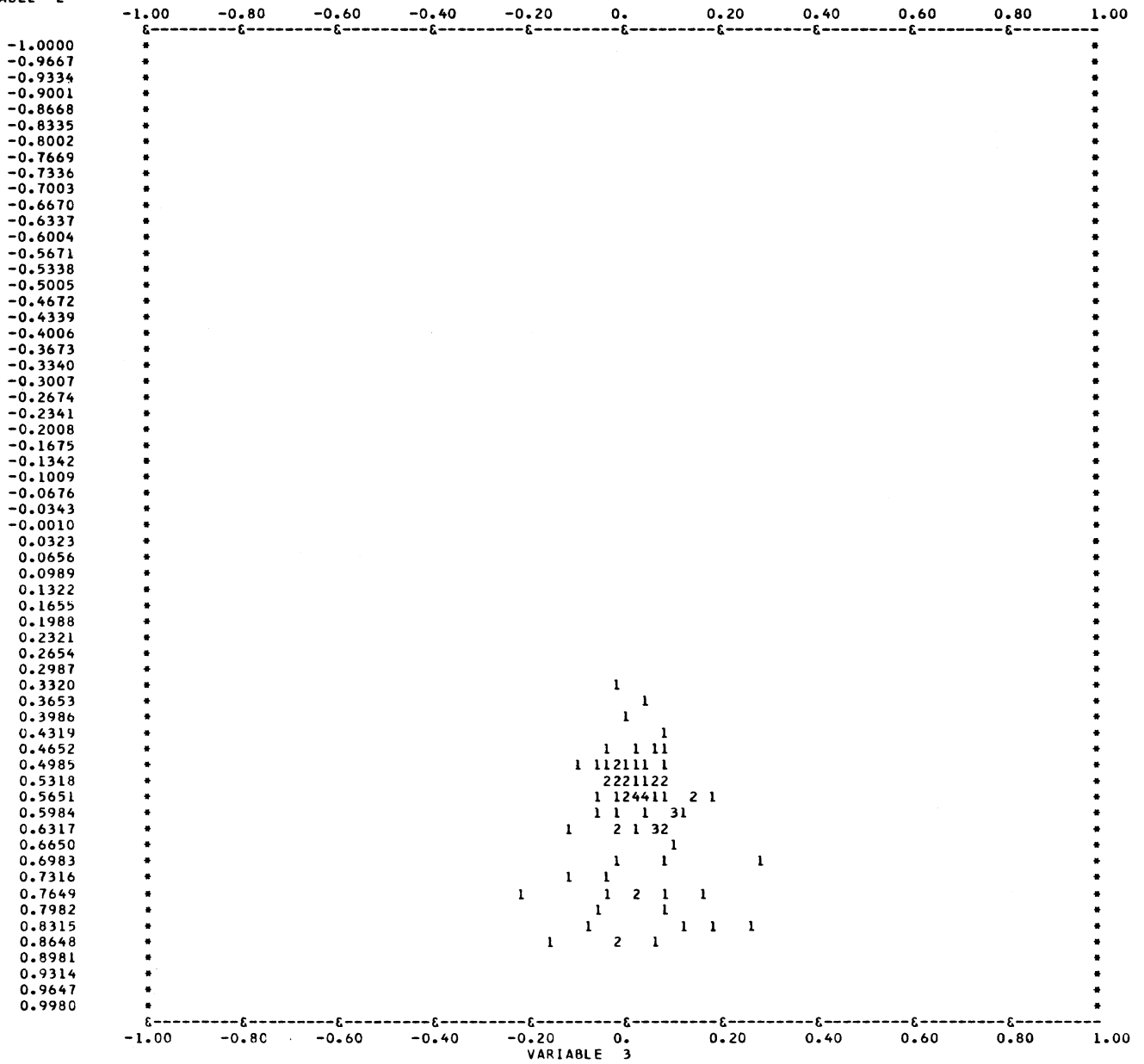


SCATTERGRAM OF ROTATED FACTORS
 FACTOR 1 VS. 3



SCATTERGRAM OF ROTATED FACTORS
 FACTOR 2 VS. 3

VARIABLE 2



****YOUR REQUESTED COMPUTATION IS COMPLETE, ITS BEEN NICE DOING BUSINESS WITH YOU****

KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

CORFAN - FORTRAN IV Computer Program for Correlation, Factor Analysis (R- and Q-Mode)
and Varimax Rotation

Date: May, 1969

Author, organization: C.W. Ondrick and G.S. Srivastava

Kansas Geological Survey, University of Kansas, Lawrence, Kansas 66044

Direct inquiries to: Authors, or

Name: D.F. Merriam

Address: Kansas Geological Survey

Lawrence, Kansas 66044

Purpose/description: Computation of correlation coefficients (≤ 100 Variables) and production of factor analysis in the R- and Q-modes together with optional VARIMAX rotation on K original factors. Options are provided to produce desired scatter diagrams of original data (X vs. Y) and plots of loadings of one factor against the other for unrotated and rotated factor matrix.

Mathematical method: Pearson product moment correlation coefficients, R-mode factor analysis, $\text{Cos } \theta$, Q-mode factor analysis (Imbrie and Purdy, 1962) and Kaiser varimax rotation (Kaiser, 1958)

Restrictions, range: Accepts, with the present program dimension, 100 variables and an unlimited sample size. Produces up to 100 and rotates ≤ 60 factors.

Computer manufacturer: GE or IBM

Model: 635 or System/360 Model 50

Programming language: FORTRAN IV

Memory required: _____ K Approximate running time: _____

Special peripheral equipment required: None

Remarks (special compilers or operating systems, required word lengths, number of successful runs, other machine versions, additional information useful for operation or modification of program) _____

Approximately 45K is required on the GE 635; 205K on the IBM System/360. About 3 minutes is necessary running time for a given problem on the GE 635.

(continued from inside front cover)

10. Three-dimensional response surface program in FORTRAN II for the IBM 1620 computer, by R.J. Sampson and J.C. Davis, 1967	\$0.75
11. FORTRAN IV program for vector trend analyses of directional data, by W.T. Fox, 1967	\$1.00
12. Computer applications in the earth sciences: Colloquium on trend analysis, edited by D.F. Merriam and N.C. Cocks, 1967	\$1.00
13. FORTRAN IV computer programs for Markov chain experiments in geology, by W.C. Krumbein, 1967	\$1.00
14. FORTRAN IV programs to determine surface roughness in topography for the CDC 3400 computer, by R.D. Hobson, 1967	\$1.00
15. FORTRAN II program for progressive linear fit of surfaces on a quadratic base using an IBM 1620 computer, by A.J. Cole, C. Jordan, and D.F. Merriam, 1967	\$1.00
16. FORTRAN IV program for the GE 625 to compute the power spectrum of geological surfaces, by J.E. Esler and F.W. Preston, 1967	\$0.75
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35. FORTRAN IV computer program for fitting observed count data to discrete distribution models of binomial, Poisson and negative binomial, by C.W. Ondrick and J.C. Griffiths, 1969	\$0.75
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38. FORTRAN II programs for 8 methods of cluster analysis (CLUSTAN I), by David Wishart, 1969	\$1.50
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42. CORFAN-FORTRAN IV computer program for correlation, factor analysis (R- and Q-mode) and varimax rotation, by C.W. Ondrick and G.S. Srivastava, 1970	\$1.50

